

# HYDROGEOLOGIC ASSESMENT

Knight-Dillacort Area of High Prairie,  
WRIA 30

Prepared for: Klickitat County Department of Natural  
Resources

Project No. 090045-017B-01 • July 27, 2015



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# 1 Introduction and Background

Water level monitoring initiated in the High Prairie area of the Klickitat River Watershed, Water Resource Inventory Area (WRIA) 30 (Figure 1), has documented trends of declining groundwater levels in three wells within the monitoring network. This information was initially documented in the 2011 report entitled Hydrologic Information Report Supporting Water Availability Assessment, High Prairie Study Area (Aspect, 2011), which was presented to a meeting of the High Prairie community in August 2011. Following two additional years of water level monitoring in the High Prairie well network, the water level declines in the previously identified wells were documented to persist, although one showed signs of stabilizing (Aspect, 2013). The observed water declines are limited to wells located within the portion of High Prairie between Knight Canyon and Dillacort Canyon (“Knight-Dillacort area”; Figure 1).

Residents of High Prairie have contacted Klickitat County periodically over the past few years to express concerns regarding wells and declining water levels in the area. In July of 2014, the High Prairie Community Council wrote a letter to the Klickitat County (County) Board of Commissioners expressing concerns regarding declining water levels and wells being deepened within an area near the intersection of Centerville Highway and Mount Adams View Road (High Prairie Community Council, 2014). Some of the wells identified in the letter were being monitored as part of the High Prairie well monitoring network, and some were not.

In response, the County engaged Aspect Consulting LLC (Aspect) to compile the available information regarding local hydrogeology, the well monitoring program, and the water level declines that had been measured. In December 2014, Aspect and the County participated in a meeting of High Prairie residents to present the technical information, answer questions, and discuss a path forward.

As an outcome of the December 2014 meeting, the County authorized Aspect to conduct a supplemental hydrogeologic assessment of the Knight-Dillacort area focused on identifying potential cause(s) of the observed declines, evaluating available information on the deeper aquifer system as a viable source for water supply, and, depending on identified cause(s) of the declines, assisting the County with identifying actions that can be taken to address the issue. This report presents the results of the hydrogeologic assessment for the Knight-Dillacort area.

Subsequent sections of this report are organized as follows:

- Section 2: Hydrogeologic Setting;
- Section 3: Groundwater Level Trends Over Time;
- Section 4: Assessment of Causes for Water Level Declines;
- Section 5: Assessment of Deeper Aquifer Zones in Study Area;
- Section 6: Conclusions and Recommendations; and

- Section 7: References.

## 2 Hydrogeologic Setting

A detailed discussion of the hydrogeologic setting for the High Prairie study area is provided in Aspect (2011). This section provides an overview of the hydrogeologic information most pertinent to the groundwater conditions of the Knight-Dillacort area.

Figures 2 and 3 are subsurface cross sections oriented east-west and north-south, respectively, across the Knight-Dillacort study area and the surrounding area of High Prairie. Figure 1 depicts the locations of the cross sections<sup>1</sup>. The location of the Knight-Dillacort area is shown on each cross section for reference. The cross sections were developed using well logs from Ecology's well log database, Washington Department of Natural Resources (DNR) regional 1:100,000 geologic mapping, and available information from other studies. The cross sections integrate the following data from each well log: location of well to the nearest quarter-quarter section; well depth; cased interval<sup>2</sup>; static water level; depth and thickness of geologic units encountered; water-bearing zones, if reported; and the surface elevation from the United States Geological Survey (USGS) digital elevation model (DEM). Each cross section depicts the inferred distribution of geologic units, reported water-bearing zones, mapped geologic structures, and wells along its alignment. For each well on the cross section, the figures also present the water level, well yield (in gallons per minute [gpm]), and, if available, specific capacity (gpm yield/feet of drawdown at that yield) that were reported at the time of drilling by the driller on the well log. The cross sections have 10-fold vertical exaggeration, meaning that depicted slopes in surface topography and geologic layering are 10 times greater than reality.

### 2.1 Aquifer Units

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Water wells in the study area generally completed within the bedrock units of the Columbia River Basalt Group (CRBG), with some wells completed in the Dalles Formation, both of which are described below. Although there are pockets of unconsolidated deposits found at the surface in the study area, these units are not expected to be a significant source of groundwater due to their limited continuity and thickness. The primary water-bearing geologic units (aquifer units) in the study area are described below.

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<sup>1</sup> These cross sections B-B' and C-C', while modified for this report, were initially presented in Aspect (2011). Cross section A-A' from that 2011 report is located outside the focus area of this report, so is not included. However, we retain the B-B' and C-C' designations in this report to avoid confusion if referencing back to the 2011 report.

<sup>2</sup> The well's cased portion is not open to adjacent formation and the uncased portion is open to the formation.

### 2.1.1 Columbia River Basalts (Wanapum and Grande Ronde)

The CRBG units are regionally continuous and in the study area have a collective thickness of several thousand feet. The Wanapum basalt formation is consistently present beneath the study area, except where removed by erosion within incised drainages (Klickitat River, Dillacort Canyon, Wheeler Canyon, and Swale Creek), and to the south of the Columbia Hills thrust fault, where it was uplifted and eroded. Where present, the Wanapum basalt is relatively thick, with thicknesses ranging between 500 and 900 feet based on the cross sections (Figures 2 and 3).

**The Wanapum formation** consists of three separate members (from youngest to oldest [shallowest to deepest]) - the Priest Rapids Roza, and Frenchman Springs - each of which is present within the study area (see Figures 2 and 3). Each member is described briefly below.

- **The Priest Rapids member (Mv[wpr])** is generally exposed at the surface across the majority of the study area. However, as depicted on the cross sections it is commonly absent (eroded away) within deeper drainages and is absent south of the Columbia Hills thrust fault. Where present, the Priest Rapids member is typically 100 to 300 feet thick. Few wells are completed solely in this shallowest basalt unit.
- **The Roza member (Mv[wr])** is commonly exposed at the surface along the flanks of the major drainages. The Roza member is absent to the south of the southern thrust fault. Where present north of the Columbia Hills thrust fault, the Roza member can be as much as 150 feet thick. Some wells appear to be producing principally from this unit.
- **The Frenchman Springs member (Mv[wfs])** is also generally exposed at the surface in the major drainages and their respective tributaries. The Frenchman Springs member is also absent immediately south of the Columbia Hills thrust fault. Where present, the Frenchman Springs member generally ranges between 450 and 600 feet in thickness across the study area. Numerous wells in the study area are drilled into the Frenchman Springs, with water bearing zones reported at depths of roughly 600 feet below ground, as depicted on Figure 2.

**The Grande Ronde formation** underlies the Wanapum basalt. The Grande Ronde basalt is present beneath the entire study area, but is generally exposed at the surface only at the base of deeply incised drainages and where it has been uplifted immediately south of the Columbia Hills thrust fault as illustrated in cross section on Figure 3. As the cross sections indicate, there are numerous wells open to and withdrawing groundwater from both the Wanapum and Grande Ronde basalts, but very few wells are completed solely in the Grande Ronde, except where it is exposed in the vicinity of the Klickitat River or other deep drainages, or to the south of the Columbia Hills thrust fault. In the latter area, wells T03/R13-27 and T03/R13-27Q1 are completed solely in the Grande Ronde basalt and are included in the water level monitoring network. These wells have reported static water levels ranging between 100 and 265 feet bgs and driller-reported yields of about 15 gpm.

### **2.1.2 Groundwater Occurrence in Basalt Aquifer Systems**

Throughout the Columbia Basin, groundwater in the CRBG occurs primarily within the tops of the individual flows (flow tops) that became vesicular (porous) as gas bubbles escaped the flows during cooling, and/or within the fractured flow bottoms (sometimes referred to as pillows). Flow tops and bottoms – collectively referred to as interflow zones – are usually porous and permeable, and therefore transmit water more readily than the intervening massive portions of the basalt flow interior, which generally constitute flow barriers, except where fractured. In addition, terrestrial sediments can be deposited between the underlying flow top and overlying flow bottom during time periods between basalt flows. These sediments are collectively considered part of the Ellensburg formation (Mc[e]) and can be either relatively permeable or impermeable; depending on composition, thickness, and lateral extent (Brown, 1979).

Based on the cross sections and the individual well logs, the water-bearing interflow zones in the study area have thicknesses ranging between 10 and 80 feet. However, both the lateral continuity and thickness of the water-bearing interflow zones are highly variable. This leads to variability in depths and productivity of water wells throughout the study area.

### **2.1.3 Dalles Formation**

Geologically younger than the CRBG, the Dalles Formation (Mc[d]) consists of thickly bedded volcanoclastic and sedimentary deposits, which can be as much as 250 feet thick in the study area. Where the Dalles Formation is present at the surface, wells appear to be drilled through it into the underlying Wanapum basalt, indicating the basalt is the principal source of water (e.g., see wells T3/R13-22C1 and T3/R13-27B1 on Figure 3).

## **2.2 Geologic Structures**

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The major geologic structures (faults and folds) in the project area, taken from DNR regional geologic mapping, are identified on Figure 1 and the cross sections (Figures 2 and 3). The geologic structures, along with topography (incised canyons) described above, have a substantial effect on the groundwater flow regime within the study area.

Regional north-south compression of the earth's crust that began during the deposition of the Grand Ronde basalt approximately 16 million years ago created the regionally extensive southwest-northeast trending Yakima Fold Belt, which includes the Columbia Hills ridge on the southern edge of the study area (Reidel et al., 1989). This compression resulted in the formation of the numerous southwest-northeast trending folds (synclines [troughs] and anticlines [ridges]) and the associated reverse and thrust faults (older rocks are slid upward over younger rocks) found in the region including the study area. The Columbia Hills thrust fault, with several hundred feet of low-angle vertical displacement, is likely associated with the formation of the Columbia Hills. The several southwest-northeast trending geologic structures across the study area are shown on Figure 1.

Superimposed upon the major southwest-northeast trending structures within the study area are numerous northwest-southeast trending normal faults (younger rocks are slid downward over older rocks) and strike-slip faults (rocks are slid laterally past each other), likely created from a rotational component of the same north-south compression that resulted in the southwest-northeast trending structures (Reidel et al., 1989).

In the subsurface, folds and faults may represent partial or complete barriers to lateral groundwater flow, laterally compartmentalizing flow within the study area. Newcomb (1969) theorized that tight anticlinal folding of basalt forms breccia (broken rock) and fine-grained fault gouge between the individual flows near the axis of an anticline, which decreases the transmissivity of the basalt and impedes groundwater flow across the anticlinal crest. In addition, due to the folding and upwarping of the individual flows in the creation of the anticlinal crest, higher heads are needed for groundwater to flow over this crest. If significant vertical displacement occurs across faults to offset the water-bearing interflow zones, the faults may act as impermeable barriers to lateral groundwater flow. Fault gouge may also decrease the permeability of the interflow zones in the vicinity of faults including strike-slip faults where horizontal displacement occurs. The Warwick Fault (strike-slip), cutting across the northeast corner of High Prairie (Figure 1), is documented to be a barrier to lateral groundwater flow in the basalt aquifer system to the east of it within Swale Valley.

## 2.3 Groundwater Recharge

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As described above, the isolation of the High Prairie area by deep canyons and geologic structures limits lateral groundwater movement to replenish groundwater withdrawn by pumping. Therefore, the source of groundwater to the basalt aquifers is largely limited to vertical recharge within the footprint of High Prairie. Recharge of basalt aquifer systems may occur where interflow zones exposed at the surface or where covered only by thin units, and/or through open fractures/faults. Recharge water can move downward to deeper aquifer zones via fractures/faults with vertical permeability and/or where lower-permeability zones pinch out depositionally or from prior erosion or tectonic offset.

Relying on estimates from a prior USGS regional hydrologic modeling assessment (Bauer and Vaccaro, 1990), Aspect (2011) estimated an average recharge rate of 7.5 inches per year, or 22,250 acre-feet per year, across the entire High Prairie study area. The recharge occurs predominantly to the shallowest aquifer zones; however, there is a strong downward vertical gradient between aquifer zones in the High Prairie area (described below), which can allow the shallower aquifer zones to gradually recharge deeper zones.

While there has not been a detailed assessment of differences in recharge to the various aquifer zones of High Prairie, groundwater quality analyses were performed as part of this assessment to estimate the age of groundwater withdrawn from shallower versus deeper wells as an indirect means to evaluate groundwater recharge from shallower to deeper aquifer zones. The groundwater quality investigation is described below in Section 5.1.

## 2.4 Groundwater Flow

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In general, groundwater in the basalt aquifer system is expected to flow regionally away from anticlinal axes, in the direction of regional geologic dip of the basalt flows, and towards major surface water bodies (Steinkampf, 1989). During the formation of an anticline, the compression of the various basalt flows leads to both the folding and uplift of the respective flows. Erosion of the upper flows exposes the lower flows at the surface, thus allowing for the areal recharge of the respective flow. For this reason, groundwater

generally flows away from these topographically higher points of recharge and down the geologic dip.

Aspect (2011) mapped groundwater elevations and thus inferred lateral groundwater flow directions for the collective Wanapum basalt aquifer system beneath High Prairie. While there is variability in the measured groundwater elevations across the entire area, the mapping indicates the highest groundwater elevations generally occur in the area near Laurel Fault (Figure 1) and along the southern portion of Schilling Road east of it (topographically higher area which is also a surface water divide). The groundwater elevation data indicate that groundwater in the Wanapum basalt west of Laurel Fault flows to the southwest towards the Klickitat River. East of Laurel Fault, there appears to be a groundwater divide along the western extension of the Horseshoe Bend anticline: north of the anticline groundwater flows to the north-northwest towards Wheeler Canyon and south of the anticline, it flows to the south-southeast towards Swale Creek canyon. While a regional groundwater flow regime was defined from the groundwater elevation mapping, the numerous geologic structures across the area can impede flow and create highly complex flow regime on the local scale.

The water level data from wells completed in vertically distinct aquifer zones indicate a consistent downward vertical gradient across High Prairie – i.e., the groundwater levels of the wells completed in the upper zones are higher than the groundwater levels of the wells completed in the lower zones. Based on the cross sections (Figures 2 and 3), groundwater levels (heads) are in the range of 200 to 400 feet lower in the deeper Grande Ronde basalt than in the shallower Wanapum basalt. The layered nature of the basalts, with thin permeable interflow zones (aquifer zones) separated vertically by thick layers of low permeability massive basalt (aquitards restricting flow), allows the large head differences between shallower and deeper zones to persist. If the aquitard layers were not present, the heads in shallower and deeper aquifer zones would equilibrate and vertical gradients would not exist.

### 3 Groundwater Level Trends Over Time

In 2007, the High Prairie well network was established with 14 wells for water level measurements. In 2010, the network was expanded to 23 wells. Water level measurements have typically been collected twice per year, in the spring and fall. In spring 2015, seven additional wells, including several wells in the deeper aquifer, were added to the network. Table 1 provides information for the current well network; all of the wells monitored to date are included, although some wells are no longer participating. The 23 wells monitored since 2010 were professionally surveyed by County staff (location and wellhead elevation); the wells added in spring 2015 are not yet surveyed. Table 2 provides the water level data collected from the network wells from 2007 through spring 2015. To date, 17 rounds of water level measurements have been collected from the High Prairie well network.

Based on the well network measurements over the past 5 to 8 years, water levels are generally stable in 20 of 23 wells covering the majority of High Prairie. This is illustrated

visually by the groundwater hydrographs (groundwater elevations versus time) representing the long-term water level measurements (Figure 4).

As noted on Figure 4 and in prior reports, three wells with documented water level declines include wells T03/R13-20N1<sup>3</sup>, T03/R13-22C1, and T03/R13-22P1, all located in the Knight-Dillacort area. Wells -22C1 and -22P1 are located within roughly ¼ mile of each other in the eastern portion of the Knight-Dillacort area, whereas well -20N1 is located toward the western side of the area (Figure 1).

On the west end of the area, well T3/R13-20N1 (520 feet deep) showed a water level decline on the order of 40 feet from the start of its monitoring in summer 2010 until spring 2012, but since then has shown more than 15 feet of water level rise as of spring 2015 (Figure 4). Discussions with the owner of well -20N1 indicates they have been actively conserving water and managing their pumping schedule so as to accommodate a well of limited yield. The adjacent well T3/R13-20N2 (530 feet deep) showed a decline on the order of 30 feet between the first two measurements (winter 2010 and winter 2011), but since then has exhibited water level rise on the order of 70 feet, far surpassing the first (winter 2010) measured water level elevation (Figure 4).

Based on the measured data, the -20N1 and -20N2 wells do not demonstrate ongoing water level declines in the western portion of the Knight-Dillacort area.

Conversely, water level continue to decline in the eastern end of the Knight-Dillacort area as of the spring 2015 measurements. In that area, wells -22C1 and -22P1 showed stable water levels between 2007 (start of monitoring) and spring 2009. Since then, water level declines on the order of 57 and 39 feet, respectively, have been measured from spring 2009 through spring 2015 with no indication of trend reversal (Table 2). In 2014, the High Prairie Community Council (2014) reported that a cluster of wells in this same general area was experiencing severely declining water levels, and that several had deepened their wells as a result.

Figure 5 illustrates in pink the parcels where water level declines have been reported – either measured in the aforementioned network wells highlighted on the figure or by anecdotal information from the local community. Parcels where wells have been deepened since 2010, based on Ecology’s well log records, are outlined in red on Figure 5.

Other wells within the Knight-Dillacort area do not show water level declines based on the available data, namely wells T03/R13-21M1, -27, -27Q1, -28B1, and -28L1 (Figure 4; Figure 5). Of these wells, well -21M1 is 520 feet deep and the others range in depth from 90 to 310 feet (Table 2). Wells -27 and -27Q1 are located south of the Columbia Hills thrust fault (Figure 1) and are likely hydraulically isolated from the basalt aquifer to the north where the declines are occurring.

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<sup>3</sup> The local well number designations used are based on location information (quarter-quarter section) in Ecology’s online well log database and may not be accurate. Locations of wells in the monitoring network have been surveyed and are accurate on the maps.

Figure 6 presents a pair of hydrographs illustrating the measured water level declines in wells -22C1 and -22P1. Based on the measurements collected twice per year, well -22C1 has experienced a decline of approximately 57 feet between 2009 and 2015, whereas well -22P1, located to the north, experienced a decline of approximately 39 feet in the same time period. As stated above, both wells showed generally stable water levels from their start of monitoring in 2007 through spring 2009. Well -22C1 initially showed a 13-foot decline between the spring and fall 2009 monitoring events, whereas well -22P1 showed a smaller initial decline (4 feet) between fall 2009 and spring 2010 measurements. Both wells show an accelerated rate of decline over time, as noted on Figure 6:

- At well -22C1, a 23-foot decline was measured in the 3-year period between 2009 and 2012 (7.9 feet/year) followed by a 33-foot decline in the 3-year period between 2012 and 2015 (11.0 feet/year).
- At well -22P1, a 13-foot decline was measured in the 5-year period between 2009 and 2014 (2.5 feet/year) followed by a 26-foot decline in the 1-year period between 2014 and 2015 (26 feet/year).

Based on the collective information available, we conclude that large ongoing water level declines are localized to the shallow aquifer in the eastern portion of the Knight-Dillacort area as documented by wells -22C1 and -22P1 located within approximately ¼ mile of each other; therefore, that area has been the focus of this assessment. The following section evaluates potential causes of the observed declines in the eastern portion of the Knight-Dillacort area.

## 4 Assessment of Causes for Water Level Declines

As outlined in Section 2, the topographic incisement and numerous regional geologic structures combine to have a substantial effect on the groundwater flow regime within the High Prairie area including the Knight-Dillacort area. High Prairie as a whole is incised on three sides (east, north, and west) by the Swale Creek and Klickitat River canyons, and it is bounded on the south by the collection of large-scale geologic structures forming the Columbia Hills. Superimposed on this isolated upland are numerous geologic structures that cut across the area, as depicted on Figure 1. The Knight-Dillacort area is further constrained by Knight Canyon and Dillacort Canyon on the southwest and northeast, respectively. The topographic canyons incise through the shallower aquifer zones, whereas it is believed that the regional geologic structures penetrate and form hydraulic barriers through the entire CRBG sequence. This combination of naturally occurring features can create compartmentalized blocks of basalt aquifer with limited lateral continuity, which, in turn, limits lateral flow of groundwater to replenish groundwater withdrawn by pumping within an aquifer block.

In short, the hydrogeologic setting of High Prairie makes it sensitive to overpumping (overdraft) of the groundwater resource.

Despite that, the available data indicate that groundwater levels across most of High Prairie appear stable across the 8-year period of monitoring in the well network (Figure

4), indicating that the current level of pumping across most of the area is sustainable. The substantial ongoing declines in groundwater levels observed over the past 6 years are limited to the shallow aquifer within the eastern portion of the Knight-Dillacort area. Possible causes for these localized declines include changes to precipitation and/or changes to groundwater withdrawals from the shallow aquifer resulting from numbers of wells constructed or deepened. Each possibility is examined below.

## 4.1 Precipitation Changes (Climate Change)

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Trends in precipitation (and thus recharge) over the past 6 years relative to prior conditions are evaluated by review of annual precipitation data from the National Oceanic and Atmospheric Administration (NOAA) Weather Observation Stations in Goldendale (Station Nos. 453222 and 453226). Based on location, elevation, and surrounding topography, the Goldendale stations are assumed to be the most representative of the actual precipitation for the Knight-Dillacort study area. While the magnitude of precipitation at Goldendale will be different from High Prairie, the trends over time (above or below normal) should be similar.

The upper plot on Figure 7 presents both the annual precipitation and the calculated 16.9-inch mean annual precipitation at Goldendale for the 83-year period of record (1931 through 2014), excluding several years for which much data are missing. In addition, a cumulative departure from the mean annual precipitation is presented in the lower plot on Figure 7. The cumulative departure analysis adds the inches above or below the average precipitation for each year into a running total, and thereby illustrates longer-term drought or wet periods. While the values of the cumulative departure (i.e. numbers on the y-axis) depend on the year the analysis is started, the trend of above- or below-normal (shape of the curve) does not depend on the year started.

The annual precipitation data indicate that while there is substantial inter-annual variability in precipitation over the period of record, the long-term trend is generally stable. Since 2009, precipitation has been within a few inches of normal with the exception of 2013 which was 6.8 inches below normal. If precipitation were a causal factor, we would expect to see water level declines across all of High Prairie, which is not the case as described above.

Based on the information, we conclude that changes in precipitation are not a cause of the localized water level declines observed in the eastern Knight-Dillacort area.

## 4.2 Well Construction and Deepening in Area

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The Knight-Dillacort area generally has a higher population density and thus higher well density than other areas of High Prairie. Figure 8 graphically depicts the numbers of wells by quarter-quarter section within and around the Knight-Dillacort area, based on records in Ecology's online well log database as of early 2015.

While there are many wells reported in and around the area of documented water level declines (around Adams View Road), there is an equal or greater density of wells reported in areas just to the west and southwest, where there is no indication of long-term declines from either monitoring data or anecdotal information from the community (see

Figure 5). Based on this information, the number (density) of wells by itself does not correlate with the location of documented water level declines.

There are no known significant changes in water use within the eastern Knight-Dillacort area corresponding in time to the observed declines (since 2009). However, there has been a steady increase in numbers of wells installed in the area, and an increase in the numbers of wells deepened to seek a more reliable source of water. These factors are evaluated below.

#### **4.2.1 Well Installations Over Time**

As illustrated on Figure 8, there are numerous wells installed within the Knight-Dillacort area and, based on Ecology's well log records, wells in the area have been installed consistently over the past few decades. Figure 9 depicts the numbers of wells installed per year between 1970 and 2014 within the 4-section area encompassing the eastern Knight-Dillacort area (Sections 21, 22, 27, and 28 of Township 3 North Range 13 East); the cumulative number of wells installed over time is also shown as the red line. The number of wells installed per year are plotted relative to the y-axis on the left side of the plot (0 to 7), whereas the cumulative number of wells installed since 1970 are plotted relative to the y-axis on the right side of the plot (0 to 70).

Ecology's records indicate that 70 wells have been installed in the 4-section area since 1970, with 0 to 3 wells installed during most years and 5 or more wells installed during a few years. This pattern is the same during the years of 2007 through 2014 (0 to 3 wells per year), so there is no indication of increased numbers of new wells in the area during the time period of measured water level declines.

If cumulative withdrawal of groundwater from increasing numbers of wells in the area were a cause of water level declines, we would expect declines to be a more widespread phenomenon across the entire 4-section area. Instead, the declines appear to be highly localized as described above.

Based on the distribution and timing of the measured water level declines relative to well installations, the total number of wells in the area does not appear to be a cause of the observed declines.

#### **4.2.2 Deepening of Wells Over Time**

Figure 5 depicts the parcels within the Knight-Dillacort area where wells have been reportedly been deepened since 2010. All of the well deepening occur in the eastern area where the water level declines are measured.

Based on Ecology's well log database, Figure 10 depicts the numbers of wells deepened per year between 1970 and 2014 within the same four Sections 21, 22, 27, and 28 of Township 3 North Range 13 East; the cumulative number of wells deepened over time is also shown as the red line. The number of wells deepened per year are plotted relative to the y-axis on the left side of the plot (0 to 5), whereas the cumulative number of wells deepened since 1970 are plotted relative to the y-axis on the right side of the plot (0 to 10).

Ecology's records indicate that ten wells have been deepened in the 4-section area since 1970: none during the 1970s, one during the 1980s, two during the 1990s, one during the 2000s, and six during the 2010s with 4 of those 6 occurring in 2014 (Figure 10).

There is a strong spatial correlation between locations of recent (since 2010) well deepenings and locations of shallow aquifer wells showing recent water level declines in the eastern Knight-Dillacort area (Figure 5). There is also a strong correlation between timing of the recent well deepenings and timing of the water level declines in that area as measured at network wells -22C1 and -22P1, as illustrated on Figure 11. The fact that well -22C1 is located closer to the deepened wells and showed an earlier onset and greater magnitude of water level decline, relative to well -22P1 (Figure 10), further strengthens the recent well deepenings as a cause for the declines.

As discussed in Section 2, there is a strong downward hydraulic gradient (a few hundred feet of head difference) between shallower and deeper aquifer zones throughout High Prairie including the Knight-Dillacort area. Therefore, there is a driving hydraulic force for groundwater to naturally move downward from shallower to deeper aquifer zones. However, the thick layers of low-permeability massive basalt (aquitards) vertically separating the basalt interflow aquifer zones greatly restrict downward movement of groundwater. If not for that vertical permeability restriction, the heads in the various aquifer zones would equilibrate, eliminating vertical gradients.

When a borehole is drilled through the basalt aquitard layers without sealing off the interflow (aquifer) zones it creates a permeable conduit for groundwater to move downward from shallower to deeper aquifer zones. Appendix B presents well logs for the 21 wells in Ecology's database that were installed to depths of 400 feet or greater within Sections 21, 22, 27, and 28 of Township 3 North Range 13 East; this includes wells drilled to that depth initially and formerly shallow wells that were deepened. Based on our review of the recorded well construction information, only one of the 21 deeper wells in the area documents sealing off of shallower aquifer zones. Several of the wells have liners installed, but the liners are designed only to prevent borehole collapse; they do not seal tightly against the borehole<sup>4</sup> so they do not prevent vertical water movement in the annular space outside of them. The one deeper well where sealing off of a shallower aquifer zone is documented on the well log, is located in the SW $\frac{1}{4}$  of the NE $\frac{1}{4}$  of Section 27 (well 27G, not in the monitoring network); this well was deepened from a depth of 330 to 680 feet in 2014 (formation had caved in between depths of 280 and 330 feet prior to deepening). The well log documents the presence of cascading water at a depth of 290 feet, which was sealed off using a shale trap with bentonite grout installed between the liner and borehole wall.

The cumulative effect of several wells drilled into deep aquifer zones without sealing off shallow aquifer zones can be a gradual draining of the shallow aquifer zone(s) into the deeper aquifer zone(s). Based on the collective available information described above, we conclude that this phenomenon is the primary reason for the localized water level declines in the shallow aquifer of the eastern Knight-Dillacort area.

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<sup>4</sup> Liner is typically 4.5-inch-diameter light-gage steel casing within a 6-inch borehole.

## 5 Assessment of Deeper Aquifer Zones in Study Area

In light of the substantial water level declines in the shallower aquifer system of the eastern Knight-Dillacort area, and the fact that several wells had been deepened in the past few years, a primary point of interest from the December 2014 meeting of High Prairie residents was the viability of the deeper aquifer system as a water supply source. Little information is available regarding the deeper aquifer zones, including no data regarding their water level trends, in the general area of the observed shallow aquifer declines. Of the seven wells added to the well monitoring network in 2015 as part of this assessment, four are greater than 400 feet deep (Table 1), so future monitoring of local water level trends in the deeper aquifer zones can be conducted.

The following subsections present data from groundwater quality testing conducted as one means to assess recharge to the deeper aquifer zone, followed by a discussion of the available information regarding reported well yields in the study area.

### 5.1 Groundwater Quality Testing to Assess Groundwater Age and thus Recharge

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As stated in Section 2.3, groundwater quality analyses were performed as part of this assessment to estimate the age of groundwater withdrawn from shallower versus deeper wells as an indirect means to evaluate groundwater recharge from shallower to deeper aquifer zones.

In April 2015, Aspect received owner permission and collected groundwater samples from six wells located in the eastern part of the Knight-Dillacort area where water level declines are documented (discussed above). An attempt was made to select both shallower and deeper wells for comparative analysis of groundwater quality between shallower and deeper aquifer zones in the immediate area. As depicted on Figure 12, the four shallower wells sampled were -22P1 (280 feet deep), -27A2 (220 feet deep), -27C1 (168 feet deep), and -28B1 (220 feet deep), and the two deeper wells sampled were -27D4 (634 feet deep) and -27D6 (410 feet deep).

Aliquots of the six groundwater samples were submitted to Analytical Resources Inc. (ARI) of Seattle, Washington, for analysis of conventional water quality parameters including common cations (calcium, magnesium, potassium, and sodium), common anions (bicarbonate [alkalinity], chloride, and sulfate), fluoride, nitrate, and silicon. In addition, an aliquot of each sample was submitted to Beta Analytic Inc. of Miami, Florida, for radiocarbon (Carbon-14 isotope) dating analysis.

The following subsections describe the information and interpretation regarding conventional water quality parameters and for the radiocarbon dating. The groundwater analytical data are presented in Table 3, which also lists the depth of wells sampled. Appendix A includes the laboratory reports for the two data sets (conventionals and radiocarbon dating).

### 5.1.1 Conventional Water Quality Parameter Data

CRBG groundwater chemistry evolves with greater residence time in the aquifer. In very general terms, recently recharged groundwater is typically dominated by calcium (Ca) and magnesium (Mg) cations and the bicarbonate anion ( $\text{HCO}_3$ ) – i.e., a Ca-Mg- $\text{HCO}_3$  type water. As groundwater moves along its regional flow path, spending greater time in contact with the basalt matrix, dissolution and hydrolysis of selected minerals and precipitation of other secondary minerals (e.g. clays) within the basalt matrix commonly remove calcium and magnesium in exchange for sodium, resulting in higher sodium concentrations in solution. The water-rock reactions also precipitate from solution into the basalt matrix carbonate, silica, and potassium (K), and can release from the basalt matrix into solution chloride, fluoride, and hydroxyl (thus raising groundwater pH). With very long residence times, the oldest CRBG groundwaters can therefore evolve to an oxygen-depleted, alkaline, sodium chloride (Na-Cl) type water with elevated fluoride concentrations (Hearn et al, 1990; Riedel et al, 2002; CBGWMA, 2009b).

Detected fluoride concentrations were the same (0.2 mg/L) in five of six wells sampled, thus no trend with well depth is apparent; the detected fluoride concentrations are an order of magnitude below the 4.0 mg/L drinking water standard. The field-measured groundwater pH was comparable for the six wells (7.0 to 8.2, neutral to slightly alkaline), also without any apparent correlation to well depth (Table 3).

Figure 13 is a “Piper plot” graphically depicting the common ion (cation and anion) data for the six water samples. The shallower wells (< 300 feet deep) and deeper wells (> 400 feet deep) are depicted with different colored symbols on the figure. The lower left triangle on the Piper plot displays the relative proportion of each major cation (Ca, Mg, K, Na), and the lower right triangle displays the relative proportion of each major anion ( $\text{HCO}_3$ , Cl, and sulfate ( $\text{SO}_4$ ))<sup>5</sup> in the samples. The position of the samples’ cation and anion proportions are then projected onto the upper diamond-shaped plot as a means to represent the major ion composition (combined cations and anions) for each sample as a single point. Differences in major ion composition would be expected for younger versus older groundwaters as outlined above (e.g., evolution from a predominantly Ca-Mg water type to a predominantly Na water type). If deeper wells represent older (more chemically evolved) groundwaters, samples from the deeper wells would be expected to cluster toward the lowermost corner of the upper diamond of the Piper plot.

As indicated on Figure 13, a trend in groundwater composition (major ions) is not apparent from the Piper plot. All of the samples represent a Ca-Mg-dominant water type, which suggests relatively little water-rock interaction.

Another approach to assess the major ion data is the cation ratio, which is calculated as the sum of sodium and potassium concentrations divided by the sum of the four major cation concentrations (i.e.,  $[\text{Na}+\text{K}]/[\text{Na}+\text{K}+\text{Ca}+\text{Mg}]$ ). In theory, groundwaters with greater residence time in basalt aquifers should be more Na-rich and therefore have

<sup>5</sup> The plot includes  $\text{HCO}_3$  plus carbonate ( $\text{CO}_3$ ) on one axis; however,  $\text{CO}_3$  is essentially absent in the samples (Table 3) so only the  $\text{HCO}_3$  is relevant.

higher cation ratios (CBGWMA, 2009b). If greater well depth equates to older and more geochemically evolved groundwater, cation ratio would increase with well depth.

The upper plot on Figure 14, depicting cation ratio as a function of well depth for the six samples, does not indicate that trend. In fact, the five wells excluding the deepest (-27D4, 634 feet deep) suggest the opposite trend – cation ratio generally decreasing with depth – with the most geochemically evolved groundwater being in the 220-foot-deep well -28B1. The deepest well -27D4 is a clear outlier from the other data (much lower cation ratio than expected). We infer that, because the two deeper well (-27D4 and -27D6) boreholes are open to shallower and deeper aquifer zones<sup>6</sup>, the water sampled from those wells represents a mixture of groundwater from shallow and deeper aquifer zones.

As stated above, silica<sup>7</sup> concentrations in CRBG groundwater can decrease with greater residence time as a result of silica being incorporated into secondary minerals, thus removed from groundwater. The lower plot on Figure 14, depicting silicon concentrations as a function of well depth, follows that trend for five of the six wells. The deepest well (-27D4) is again an outlier from the other samples (much higher silicon concentration than expected), which, again, is inferred to reflect a mixed groundwater quality. There is no drinking water standard for silicon.

In theory, higher chloride concentrations are indicative of an older (geochemically evolved) groundwater, as stated above. The six samples do not show a clear trend of chloride concentrations versus well depth (upper plot on Figure 15). The 220-foot-deep well -28B1 had the highest detected chloride concentration (13.1 mg/L), like it had the highest cation ratio. Detected chloride concentrations in the other five wells are similar (2.5 to 4.6 mg/L), with no clear correlation to well depth. The detected chloride concentrations are an order of magnitude below the 250 mg/L secondary drinking water standard based on aesthetics (taste).

Nitrate is typically associated with surface processes (including fertilizers and septic systems), therefore higher nitrate concentrations would be expected in groundwater from shallower aquifers. The lower plot on Figure 15 depicts the six wells' nitrate concentrations as a function of well depth, which may indicate that trend generally but not clearly. Nitrate was not detected (< 0.1 mg/L) in samples from wells -22P1 (280 feet deep) and -27D6 (410 feet deep). The detected nitrate concentrations in the other four wells ranged from 0.2 to 1.0 mg/L, with all being an order of magnitude below the 10 mg/L drinking water standard. The highest nitrate concentration was detected in well -28B1, which also had the anomalously high chloride detection (described above) and the highest measured water temperature (13.9° C; Table 3). Well -27C1 (168 feet deep) had the second highest detected concentrations of both nitrate (0.9 mg/L) and chloride (4.6 mg/L) (Table 3). High nitrate in combination with high chloride can be indicative of septic system effluent; however, radiocarbon dating data indicates that groundwater from

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<sup>6</sup> Well -27D4 (634 feet deep) has a 4.5-inch-diameter liner extending to 350 feet, but the liner does not seal off the nominal 6-inch borehole in which it is set.

<sup>7</sup> Silica refers to a combination of silicon and oxygen (e.g. quartz), but the laboratory analyzes for the element silicon.

that well is a few thousand years old, thus precluding septic as a cause (discussed below in Section 5.1.2).

In summary, the water quality data from shallower versus deeper wells do not demonstrate the patterns of water quality change that are observed regionally in the CRBG, where deeper wells tap into older and thus more geochemically evolved groundwater. We expect that is largely due to the fact that the two deeper wells sampled in the study area are open across both shallower and deeper aquifer zones, so their samples likely reflect a blend of groundwater quality from the various zones.

### **5.1.2 Radiocarbon Age Dating**

The six groundwater samples were submitted for radiocarbon age dating, which is commonly used to estimate the age of carbon-containing materials that are less than approximately 50,000 years old. Radiocarbon, or carbon-14, is an unstable isotope of carbon that is naturally produced in the atmosphere and converts to the stable carbon-12 and/or carbon-13 isotopes over time, with a half-life of approximately 5,730 years. The analytical method determines the proportion of unstable carbon-14 to stable carbon-12 or carbon-13 isotopes and estimates the age based on comparison of the measured isotope ratios to reference samples (the older the sample, the less carbon-14 will remain). Inorganic carbon present in the groundwater samples is the material dated for this assessment. Radiocarbon dates are rounded by the laboratory to the nearest 10 years per the conventions of the 1977 International Radiocarbon Conference. Table 3 presents for each sample the measured fraction of carbon-14 (“modern carbon”) with the reported error range (+/-), and the resulting estimated radiocarbon age and error range in years. The upper plot on Figure 16 presents the estimated radiocarbon ages as function of well depth.

As presented in Table 3 and Figure 16, the estimated age of the groundwater sampled from the six wells ranges from approximately 3,560 to 7,570 years. In other words, all of the groundwater sampled in this assessment is older than 3,500 years. Samples from five of the six wells show a general trend of increasing age with increasing well depth, but the deepest well (-27D4, 634 feet deep) is an outlier to that trend, like it is an outlier for other geochemical indicators as discussed above. Mixing of groundwater from shallower and deeper aquifer zones is a likely explanation for that outlier result.

This range of age values is consistent with measurements of groundwater age within the CRBG elsewhere in the Columbia Basin (ranging from a few thousand to several tens of thousands of years; Douglas et al, 2007; CBGWMA, 2009). The age data indicate relatively long flow paths, and thus residence times, for recharge water to reach the aquifer zones being tapped for water supply by these wells. Note that the estimated 5,920-year age for groundwater from well -28B1 indicates that that well’s elevated nitrate and chloride concentrations are not attributable to septic systems (generated near surface in past decade), as was mentioned above as a possibility.

The lower plot on Figure 16 presents cation ratio as a function of radiocarbon age, with the expectation that older groundwater (longer residence time) should have a greater cation ratio. The sample data do not show that trend. In fact, the opposite trend is

generally indicated for five of six wells (including deepest well -27D4), but with well -28B1 being an outlier relative to the other five wells.

## 5.2 Reported Well Yields

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Driller's logs commonly present information on well yield (gallons per minute [gpm]) as measured from the driller's air lift well development conducted on newly installed or deepened wells. Air lifting is conducted primarily to remove from the well accumulated sediment and turbid water generated during drilling. The air lifting is commonly conducted for time periods of 1 to 4 hours and the reported information on flow rate may not be accurate nor representative of a well's true yield since it is short term and it is controlled by the air pressure generated by the driller's air compressor. A permanent pump placed in the well may yield lesser or greater quantities of groundwater than the rate reported on the driller's log. Nevertheless, in the absence of more reliable data, the yield data reported on the drillers' logs is readily available information from nearly all of the wells in the study area, so is worth evaluating for general patterns with respect to both geographic location and well depth (aquifer zone).

The yield of a well is controlled both by the transmissivity of the aquifer zone(s) adjacent to the well and the available drawdown<sup>8</sup> within the well, the latter being a function largely of the artesian pressure within the aquifer zone(s) supplying the well. The depth at which the pump is set is also a factor in well yield, but that is not a function of the aquifer productivity or well construction and it is not typically reported on driller's logs, so is not considered in this evaluation.

The upper plot on Figure 17 plots the depth to water reported at time of drilling (on driller's log) versus the well total depth for all wells in the 4-section area encompassing the eastern Knight-Dillacort area (Sections 21, 22, 27, 28 of T03N/R13E). The data show a clear pattern of deeper static water levels with increasing well depth. Shallower static water levels could occur in deeper wells if the deeper aquifer zones tapped by the deeper wells had great excess pressure (artesian pressure). The data indicate that such highly pressurized deep aquifer zones are not present to the depths of drilling (approximately 700 feet) within the study area.

The lower plot on Figure 17 presents the wells' available drawdown as a function of well depth. While there is considerable variability among wells, there is an overall pattern of greater available drawdown with greater well depth. However, the general trend of the data is considerably less than a 1:1 slope; in other words, for the majority of wells, drilling an extra X feet in well depth does not return the same X feet in available drawdown. Nevertheless, the generally greater available drawdown afforded by deeper wells overall suggests that somewhat greater yields should be available in deeper wells in the study area, if deeper aquifer zones are equally transmissive to shallow aquifer zones, which is not known.

While there is in general somewhat greater available drawdown in deeper wells of the study area, the reported well yields do not show a clear trend with well depth. The upper plot on Figure 18 presents the reported well yields as a function of well depth, which

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<sup>8</sup> The length of water column within the well (static water level depth minus well depth).

demonstrates considerable variability with no clear trend overall. Because well depth is a function of the ground surface elevation that the well is drilled from (to reach a specific aquifer zone), the lower plot on Figure 18 presents the same reported well yields as a function of the elevations of the well bottoms, which normalizes changes in ground surface elevation; there is no clear trend of reported yield versus the well's bottom elevation. As stated above, the well yields reported on driller's logs may not be representative of yields that the wells would produce with a permanent pump installed.

While the existing information on well yields is of limited reliability, it does not indicate that deeper aquifer zone(s) beneath the study area are more productive (higher yielding) than the shallower aquifer zones.

Figure 19 presents the reported well yield data in plan view for the 4-section area, without consideration of well depth. Listed for each quarter-quarter section are the number of reported wells and the minimum, average, and maximum reported well yields for those wells. Each quarter-quarter section is color coded based on the maximum reported yield. Notwithstanding the caveats on reliability of the yield data reported on driller's logs, the available data indicate an area with yields of 100 gpm or higher in the northern quarter-quarter sections of Sections 27 and 28. Review of the well log information also indicates no correlation between the reported yields of the wells and the years they were installed (Figure 20).

## 6 Conclusions and Recommendations

Although the natural hydrogeologic setting of High Prairie limits recharge to the groundwater aquifers and thus makes the area sensitive to groundwater depletion from overpumping, water level monitoring conducted since 2010 or earlier indicates that groundwater levels are generally stable over time across the vast majority of High Prairie. However, within a localized eastern portion of the Knight-Dillacort area, near Adams View Road, substantial and ongoing declines in water levels have been measured in two wells since 2009, and the rates of declines have accelerated in the past few years.

The observed water level declines do not appear to be related to the increased total number of wells in the area. Rather, based on multiple lines of evidence, the accelerating declines appear to be related to recent deepening of several wells in the immediate area of the declining wells. During the deepening process, the shallow aquifer zone(s) do not appear to have been sealed off to prevent vertical movement of water (cascading water) from the shallow aquifer zone(s) within the deepened well. Consequently, it appears that the deepened wells have been gradually draining groundwater from the shallow aquifer zone(s) in which the declining wells are completed.

Little information is currently available regarding the deeper aquifer system within the eastern Knight-Dillacort area, but deeper wells in the area were added to the well monitoring network as part of this assessment so monitoring for water level trends can continue into the future. There is no consistent evidence that the local deeper aquifer zone is more productive than the shallower aquifer zones.

Based on these conclusions, we provide the following recommendations:

- Retrofit the deepened wells in the area of declines to seal off the shallower aquifer zones and prevent cascading water. We expect that this would not create a rapid recovery of the declines that have already occurred, but it should curb further declines in affected wells and limit expansion of the area of decline.
- Continue the High Prairie water level monitoring program with regular evaluation of the data to watch for changes in groundwater levels over time. The value of the monitoring program is evident by now having the data that document the localized groundwater declines and provide a basis to diagnose their cause. We recommend that additional wells be added to the network, as practical, to provide greater coverage of areas lacking monitoring, and, where possible, to monitor water levels in shallower and deeper aquifer zones.
- Implement voluntary water conservation measures throughout High Prairie, particularly limiting outdoor water use.

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## Limitations

Work for this project was performed for the Klickitat County Department of Natural Resources (Client), and this report was prepared in accordance with generally accepted professional practices for the nature and conditions of work completed in the same or similar localities, at the time the work was performed. This report does not represent a legal opinion. No other warranty, expressed or implied, is made.

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# **TABLES**

**Table 1 - Groundwater Level Monitoring Network for High Prairie**

Hydrogeologic Assessment Knight-Dillacort Area

Ecology Well Log Data				Well Survey Data			
TRS Label	Well Log Date	Dia. (in)	Depth (ft)	Northing <sup>1</sup> (SPS 83; ft)	Easting <sup>1</sup> (SPS 83; ft)	Top of Casing Elevation <sup>2</sup> (NAVD 88; ft)	Comments as of Spring 2015
<b>Wells in Original Monitoring Network</b>							
T03/R13-3B1	11/12/86	6	76	162902.9	1472929.6	2011.17	
T03/R13-3R1	4/15/87	6	745	159389.4	1472760.9	2146.99	No longer monitored due to numerous obstructions in the well.
T03/R13-4L1	10/25/95	6	620	160519.0	1464962.0	2126.25	
T03/R13-11M1	8/31/94	6	524	155087.0	1474093.1	2037.44	
T03/R13-14A1	10/16/92	6	500	152621.1	1478289.8	2181.16	
T03/R13-14G1	7/7/95	6	500	151451.4	1476350.7	2085.99	
T03/R13-14G2	2/28/07	6	458	151661.4	1476308.2	2082.02	
T03/R13-14J	5/30/90	6	460	149010.8	1477037.7	2000.84	Located under bird house. Owner does not have well log. Well log chosen based on water level. Limited access, remove expansion bolt.
T03/R13-15L1	8/13/87	6	105	149748.7	1470418.5	1885	Airline installed to unknown depth. GPS Location; Google Earth elevation.
T03/R13-20N1	11/22/94	6	520	144704.4	1457869.5	1452.74	Airline installed at approximate depth of 520 ft.
T03/R13-20N2	7/15/04	6	530	144430.9	1458080.8	1427.90	Well Tag: AKL-875
T03/R13-21M1	7/11/97	6	520	145315.8	1463014.1	1745.30	Sonic water level indicator not accurate.
T03/R13-21P1	5/6/94	6	200	139938.4	1465005.9	1569.93	
T03/R13-22C1	5/9/02	6	225	143235.9	1470655.1	1777.48	
T03/R13-22P1	10/19/95	6	280	144550.2	1470944.8	1763.36	
T03/R13-23L1	5/30/81	6	449	145104.1	1475387.6	1808.08	Originally had an airline installed at depth of 140 ft. Access port later installed (May/June 2010).
T03/R13-27	8/7/08	6	165	140168.2	1469338.5	1747.10	Well Tag: APT-283
T03/R13-27Q1	10/27/93	6	310	138228.3	1471376.8	1996.03	
T03/R13-28B1	9/7/94	6	220	143022.4	1466216.1	1622.75	
T03/R13-28F1	11/4/03	6	335	140751.7	1464326.2	1527.26	Well Tag: AHK-331 2 wells; well not currently in use is monitored.
T03/R13-28L1	12/27/72	8	90	141586.1	1465563.3	1498.67	
T03/R14-18N1	5/20/97	6	695	149041.9	1484973.1	2153.66	
T04/R14-31L1	10/12/00	6	506	167675.2	1486274.0	1785.85	No longer wants to participate in monitoring program.
<b>Wells Added During this Study (2015)</b>							
T03/R13-24C1	5/30/1997	6	560	147297	1480932	NA	Well Tag: AAG-918
T03/R13-27A2	8/13/1998	6	220	142706	1472370	NA	Well Tag: ACX-768
T03/R13-27C1	7/30/2002	6	168	142810	1470134	NA	Well Tag: AGB-465
T03/R13-27D4	10/8/2001	6	634	142393	1470381	NA	Well Tag: AGM-070
T03/R13-27D5	2/17/2010	6	665	142756	1469398	NA	Well Tag: AFQ-965
T03/R13-27D6	7/11/2014	6	410	143353	1471194	NA	Well Tag: BIF-979
T03/R13-28C2	5/9/1990	6	160	141541	1464199	NA	

Note: The wells added in 2015 have not been surveyed at the time of this report. The coordinates (northing/easting) are from GPS. NA: Surveyed elevation not available at time of this report.

**Table 2 - Groundwater Level Data from Monitoring Network**

Hydrogeologic Assessment Knight-Dillacort Area

Ecology Well Log Data		June 2007 Measurements			November 2007 Measurements			April 2008 Measurements			December 2008 Measurements			April 2009 Measurements			December 2009 Measurements			May/June 2010 Measurements		
Ecology Well ID	TRS Label	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments
<b>Wells in Original Monitoring Network</b>																						
140432	T03/R13-3B1	203.6	1807.5		-	-	Well box frozen shut	-	-	No permission	207.2	1804.0		205.6	1805.6		206.2	1805.0		204.5	1806.7	
141250	T03/R13-3R1	549.5	1597.5		549.7	1597.3		549.7	1597.3		549.7	1597.3		549.4	1597.6		549.0	1598.0		-	-	Not monitored
377250	T03/R13-4L1	-	-		-	-		-	-		-	-		-	-		-	-		524.7	1601.6	
141715	T03/R13-11M1	115.1	1922.3		115.1	1922.4		115.2	1922.2		116.1	1921.4		115.4	1922.0		114.8	1922.6		115.5	1921.9	
139955	T03/R13-14A1	435.4	1745.7		434.4	1746.8		435.2	1746.0		434.2	1747.0		435.8	1745.4		-	-	Not monitored	434.8	1746.4	
377252	T03/R13-14G1	195.1	1890.9		196.0	1890.0		197.4	1888.6		197.0	1889.0		196.4	1889.6		196.8	1889.2		195.1	1890.9	
477832	T03/R13-14G2	173.2	1908.8		174.5	1907.6		177.6	1904.4		180.5	1901.6		181.1	1900.9		-	-	Unstable water level	176.8	1905.2	
136943	T03/R13-14J	-	-		-	-		-	-		-	-		-	-		-	-		323.4	1677.5	Rising water level
145893	T03/R13-15L1	-	-		-	-		-	-		-	-		-	-		-	-		13.4	1871.6	
144433	T03/R13-20N1	-	-		-	-		-	-		-	-		-	-		-	-		462.0	990.7	
384137	T03/R13-20N2	-	-		-	-		-	-		-	-		-	-		-	-		436.5	991.4	Rising water level
143160	T03/R13-21M1	-	-		-	-		-	-		-	-		-	-		-	-		492.4	1252.9	
145685	T03/R13-21P1	-	-		-	-		-	-		-	-		-	-		-	-		179.5	1390.5	Rising water level
335153	T03/R13-22C1	162.2	1615.3		161.3	1616.2		160.7	1616.8		161.9	1615.6		162.0	1615.5		175.0	1602.5		182.0	1595.5	
377254	T03/R13-22P1	139.5	1623.8	Unstable water level	139.7	1623.7		140.2	1623.2		139.7	1623.7		139.6	1623.8		140.9	1622.5		145.3	1618.1	
139217	T03/R13-23L1	75.3	1732.8	Airline measurement	-	-	Not monitored	-	-	Not monitored	-	-	Not monitored	-	-	Not monitored	-	-	Not monitored	41.7	1766.4	
556399	T03/R13-27	-	-		-	-		-	-		-	-		-	-		-	-		87.6	1659.5	
139404	T03/R13-27Q1	262.3	1733.7		261.4	1734.6		262.2	1733.8		261.8	1734.2		261.4	1734.6		260.0	1736.0		261.4	1734.6	
143537	T03/R13-28B1	141.2	1481.6		145.8	1477.0		141.8	1480.9		145.1	1477.6	Rising water level	141.4	1481.3		143.8	1478.9		142.0	1480.7	
372465	T03/R13-28F1	-	-		-	-		-	-		-	-		-	-		-	-		107.3	1420.0	
139337	T03/R13-28L1	21.4	1477.3	Rising water level	25.2	1473.5		20.4	1478.2		24.4	1474.3	Rising water level	21.0	1477.7		23.0	1475.7		19.4	1479.3	
354742	T03/R14-18N1	516.7	1637.0		518.3	1635.4		517.9	1635.7		519.5	1634.2		518.3	1635.3		-	-	Not monitored	518.6	1635.1	
302764	T04/R14-31L1	267.1	1518.7		265.4	1520.5		264.9	1521.0		265.2	1520.7		265.9	1520.0		264.8	1521.1		-	-	No permission
<b>Wells Added in 2015</b>																						
144057	T03/R13-24C1	-	-		-	-		-	-		-	-		-	-		-	-		-	-	
418100	T03/R13--27A2	-	-		-	-		-	-		-	-		-	-		-	-		-	-	
341503	T03/R13--27C1	-	-		-	-		-	-		-	-		-	-		-	-		-	-	
316087	T03/R13--27D4	-	-		-	-		-	-		-	-		-	-		-	-		-	-	
648556	T03/R13--27D5	-	-		-	-		-	-		-	-		-	-		-	-		-	-	
923889	T03/R13--27D6	-	-		-	-		-	-		-	-		-	-		-	-		-	-	
146705	T03/R13--28C2	-	-		-	-		-	-		-	-		-	-		-	-		-	-	

**Table 2 - Groundwater Level Data from Monitoring Network**

Hydrogeologic Assessment Knight-Dillacort Area

Ecology Well Log Data		November/December 2010 Measurements			April 2011 Measurements			November/December 2011 Measurements			April-June 2012 Measurements			October/November 2012 Measurements			April 2013 Measurements			November 2013 Measurements		
Ecology Well ID	TRS Label	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments
<b>Wells in Original Monitoring Network</b>																						
140432	T03/R13-3B1	214.6	1796.6		212.5	1798.7		211.5	1799.6		212.5	1798.7		206.0	1805.2		205.0	1806.2		204.9	1806.3	
141250	T03/R13-3R1	-	-	Not monitored	-	-	Not monitored	-	-	Not monitored	-	-	Not monitored	-	-	Not monitored	-	-	Not monitored	-	-	Not monitored
377250	T03/R13-4L1	524.2	1602.1		524.8	1601.4		524.7	1601.6		524.0	1602.3		524.2	1602.1		523.9	1602.3		-	-	No access - road too wet
141715	T03/R13-11M1	115.7	1921.8		115.8	1921.6		115.7	1921.7		114.4	1923.0		114.7	1922.7		114.7	1922.7		113.2	1924.2	
139955	T03/R13-14A1	436.1	1745.1		436.5	1744.6		439.5	1741.7		435.8	1745.4		436.4	1744.8		436.4	1744.7		439.1	1742.0	
377252	T03/R13-14G1	197.2	1888.8		197.6	1888.4		197.0	1889.0		196.4	1889.6		195.9	1890.1		196.3	1889.7		195.8	1890.2	
477832	T03/R13-14G2	182.7	1899.3		182.7	1899.4		181.6	1900.4		181.6	1900.4		181.5	1900.6		186.8	1895.3		183.1	1898.9	
136943	T03/R13-14J	322.3	1678.5		320.5	1680.4		-	-	No Permission	-	-	No Permission	-	-	No Permission	-	-	No Permission	-	-	
145893	T03/R13-15L1	11.4	1873.6		-	-	No Permission	-	-	Airline 23 psi	14.6	1870.4	Airline 26 psi	19.6	1865.4	Airline 24 psi	14.9	1870.1	Airline 26 psi	17.3	1867.8	Airline 25 psi
144433	T03/R13-20N1	478.4	974.3		478.4	974.3		492.2	960.5		506.1	946.6	Airline 6 psi	496.9	955.8	Airline 10 psi	496.9	955.8	Airline 10 psi	496.9	955.8	Airline 10 psi
384137	T03/R13-20N2	326.2	1101.7		343.0	1084.9	Rising water level	355.9	1072.0	Airline 58 psi	449.4	978.5	(Pump on) Airline 20 psi	341.4	1086.5	Airline 64 psi	399.4	1028.5	(Recovering) Airline 40 psi	315.4	1112.5	
143160	T03/R13-21M1	492.5	1252.8		489.3	1256.0		486.3	1259.0		485.1	1260.2	Airline 4 psi	484.0	1261.3	Airline 8 psi	483.0	1262.3	Airline 8.5 psi	482.0	1263.3	
145685	T03/R13-21P1	179.0	1390.9		177.1	1392.8		178.5	1391.4		177.9	1392.0		179.2	1390.7		178.1	1391.8		-	-	No permission
335153	T03/R13-22C1	185.0	1592.5		185.7	1591.8		188.1	1589.4		185.7	1591.8		193.8	1583.7		196.4	1581.1		205.1	1572.4	
377254	T03/R13-22P1	146.4	1617.0		150.6	1612.8		148.1	1615.3		149.2	1614.2		150.1	1613.3		151.0	1612.4		151.6	1611.8	
139217	T03/R13-23L1	38.6	1769.5		37.5	1770.6		38.4	1769.7		42.1	1766.0		39.1	1768.9		38.4	1769.7		40.0	1768.1	
556399	T03/R13-27	88.7	1658.4		87.6	1659.5		87.8	1659.3		86.9	1660.2		88.6	1658.5		88.5	1658.6		89.5	1657.6	
139404	T03/R13-27Q1	262.4	1733.6		263.3	1732.7		263.0	1733.0		263.3	1732.7		263.0	1733.0		264.0	1732.0		263.5	1732.5	Well head icy - lots of negative pressure
143537	T03/R13-28B1	143.2	1479.6		139.4	1483.3		141.0	1481.8		137.9	1484.8		147.9	1474.8		143.2	1479.5		144.4	1478.3	
372465	T03/R13-28F1	100.7	1426.6		95.8	1431.5		97.0	1430.3		94.3	1433.0		-	-	No Permission	-	-	No Permission	-	-	No Permission
139337	T03/R13-28L1	22.6	1476.1		18.6	1480.1		20.6	1478.1		17.6	1481.0		27.1	1471.5		22.1	1476.6		23.7	1475.0	
354742	T03/R14-18N1	519.1	1634.6		518.7	1635.0		-	-	No Permission	-	-	No Permission	-	-	No Permission	-	-	No Permission	520.0	1633.6	
302764	T04/R14-31L1	-	-	Not monitored	-	-	Not monitored	-	-	No Permission	-	-	No Permission	-	-	No Permission	-	-	No Permission	-	-	No Permission
<b>Wells Added in 2015</b>																						
144057	T03/R13-24C1	-	-		-	-		-	-		-	-		-	-		-	-		-	-	
418100	T03/R13--27A2	-	-		-	-		-	-		-	-		-	-		-	-		-	-	
341503	T03/R13--27C1	-	-		-	-		-	-		-	-		-	-		-	-		-	-	
316087	T03/R13--27D4	-	-		-	-		-	-		-	-		-	-		-	-		-	-	
648556	T03/R13--27D5	-	-		-	-		-	-		-	-		-	-		-	-		-	-	
923889	T03/R13--27D6	-	-		-	-		-	-		-	-		-	-		-	-		-	-	
146705	T03/R13--28C2	-	-		-	-		-	-		-	-		-	-		-	-		-	-	

**Table 2 - Groundwater Level Data from Monitoring Network**

Hydrogeologic Assessment Knight-Dillacort Area

Ecology Well Log Data		April 2014 Measurements			November 2014 Measurements			April 2015 Measurements		
Ecology Well Log ID	TRS Label	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments	Depth to Water (ft bTOC)	GW Elevation <sup>2</sup> (ft)	Comments
<b>Wells in Original Monitoring Network</b>										
140432	T03/R13-3B1	204.0	1807.2		216.1	1795.1	Not static	-	-	No permission
141250	T03/R13-3R1	-	-	Not monitored	-	-	No permission	-	-	No permission; no contact info - <b>discontinue monitoring</b>
377250	T03/R13-4L1	523.6	1602.6		523.8	1602.5		520.1	1606.2	access issues; Sonic usually inaccurate
141715	T03/R13-11M1	112.6	1924.8		111.4	1926.0		112.2	1925.2	Sonic OK.
139955	T03/R13-14A1	435.5	1745.6		436.5	1744.7	Not static	429.4	1751.8	
377252	T03/R13-14G1	194.7	1891.3		142.4	-	Measurement ~50 ft higher than normal; likely measurement error	193.9	1892.1	
477832	T03/R13-14G2	182.3	1899.8		182.5	1899.5		181.5	1900.5	
136943	T03/R13-14J	316.9	1683.9		-	-	No permission	-	-	No permission
145893	T03/R13-15L1	16.1	1868.9	Airline 25.5 psi	15.1	1869.9	Airline 24.5 psi	13.1	1871.9	
144433	T03/R13-20N1	492.3	960.5	Airline 12 psi	492.3	960.5	Airline 12 psi	486.5	966.2	Airline 14.5 psi
384137	T03/R13-20N2	286.6	1141.3	Airline 88.5 psi; non-static	-	-	No permission	284.1	1143.8	
143160	T03/R13-21M1	480.8	1264.5		-	1266.2	Airline 9 psi; waterline access issues	479.1	1266.2	Airline 9.0 psi
145685	T03/R13-21P1	179.8	1390.2		180.5	1389.5		178.6	1391.3	
335153	T03/R13-22C1	207.4	1570.1		217.2	1560.3		218.8	1558.7	
377254	T03/R13-22P1	152.3	1611.1		173.9	1589.5		178	1585	Reading provided by well owner.
139217	T03/R13-23L1	-	-	Airline 37.5 psi	39.4	1768.6	Airline 38 psi	33.2	1774.9	
556399	T03/R13-27	89.0	1658.1		88.8	1658.3		91.0	1656.1	
139404	T03/R13-27Q1	264.6	1731.5		259.9	1736.1		266.4	1729.6	
143537	T03/R13-28B1	142.0	1480.7		142.4	1480.3		143.0	1479.7	
372465	T03/R13-28F1	-	-	No Permission	-	-	No permission	-	-	No permission; no contact info - <b>discontinue monitoring</b>
139337	T03/R13-28L1	21.0	1477.7		23.9	1474.7	Not static	20.9	1477.8	
354742	T03/R14-18N1	519.0	1634.6	Sonic inaccurate	312.8	-	Waterline access issues; Sonic likely inaccurate	248.8	-	Sonic likely inaccurate (248.8 deep, 61.9 normal); use waterline only
302764	T04/R14-31L1	-	-	No Permission	-	-	No permission	-	-	<b>Discontinue monitoring;</b> no contact info -
<b>Wells Added in 2015</b>										
144057	T03/R13-24C1	-	-		-	-		333.6		Not static, sonic ok
418100	T03/R13--27A2	-	-		-	-		173.4		Tape stuck at 150', used sonic
341503	T03/R13--27C1	-	-		-	-		148.9		Sonic no good
316087	T03/R13--27D4	-	-		-	-		-		Cannot access well, port too small to fit tape. Sonic no good
648556	T03/R13--27D5	-	-		-	-		457.7		Sonic no good
923889	T03/R13--27D6	-	-		-	-		207.9		Sonic no good
146705	T03/R13--28C2	-	-		-	-		-		Removed well cap, water shot out

**Notes:**

<sup>1</sup> Northing and Easting coordinates are in Washington South State Plane coordinate system (NAD 1983 datum).

<sup>2</sup> Elevations are in NAVD88 vertical datum.

<sup>3</sup> Blank cell in Depth to Water column indicates that the well was not yet included in the monitoring network.

<sup>4</sup> See Table 1 regarding survey of wells added in 2015.

**Table 3 - Groundwater Quality Analytical Results, April 2015**

Knight-Dillacort Area Hydrogeologic Assessment

Analyte	22P1 280 ft deep 4/15/2015	27A2 220 ft deep 4/15/2015	27C1 168 ft deep 4/15/2015	27D4 634 ft deep 4/15/2015	27D6 410 ft deep 4/15/2015	28B1 220 ft deep 4/15/2015
<b>Conventionals</b>						
<i>Common Cations</i>						
Calcium in mg/L	24.4	16.1	21	22.2	23.5	19.8
Magnesium in mg/L	15.4	7.88	9.91	11.6	14.0	11.4
Potassium in mg/L	3.4	2.4	2.3	3.2	2.6	2.6
Sodium in mg/L	11.7	8.8	11.6	11.2	11.3	14.6
Cation Ratio (calculated)	0.28	0.32	0.31	0.30	0.27	0.36
<i>Common Anions</i>						
Alkalinity in mg/L as CaCO <sub>3</sub>	129	88.8	113	124	138	103
Bicarbonate in mg/L as CaCO <sub>3</sub>	129	88.8	113	124	138	103
Carbonate in mg/L as CaCO <sub>3</sub>	1 U	1 U	1 U	1 U	1 U	1 U
Hydroxide in mg/L as CaCO <sub>3</sub>	1 U	1 U	1 U	1 U	1 U	1 U
Chloride in mg/L	3.2	2.6	4.6	3.8	2.5	13.1
Sulfate in mg/L	21.0	1.7	1.6	3.4	3.8	7.0
<i>Other Constituents</i>						
Fluoride in mg/L	0.2	0.2	0.2	0.2	0.2	0.4
Nitrate in mg-N/L	0.1 U	0.4	0.9	0.2	0.1 U	1.0
Silicon in mg/L	22.1	27.0	28.5	23.4	19.7	26.1
<b>Carbon 14 Isotope Parameters</b>						
fMDN (fraction modern carbon) with error range	0.4756 +/- 0.0018	0.6010 +/- 0.0022	0.6420 +/- 0.0024	0.5386 +/- 0.0020	0.3897 +/- 0.0014	0.4786 +/- 0.0018
Radiocarbon Age in Years	5,970	4,090	3,560	4,970	7,570	5,920
Estimated Error in Radiocarbon Age (Years +/-)	20	10	10	20	30	20
<b>Field Parameters</b>						
Temperature in deg C	9.3	9.7	12.6	12.5	12.8	13.9
Specific Conductance in uS/cm	282	178	223	237	257	254
Dissolved Oxygen in mg/L	8.9	5.4	8.7	3.8	0.1	4.2
pH in pH units	8.2	7.0	7.5	7.7	8.1	7.6
ORP in mV	94	102	89	88	82	86
Turbidity in NTU	1	7	1	3	14	1

Radiocarbon age estimates rounded to nearest 10 years.

U: Not detected at associated reporting limit.

**Aspect Consulting**

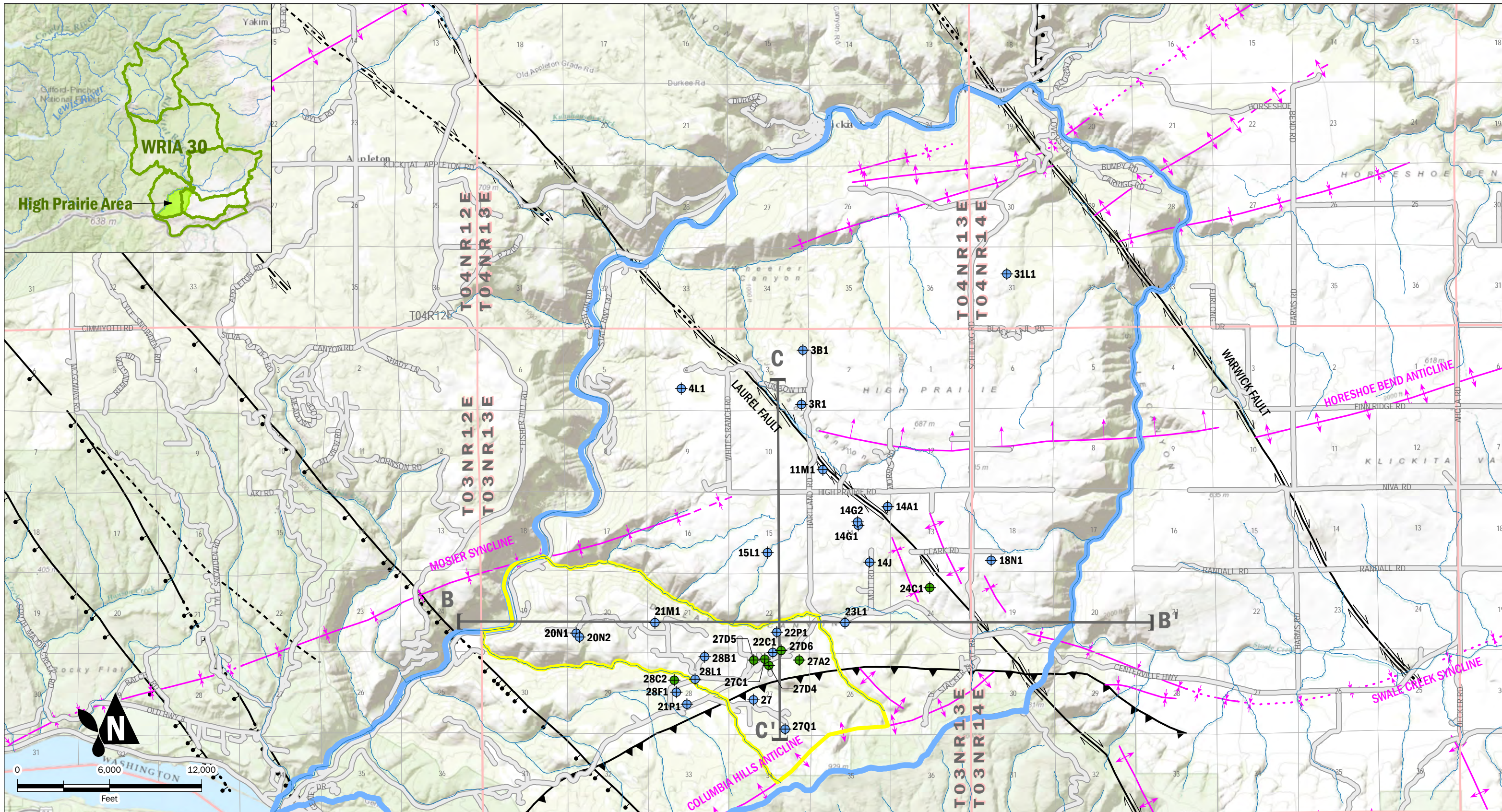
7/27/2015

W:\090045 WRIA 31 Phase 4\Deliverables\Hydrogeologic Assessment\Tables & Figures\Table 3 + Figs 13 14 15 16 GW Quality.xlsx

**Table 3**

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# FIGURES



<b>High Prairie Well Network</b> Monitoring Started 2015 Monitored Since 2010 or Earlier Cross Section Knight-Dillacort Study Area High Prairie Area		<b>Folds (Washington DNR 1:100K mapping)</b> Anticline (dashed where inferred). Syncline (dashed where inferred). Monocline, anticlinal bend (dashed where inferred).		<b>Faults (Washington DNR 1:100K mapping)</b> Thrust fault (dashed where inferred). Sawteeth on upper plate. Normal fault (dashed where inferred). Bar and ball on downthrown block. Fault, unknown offset (dashed where inferred). Strike-slip fault (dashed where inferred; arrows show relative motion)	
Roads Township/Range Sections					

**High Prairie Well Monitoring Network  
and Knight-Dillacort Study Area**  
Knight-Dillacort Area Hydrogeologic Assessment  
WRIA 30, Washington

	JUL-2015	BY: JMS / PPW	FIGURE NO. <b>1</b>
	PROJECT NO. 090045-17B	REV BY: EAC	

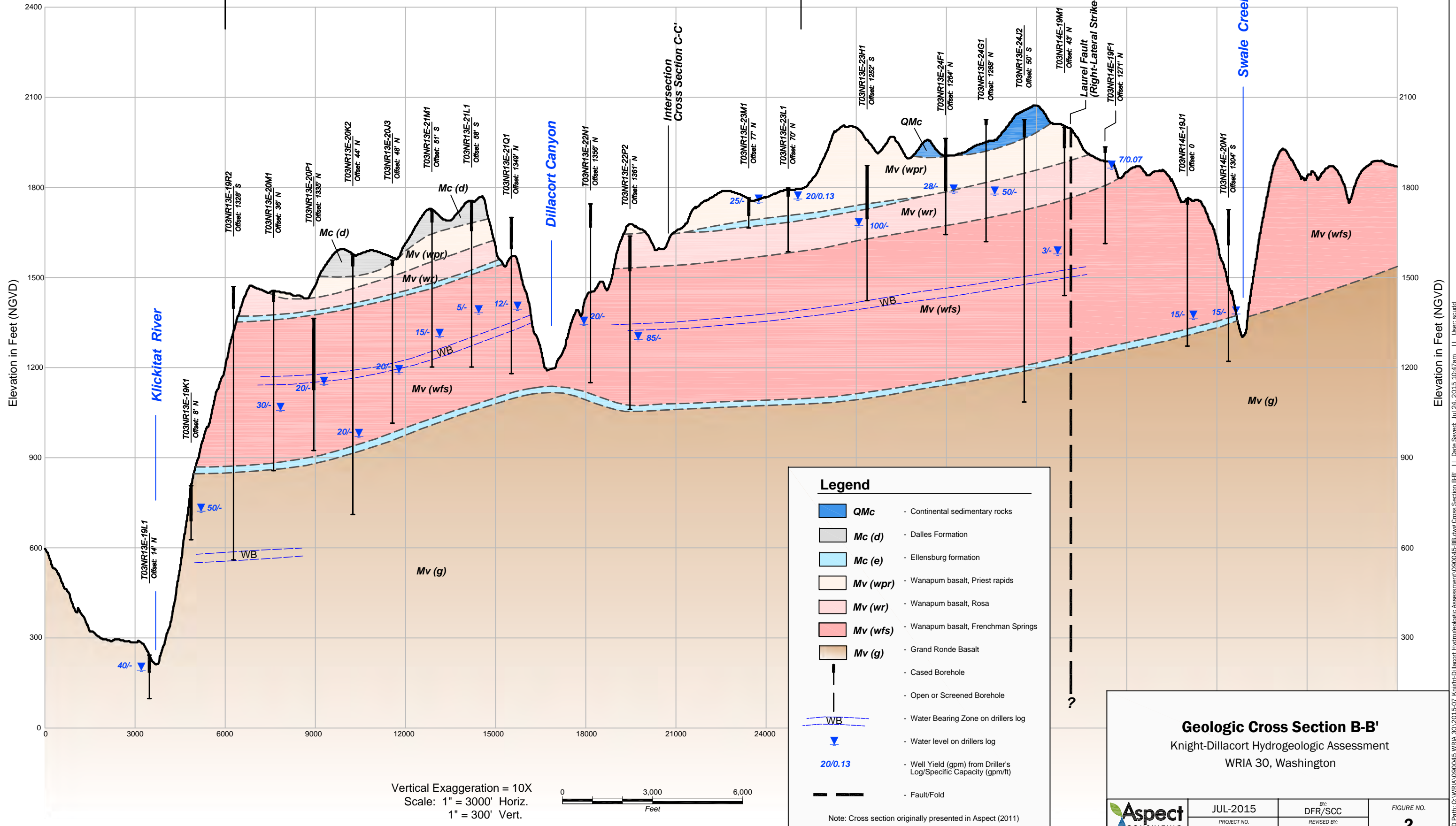
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High Prairie

B West

East B'

Knight-Dillacort Study Area



**Legend**

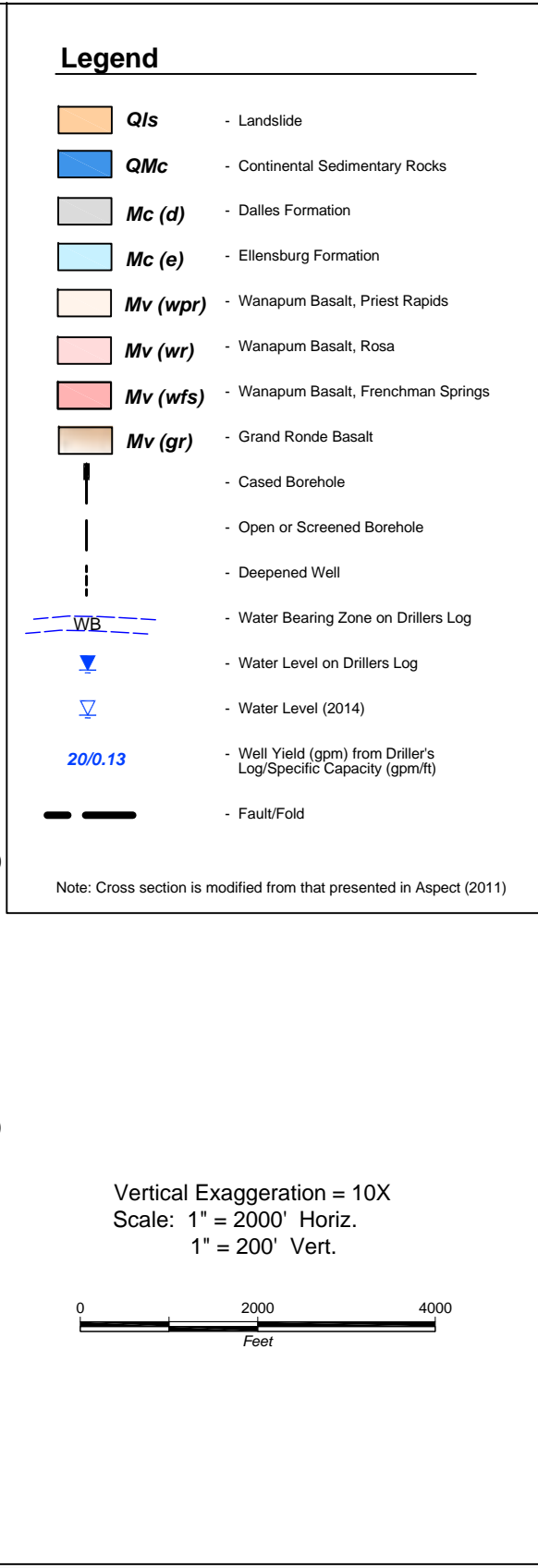
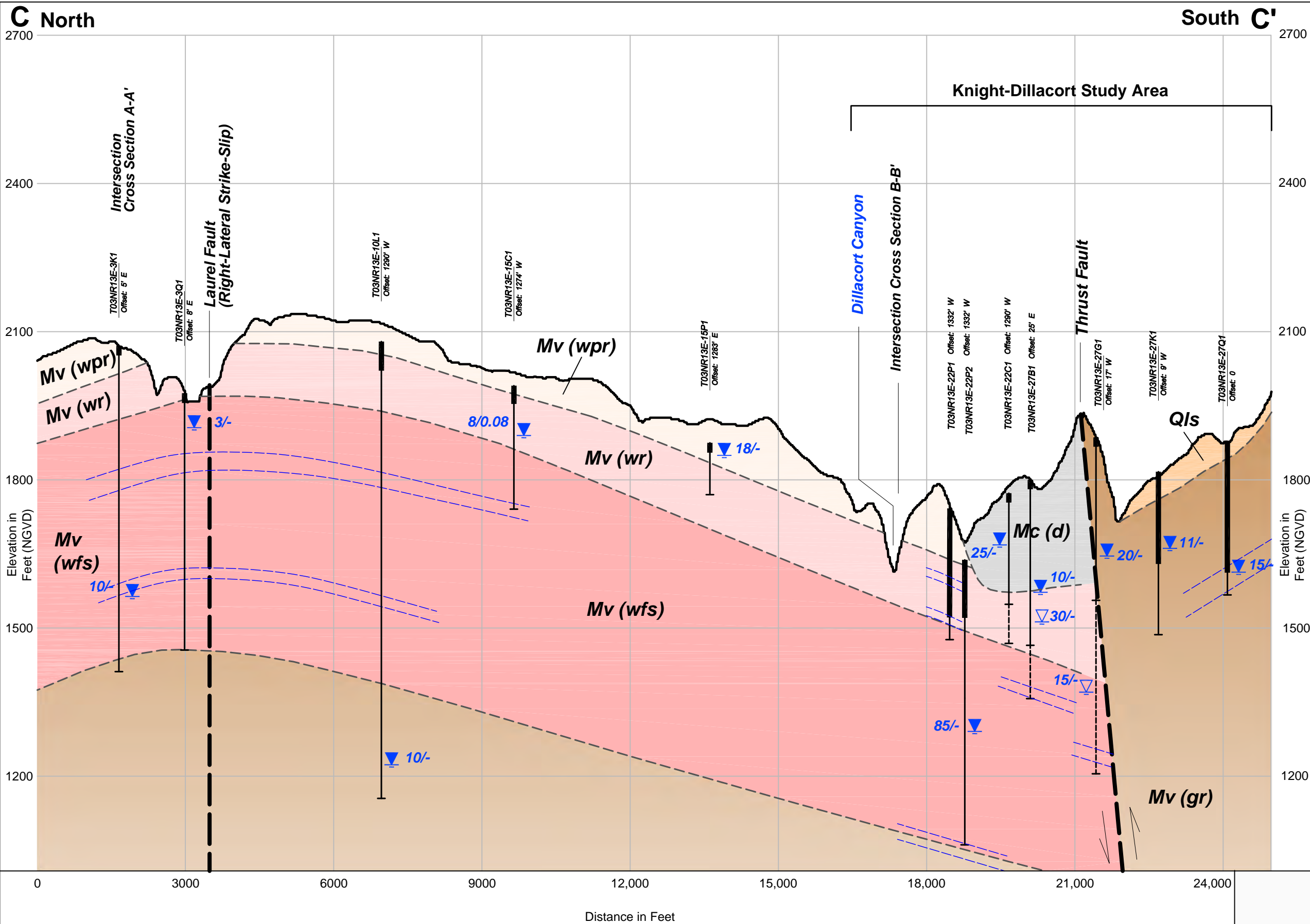
- QMc** - Continental sedimentary rocks
- Mc (d)** - Dalles Formation
- Mc (e)** - Ellensburg formation
- Mv (wpr)** - Wanapum basalt, Priest rapids
- Mv (wr)** - Wanapum basalt, Rosa
- Mv (wfs)** - Wanapum basalt, Frenchman Springs
- Mv (g)** - Grand Ronde Basalt
- Cased Borehole
- Open or Screened Borehole
- WB** - Water Bearing Zone on drillers log
- Water level on drillers log
- 20/0.13** - Well Yield (gpm) from Driller's Log/Specific Capacity (gpm/ft)
- Fault/Fold

Note: Cross section originally presented in Aspect (2011)

Vertical Exaggeration = 10X  
 Scale: 1" = 3000' Horiz.  
 1" = 300' Vert.

**Geologic Cross Section B-B'**  
 Knight-Dillacort Hydrogeologic Assessment  
 WRIA 30, Washington

	JUL-2015	BY: DFR/SCC	FIGURE NO. <b>2</b>
	PROJECT NO. 090045	REVISED BY: SCC	

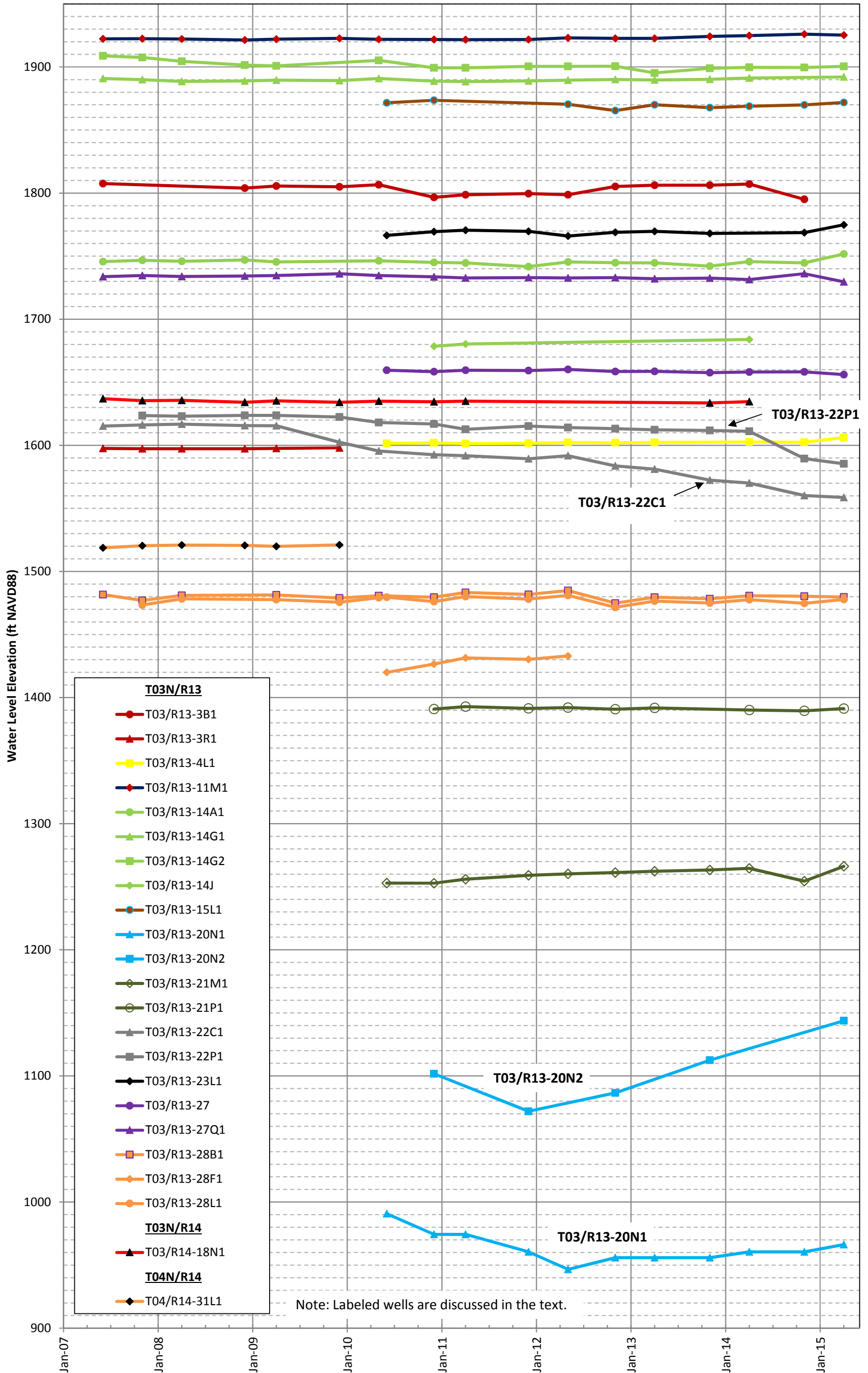


<b>Geologic Cross Section C-C'</b>		Knight-Dillacort Hydrogeologic Assessment		WRIA 30, Washington	
	JUL-2015	BY:	DFR/SCC	FIGURE NO.	
	PROJECT NO. 090045	REVISED BY:	SCC	<b>3</b>	

CAD Path: Q:\WRIA\090045\WRIA\_30\2015-07\_Knight-Dillacort\_Hydrogeologic\_Assessment\090045-CC\_Detail.dwg Cross Section CC (2) | Date Saved: Jul 24, 2015 11:54am | User: scudd

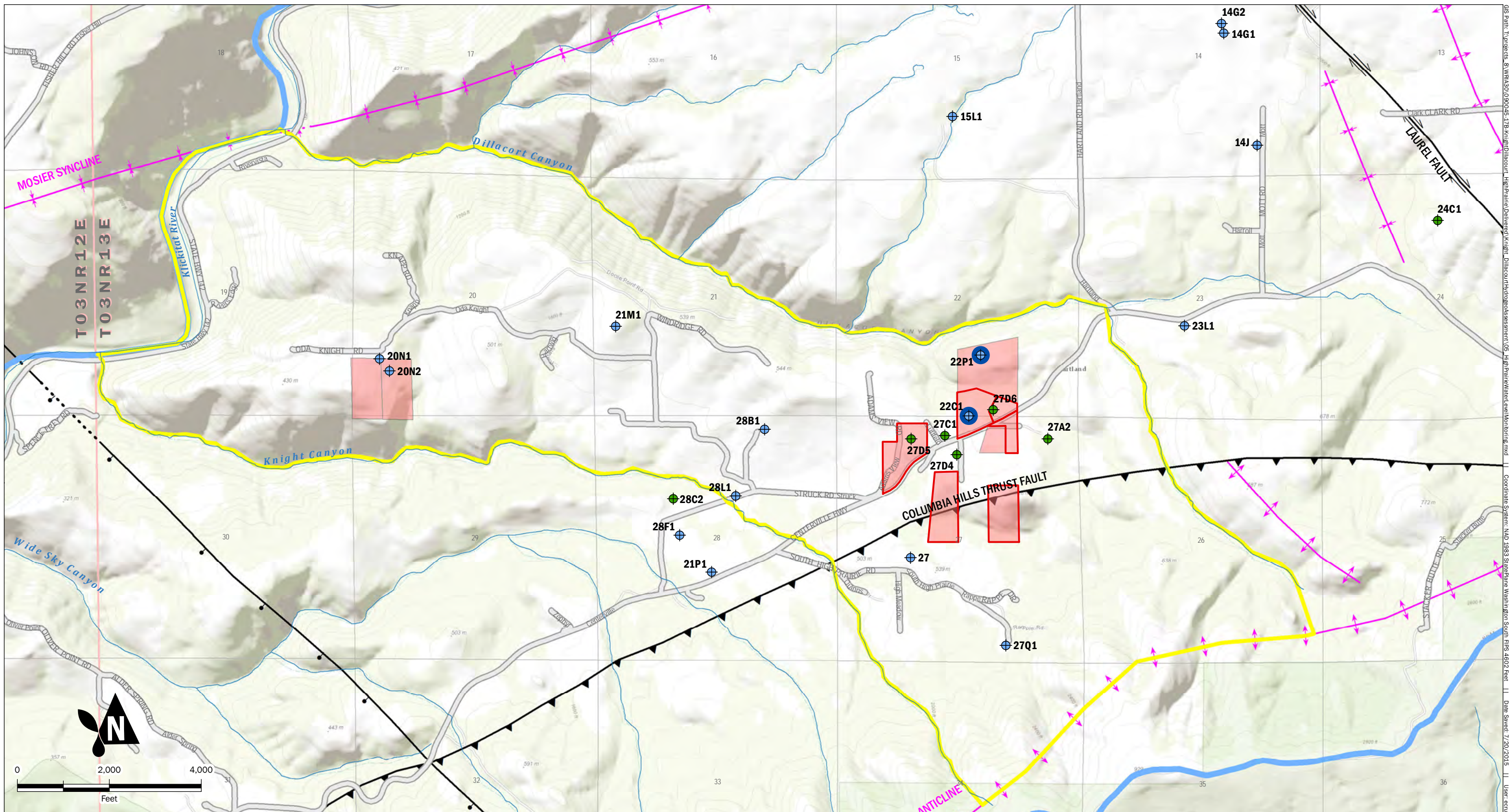
**Notes:**

Any depth-to-water measurements from Table 6 which had non-static water levels were not included in the hydrographs.



**Figure 4 - High Prairie Monitoring Network Water Level Hydrographs**

Hydrogeologic Assessment  
Knight-Dillacort Area of High Prairie



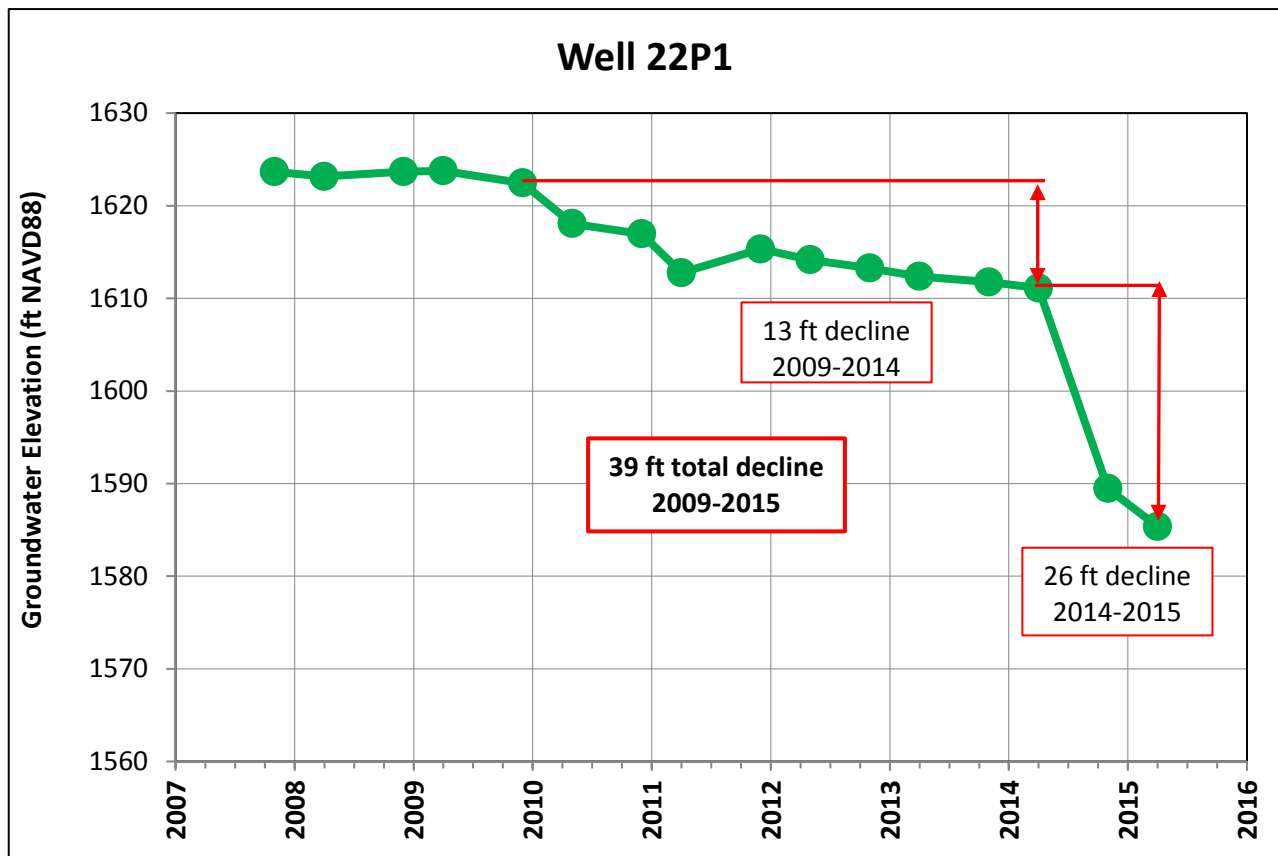
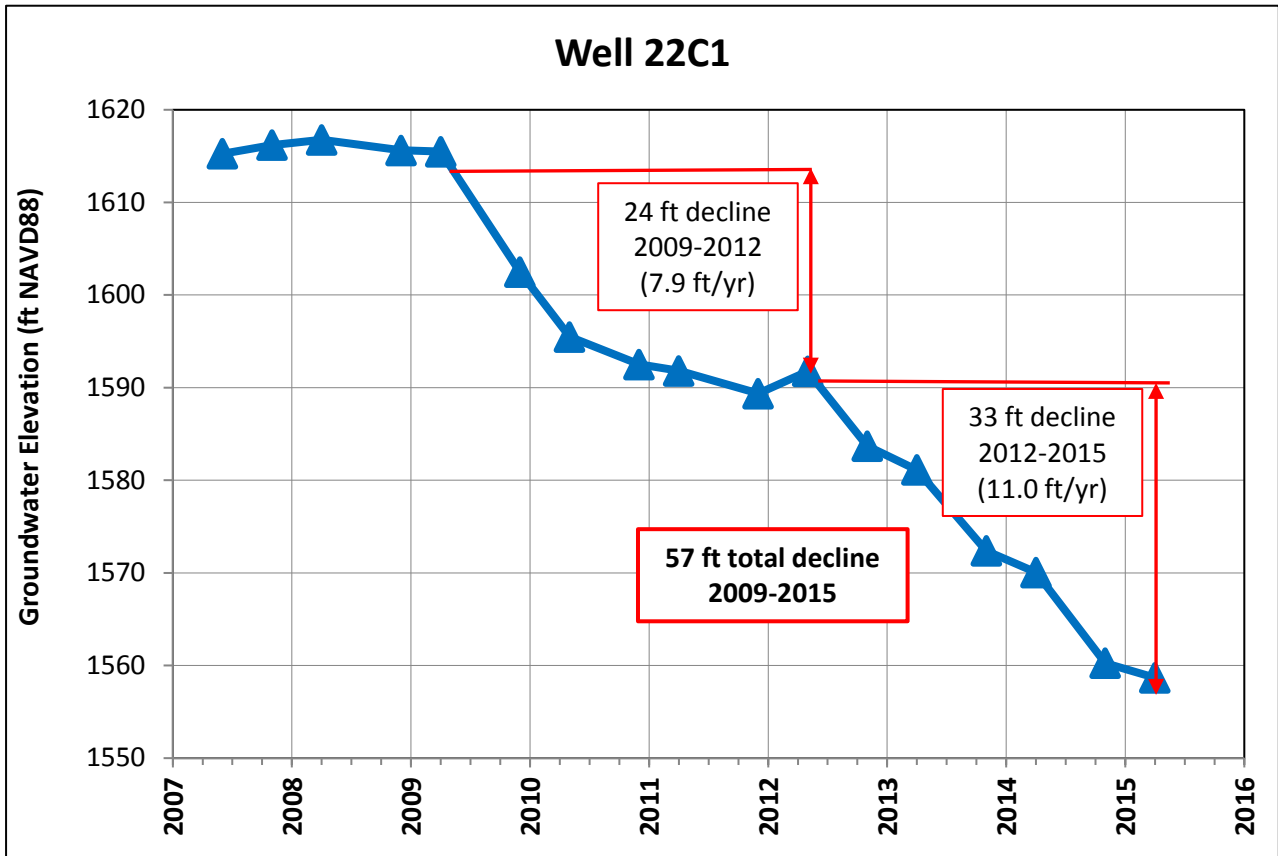
<b>High Prairie Well Network</b> Monitoring Started 2015 3B1 Monitored Since 2010 or Earlier Monitoring Network Well with Documented Ongoing Water Level Decline Knight-Dillacort Study Area High Prairie Area		Parcels with Well Deepened Since 2010 Parcels with Observed Decline in Groundwater Level or Yield Roads Township/Range Sections		<b>Folds (Washington DNR 1:100K mapping)</b> Anticline (dashed where inferred). Syncline (dashed where inferred). Monocline, anticlinal bend (dashed where inferred).		<b>Faults (Washington DNR 1:100K mapping)</b> Thrust fault (dashed where inferred). Sawteeth on upper plate. Normal fault (dashed where inferred). Bar and ball on downthrown block. Fault, unknown offset (dashed where inferred). Strike-slip fault (dashed where inferred; arrows show relative motion)	
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### Areas with Reported Groundwater Declines and Recently Deepened Wells

Knight-Dillacort Area Hydrogeologic Assessment  
WRIA 30, Washington

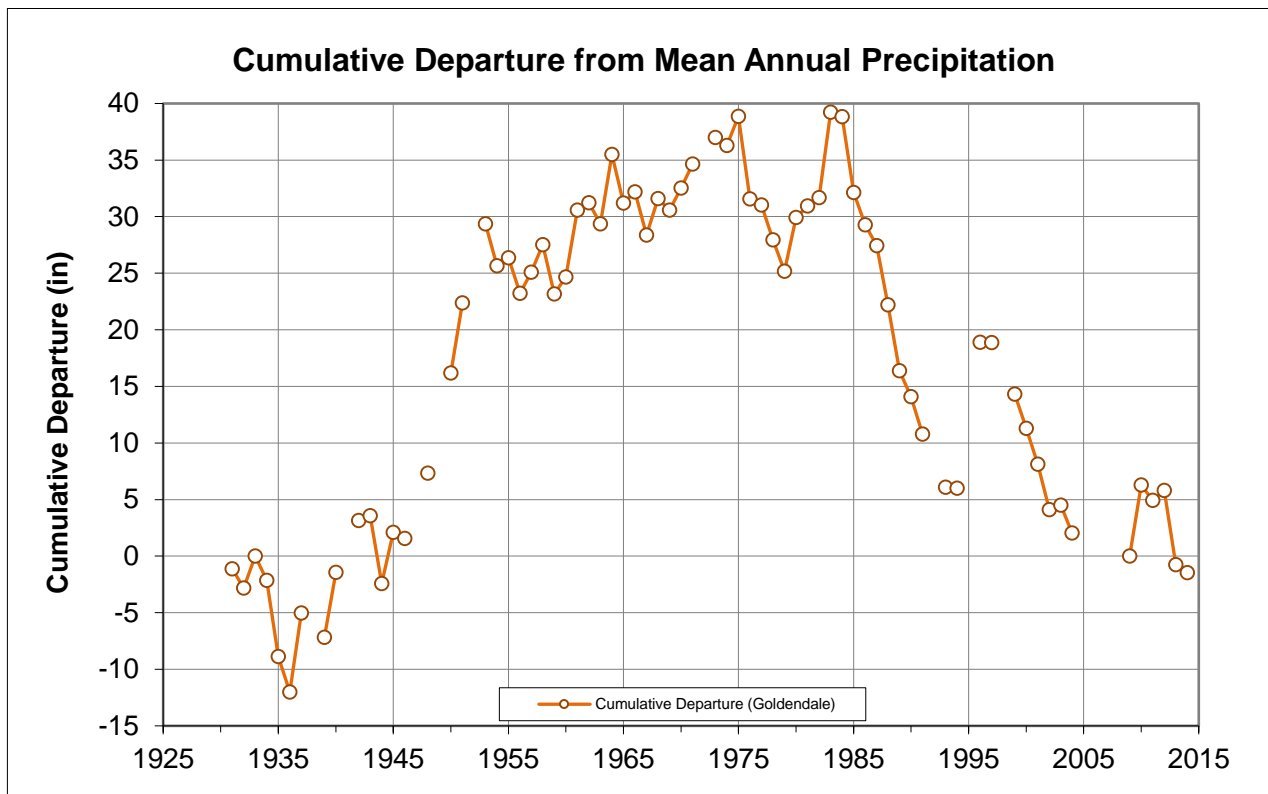
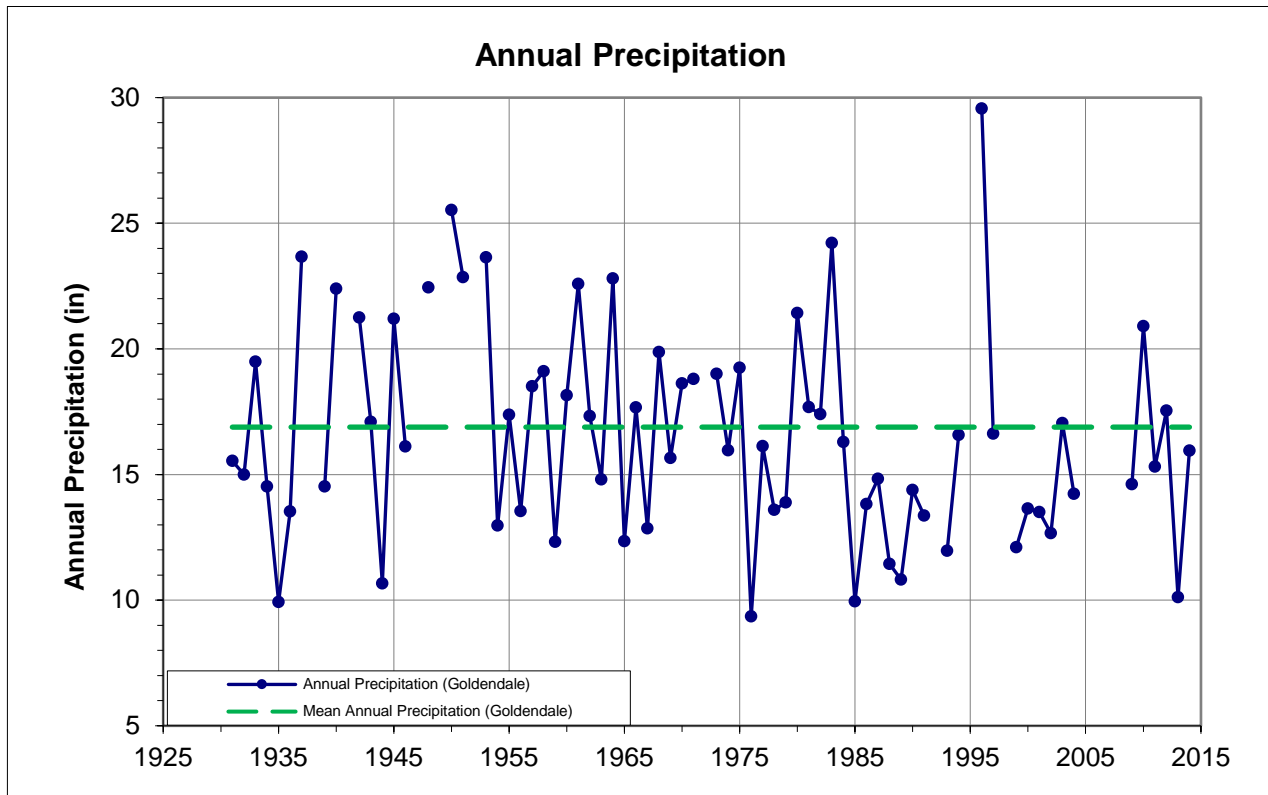
	JUL-2015	BY: JMS / PPW	FIGURE NO. <b>5</b>
	PROJECT NO. 090045-17B	REVISED BY: EAC	

GIS Path: \\projects\_8\WRIA30\090045-17B\KnightDillacort\Knight-DillacortHydrogeologicAssessment\05\_HighPrairieWellNetworkExam\Knight-DillacortHydrogeologicAssessment.mxd | Coordinate System: NAD 1983 StatePlane Washington South FIPS 4602 Feet | Date Saved: 7/20/2015 | User: eacumbaker | Print Date: 7/21/2015



**Figure 6**

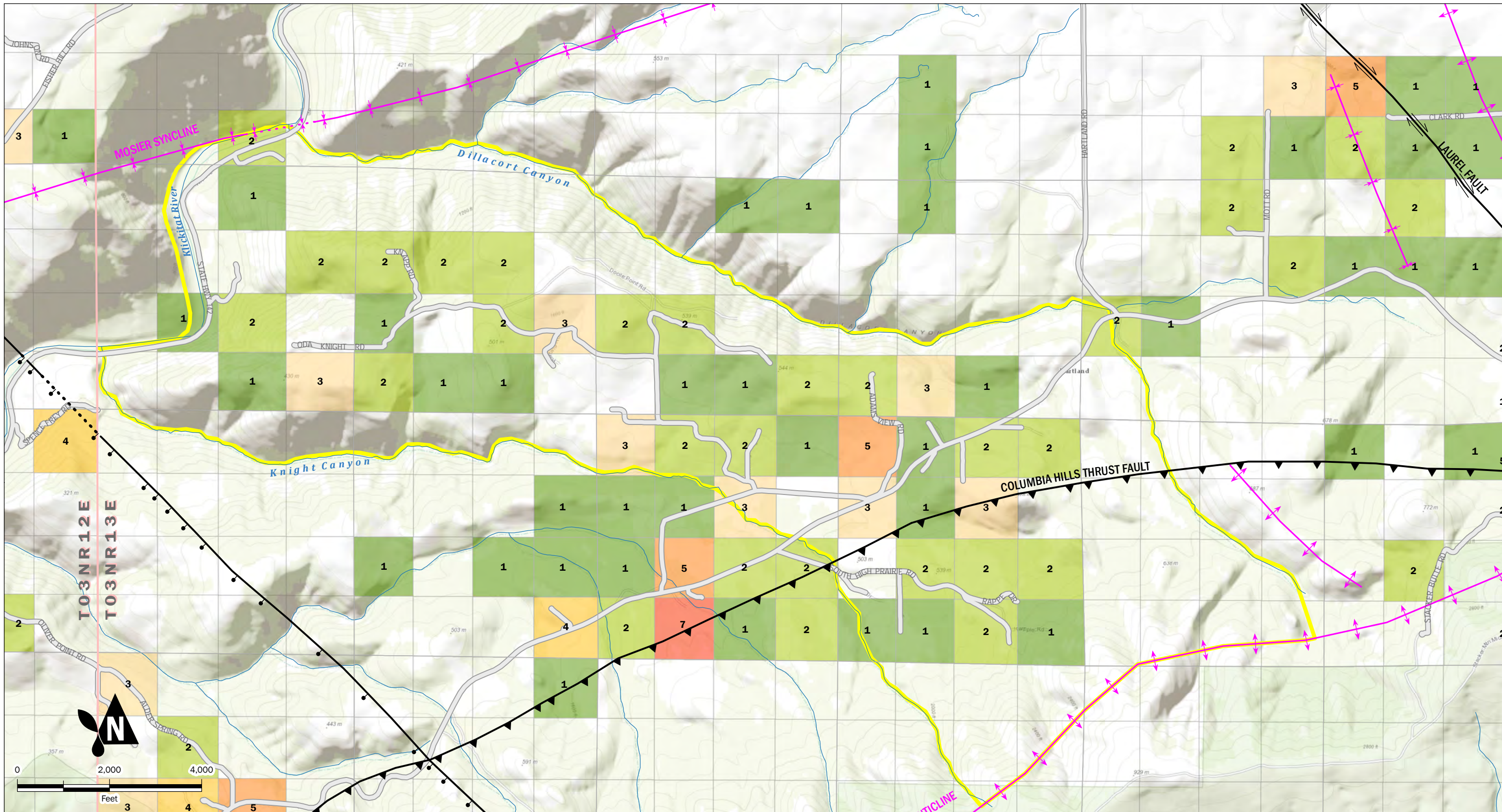
**Measured Water Level Declines,  
Eastern Knight-Dillacort Area**



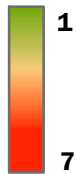
**Notes:**

Considered most applicable and reliable for evaluating long-term trends for High Prairie, the annual precipitation data are from Goldendale station (NOAA #453222) and Goldendale 2E station (NOAA #453226). While the magnitude of precipitation will be different from High Prairie, the trends (above or below normal) should be comparable.

Individual months with more than 5 days of missing data were not used for either monthly or annual statistics.



**Well Density**  
(Number of Wells per Quarter Section)



Note:  
Data from Dept. of Ecology  
well log database (Nov. 2014).

- Knight-Dillacort Study Area
- Township/Range
- Sections

- Folds (WA DNR 1:100K)**
- Anticline (dashed where inferred).
  - Syncline (dashed where inferred).

- Faults (WA DNR 1:100K)**
- Thrust fault (dashed where inferred). Sawteeth on upper plate
  - Normal fault (dashed where inferred). Bar and ball on downthrown block
  - Strike-slip fault (dashed where inferred; arrows show relative motion)

**Well Density within Knight-Dillacort Area**  
Knight-Dillacort Area Hydrogeologic Assessment  
WRIA 30, Washington

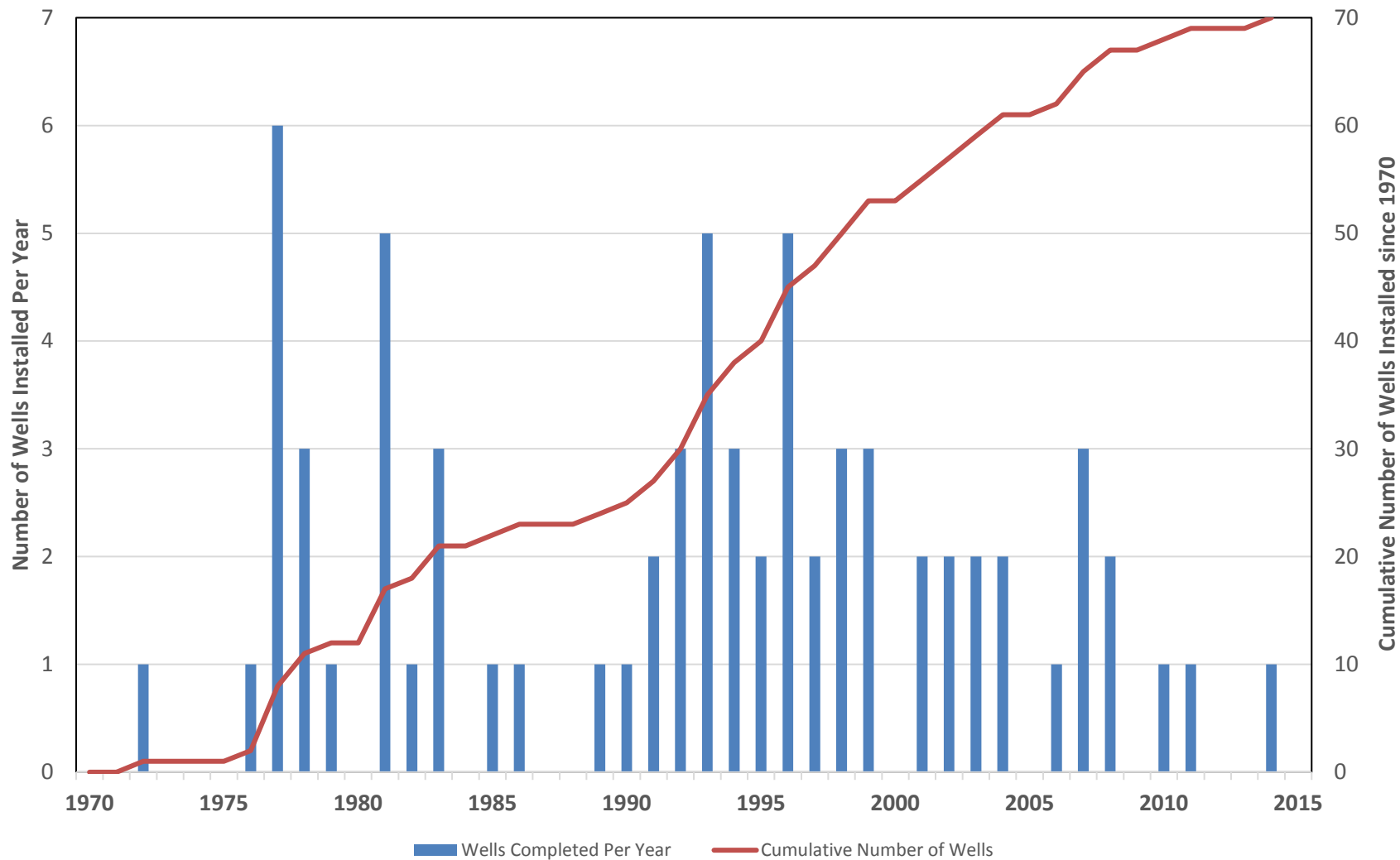


JUL-2015  
PROJECT NO.  
090045-17B

BY:  
DFR / RAA  
REVISED BY:  
EAC

FIGURE NO.  
**8**

GIS Path: \\pdr\cda\_8\WRIA30\090045-17B\KnightDillacort\_Area\HydrogeologicAssessment\08\_WellDensity\KnightDillacort.mxd | Coordinate System: NAD 1983 StatePlane Washington South FIPS 4602 Feet | Date Saved: 7/20/2015 | User: ecumshaver | Print Date: 7/20/2015



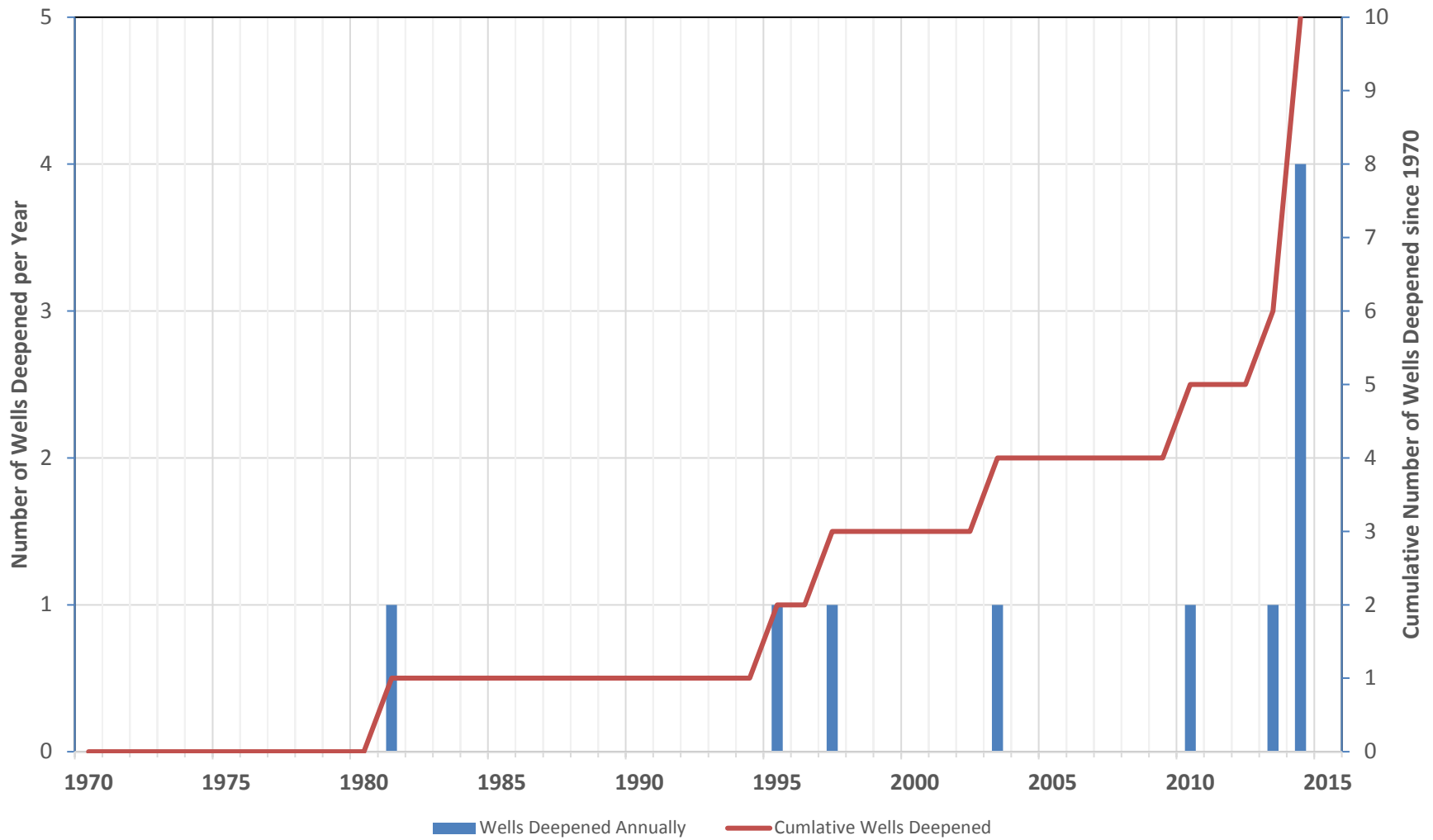
Wells within Sections 21, 22, 27, and 28 of Township 3 North Range 13 East. Data based on Ecology well log database.

Aspect Consulting

7/27/2015

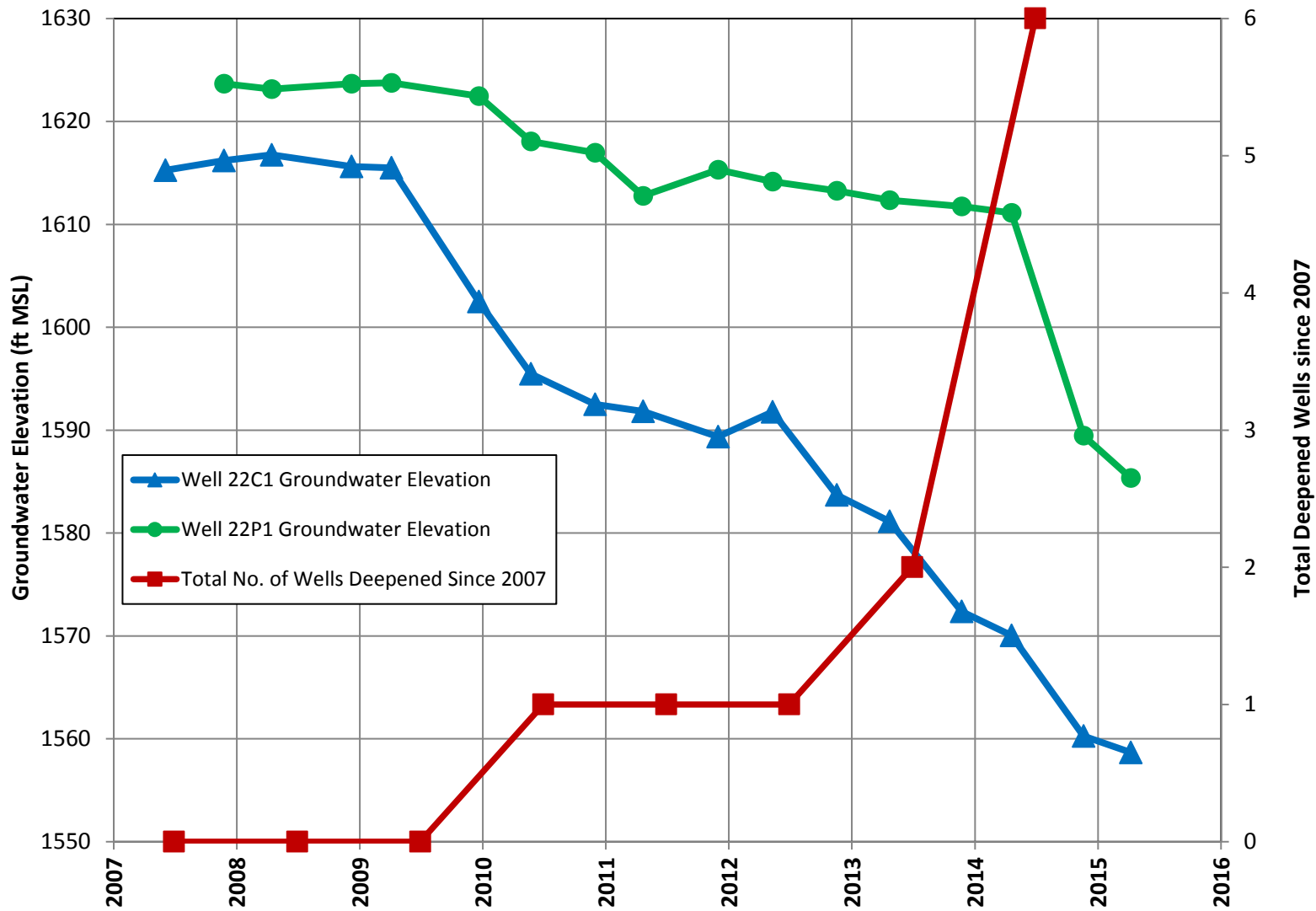
W:\090045 WRIA 31 Phase 4\Deliverables\Hydrogeologic Assessment\Tables & Figures\  
Tables 1&2 + Figs 4 6-7 9-11.xlsx

**Figure 9**  
**Number of Well Installations Over Time**

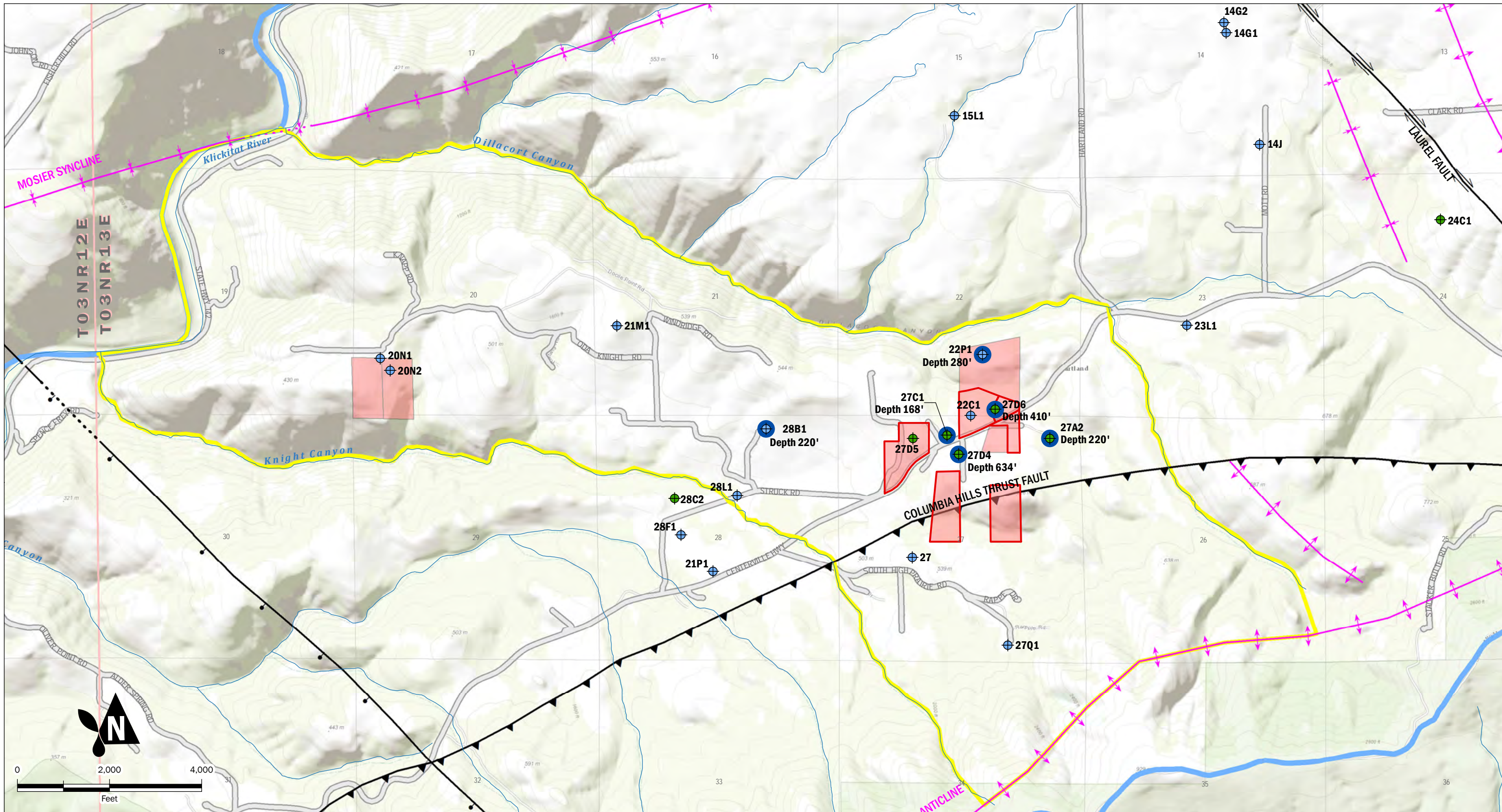


Wells within Sections 21, 22, 27, and 28 of Township 3 North Range 13 East. Data based on Ecology well log database.

**Figure 10**  
**Number of Wells Deepened**  
**Over Time**



**Figure 11**  
**Timing of Water Level Declines and**  
**Local Well Deepenings**



<b>High Prairie Well Network</b> Monitoring Started 2015 3B1 Monitored Since 2010 or Earlier Sampled Wells Knight-Dillacort Area High Prairie Study Area		Parcels with Well Deepened Since 2010 Parcels with Observed Decline in Groundwater Level or Yield Roads Township/Range Sections		<b>Folds (Washington DNR 1:100K mapping)</b> Anticline (dashed where inferred). Syncline (dashed where inferred). Monocline, anticlinal bend (dashed where inferred).		<b>Faults (Washington DNR 1:100K mapping)</b> Thrust fault (dashed where inferred). Sawteeth on upper plate. Normal fault (dashed where inferred). Bar and ball on downthrown block. Fault, unknown offset (dashed where inferred). Strike-slip fault (dashed where inferred; arrows show relative motion)	
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### Wells Sampled for Groundwater Quality

Knight-Dillacort Area Hydrogeologic Assessment  
WRIA 30, Washington

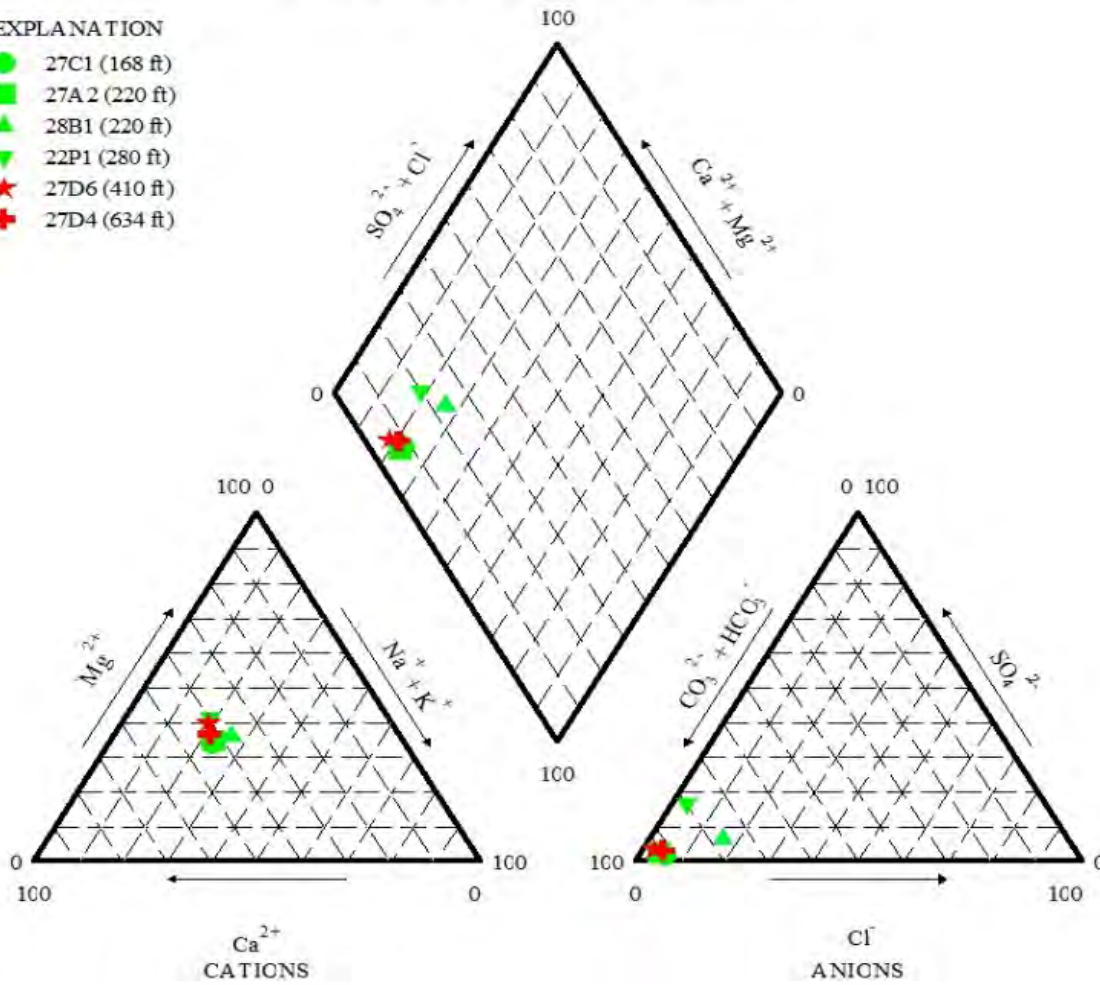
	JUL-2015	BY: JMS / PPW	FIGURE NO. <b>12</b>
	PROJECT NO. 090045-17B	REVISED BY: EAC	

GIS Path: T:\projects\_8\WRIA30\090045-17B\KnightDillacort\_Area\HydrogeologicAssessment\_V2\WellSamples\of\GroundwaterQuality.mxd | Coordinate System: NAD 1983 StatePlane Washington South FIPS 4602 Feet | Date Saved: 7/21/2015 | User: ecumshaw | Print Date: 7/21/2015

### Piper Plot of Groundwater Common Ions

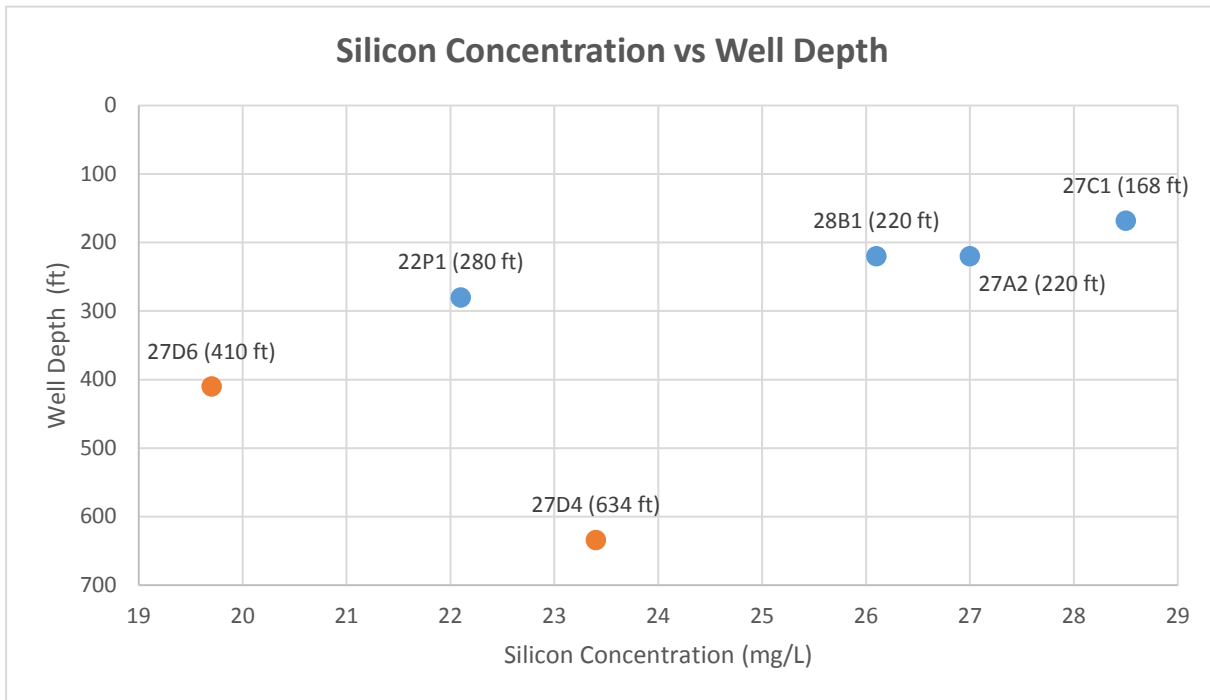
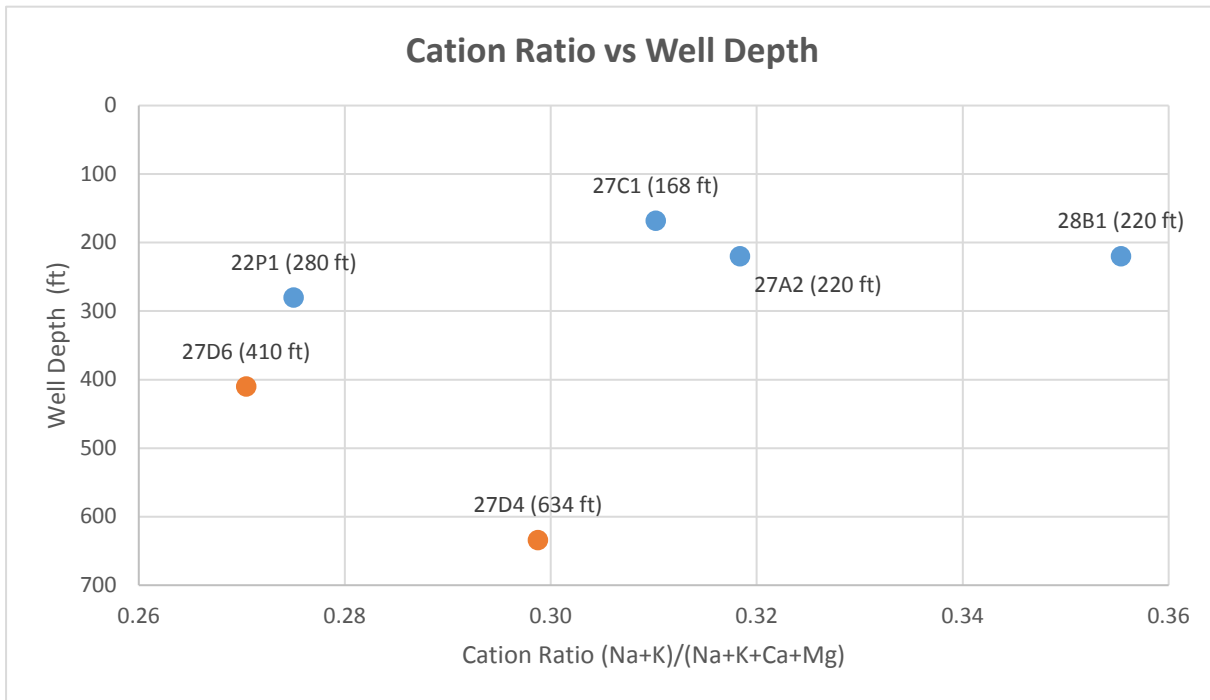
**EXPLANATION**

- 27C1 (168 ft)
- 27A 2 (220 ft)
- ▲ 28B1 (220 ft)
- ▼ 22P1 (280 ft)
- ★ 27D6 (410 ft)
- ✚ 27D4 (634 ft)



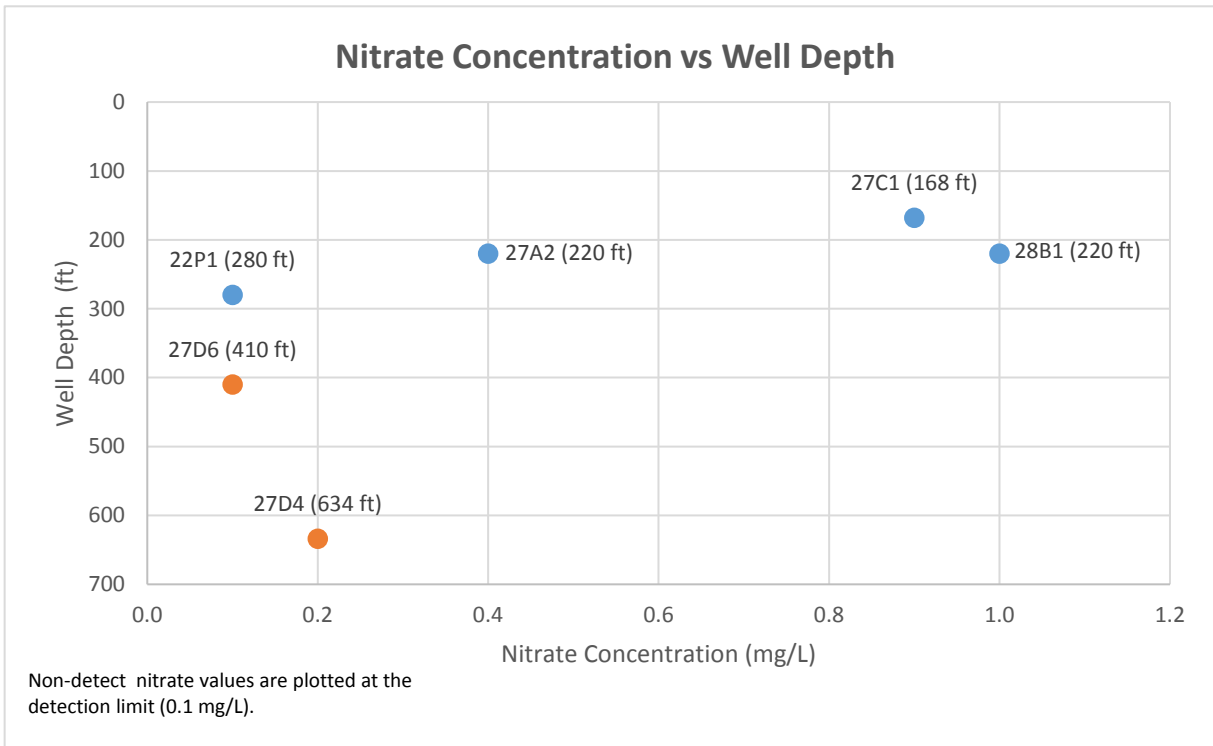
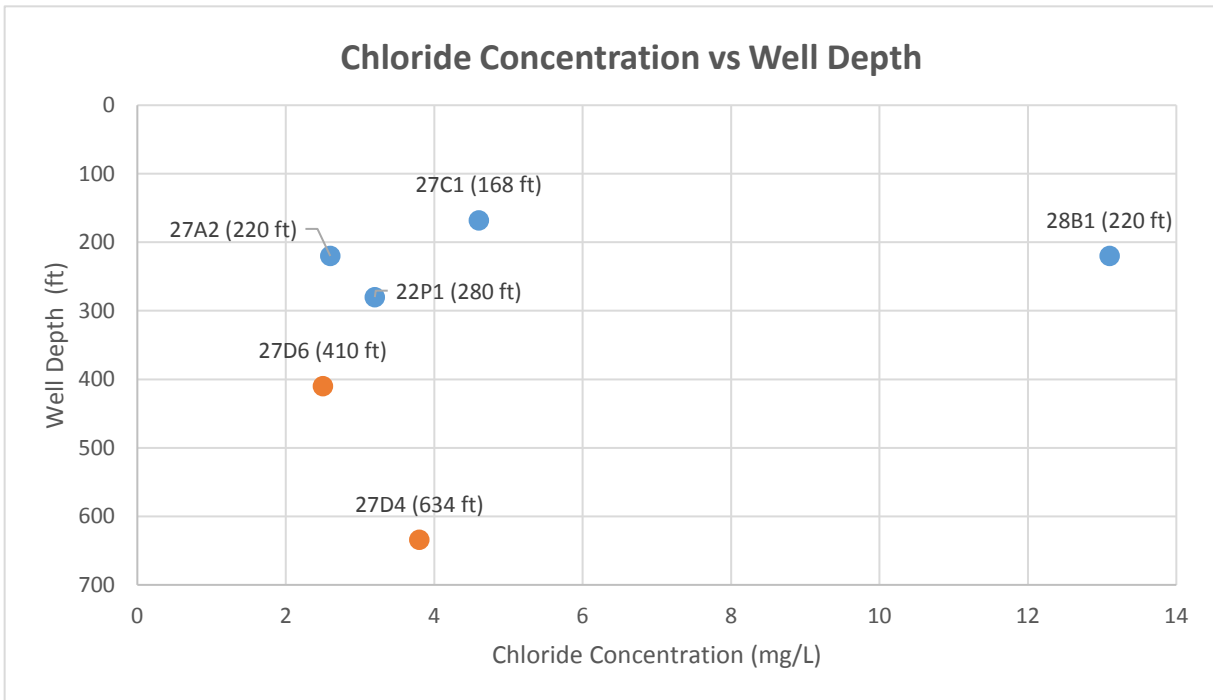
**Figure 13**

**Piper Plot of Groundwater Common Ion Concentrations**



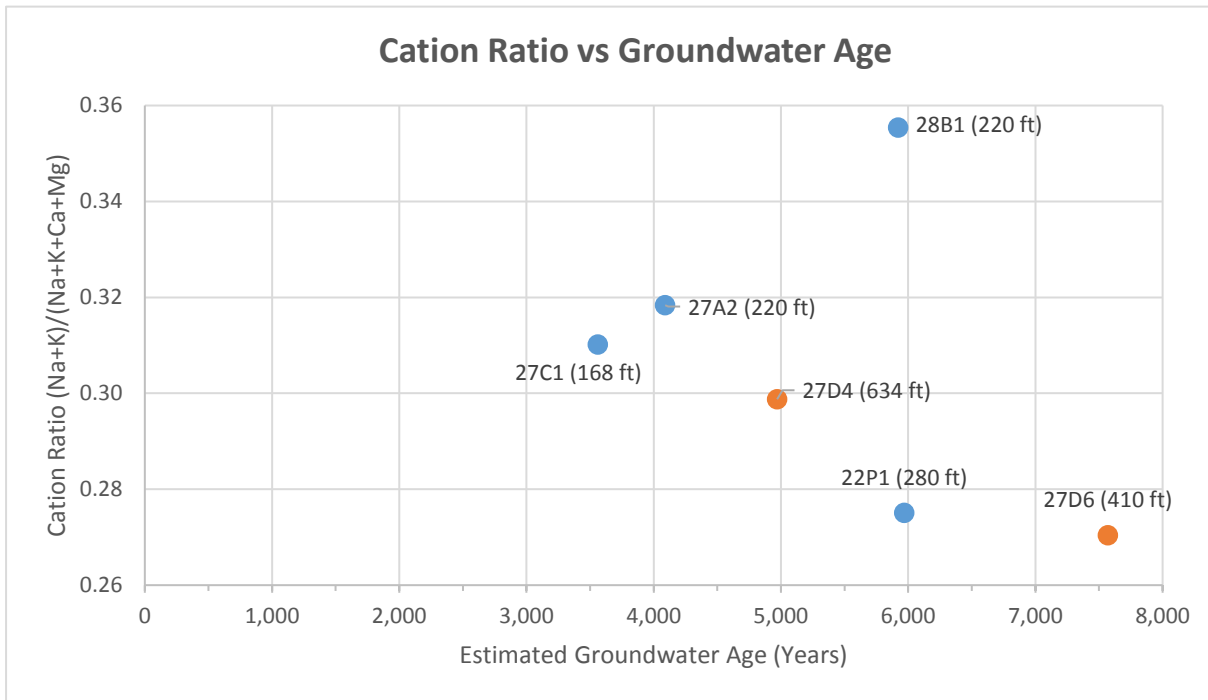
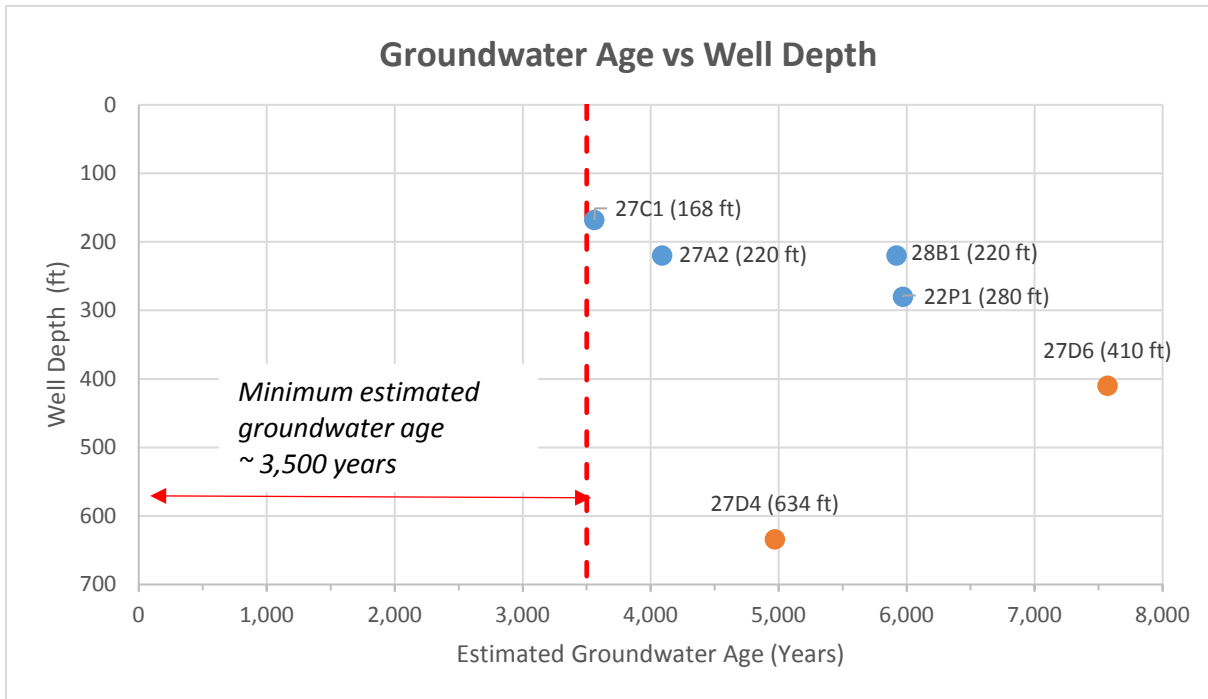
**Figure 14**

**Groundwater Cation Ratios and Silicon Concentrations vs Well Depth**

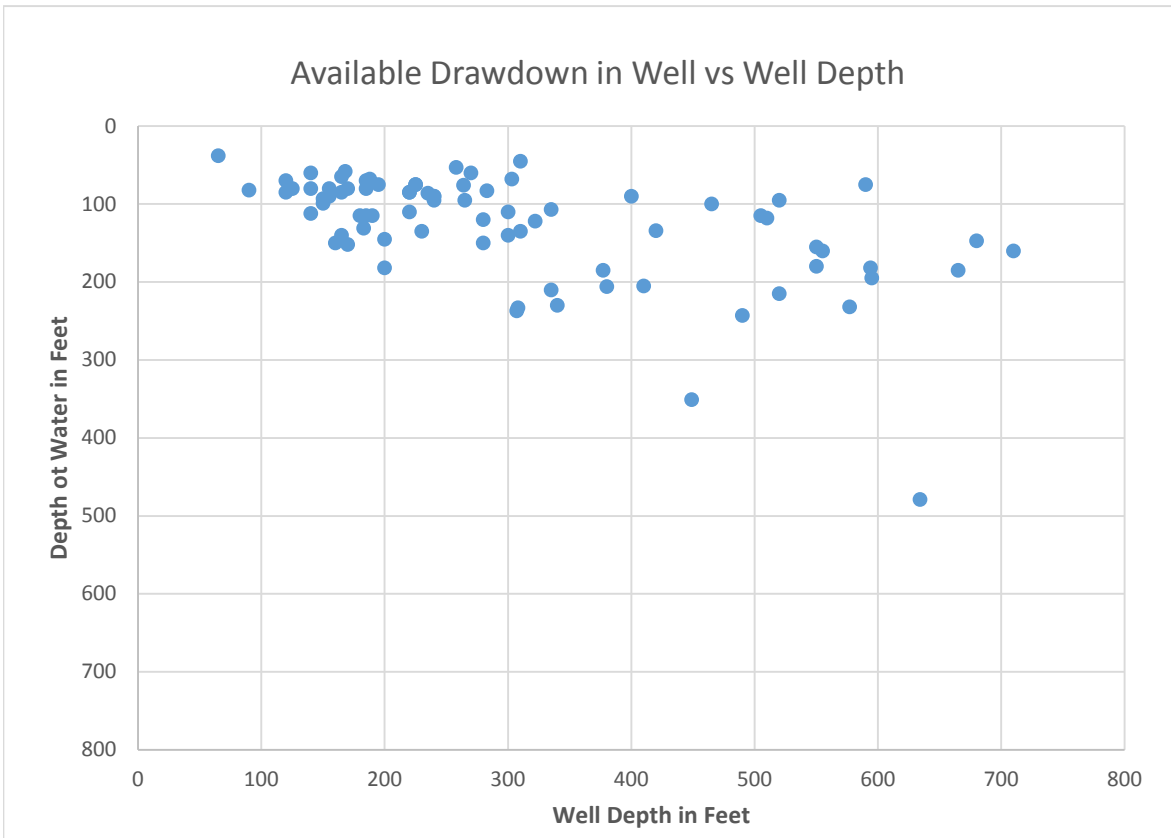
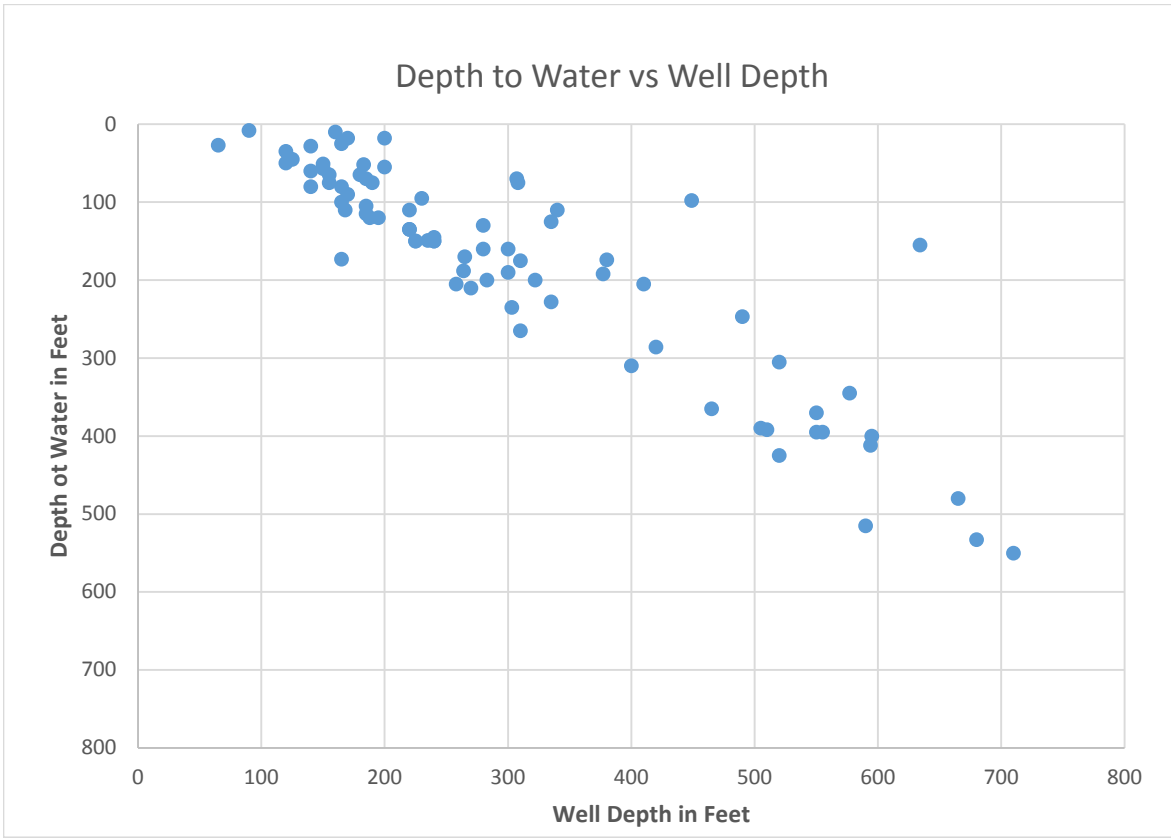


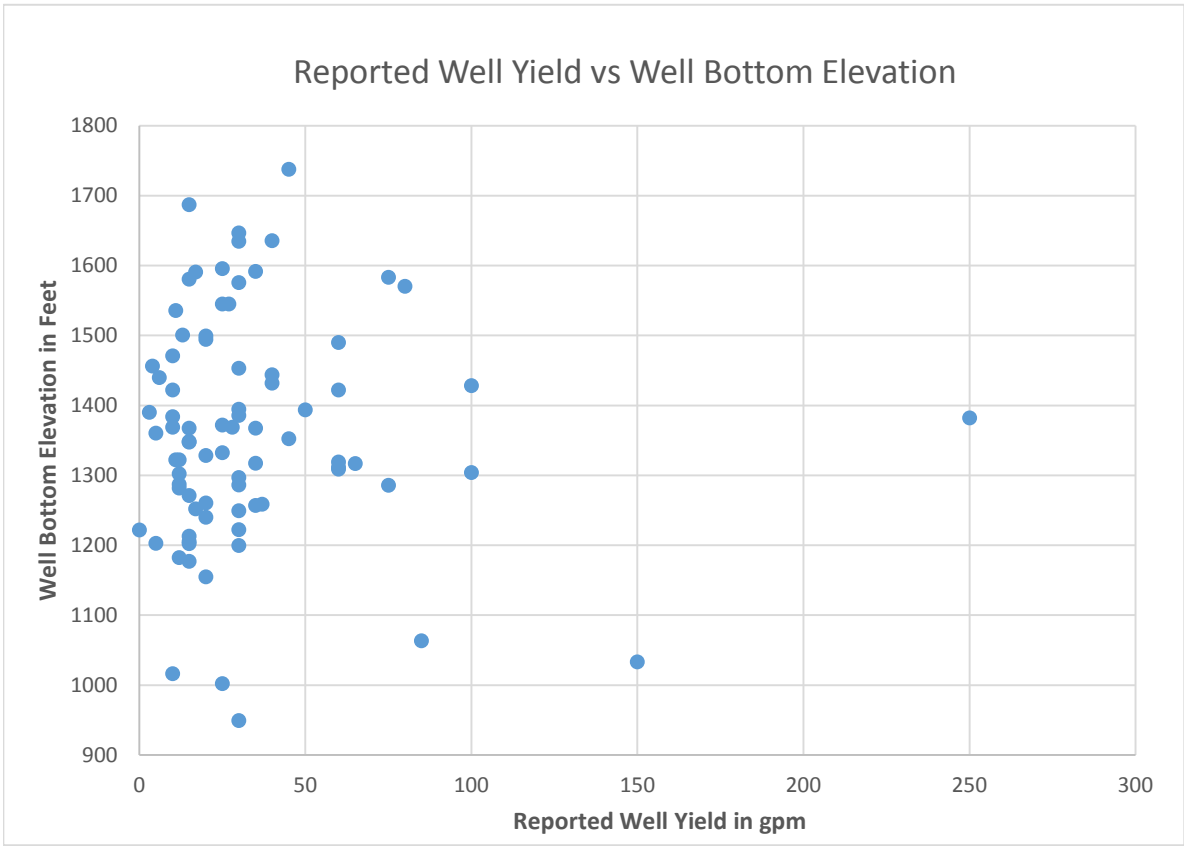
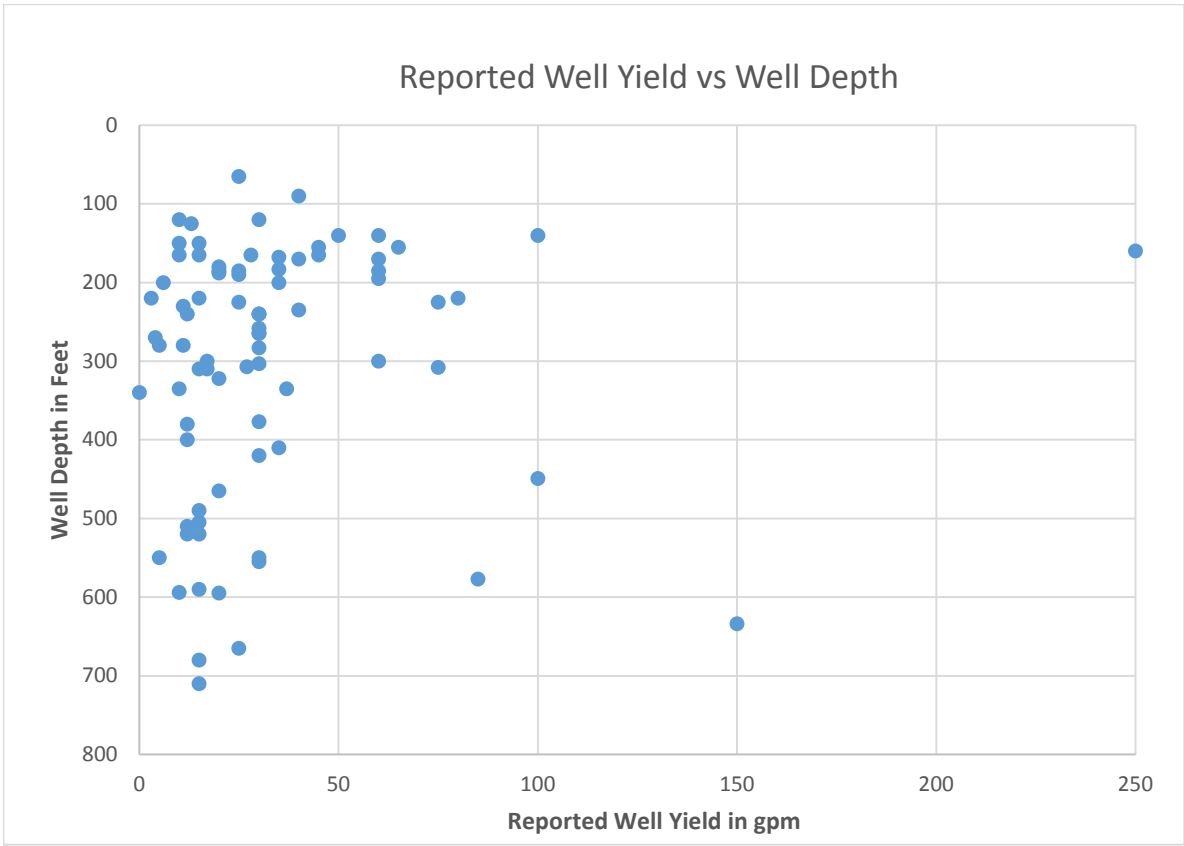
**Figure 15**

**Groundwater Chloride and Nitrate Concentrations vs Well Depth**

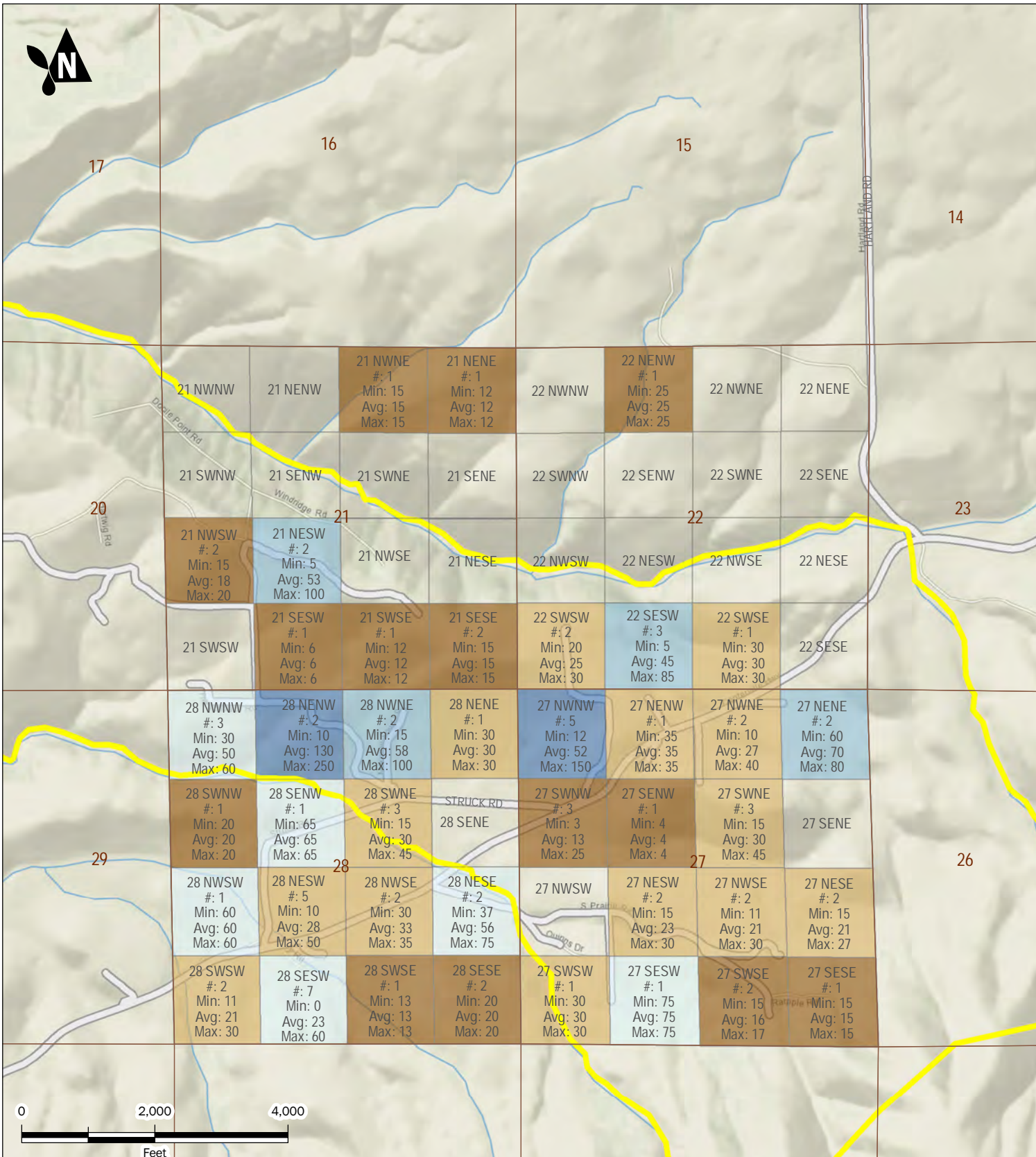


**Figure 16**  
**Groundwater Age vs Well Depth**  
**and Cation Ratio**





**Figure 18**  
**Reported Well Yield**  
**vs Well Depth**



## Reported Well Yield Distribution in Study Area

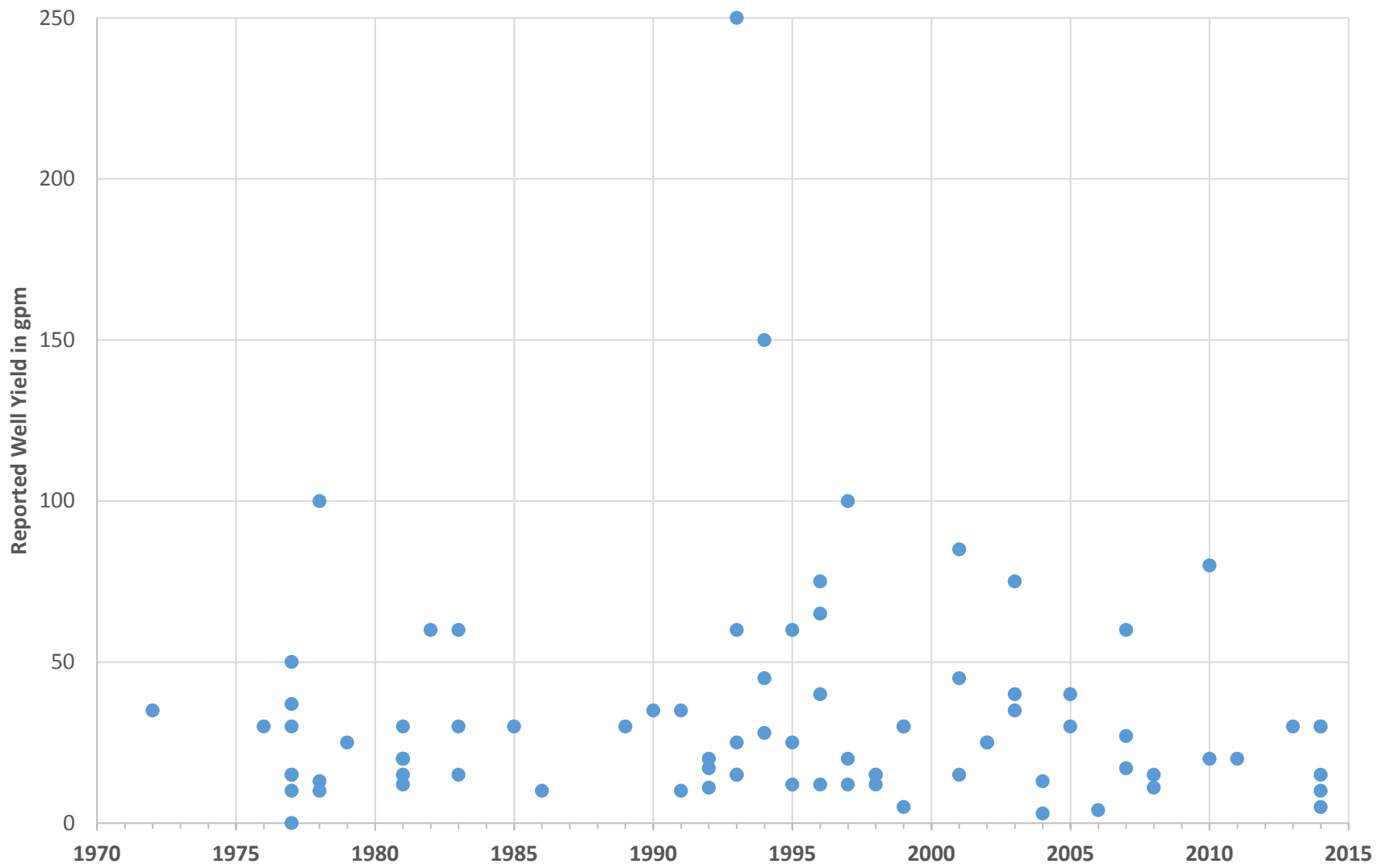
Knight-Dillacort Area Hydrogeologic Assessment  
WRIA 30, Washington



JUL-2015  
PROJECT NO.  
090045-17B-01

BY: MML / EAC  
REVISED BY: ---

FIGURE NO.  
**19**



**Figure 20**  
**Reported Well Yield vs**  
**Year of Well Installation**

## **APPENDIX A**

### **Laboratory Certificates of Analysis for Groundwater Analyses**



**Analytical Resources, Incorporated**  
Analytical Chemists and Consultants

28 April 2015

Dave Rugh  
Aspect Consulting  
401 Second Avenue South, Suite 201  
Seattle, WA 98104

**RE: WRIA 30, 070024**  
**ARI Job: AEL6**

Dear Dave:


Please find enclosed the original chain of custody (COC) record and the final results for the samples from the project referenced above. Analytical Resources, Inc. accepted six water samples on April 16, 2015. The samples were analyzed for Total metals, dissolved silicon and conventional parameters as requested.

No analytical complications were noted.

An electronic copy of these reports and all associated raw data will be kept on file at ARI. If you have questions or require additional information, please feel free to contact me at your convenience.

Sincerely,

ANALYTICAL RESOURCES, INC.

  
Mark D. Harris  
Project Manager  
206/695-6210  
[markh@arilabs.com](mailto:markh@arilabs.com)

Enclosures

cc: file AEL6

MDH/mdh

# Chain of Custody Record & Laboratory Analysis Request

ARI Assigned Number: **AEL6** Turn-around Requested: \_\_\_\_\_ of \_\_\_\_\_ Page \_\_\_\_\_

ARI Client Company: **Aspect Consulting** Phone: **206-838-5837** Date: **4/16/15** Ice Present?

Client Contact: **Dave Rugh** No. of Coolers: \_\_\_\_\_ Cooler Temps: \_\_\_\_\_

Client Project Name: **WRFA 30** **WRIA 30** Analysis Requested: \_\_\_\_\_

Client Project #: **070024** Samplers: **SMB**

Sample ID	Date	Time	Matrix	No Containers
27A2-041515	4/15/15	0855	Water	4
27D6-041515		1040		
28B1-041515		1220		
22P1-041515		1345		
27C1-041515		1510		
27D4-041515		1600		

Comments/Special Instructions	Relinquished by		Received by	
	(Signature)	Date & Time	(Signature)	Date & Time
Samples placed in bags due to streaking labels. Bags have sample ID written on front.	<i>Simon Butler</i>	4/16/15 1150	<i>[Signature]</i>	
	Simon Butler Company: Aspect		[Signature] Printed Name: Rich Nelson Company: ARI	

**Limits of Liability:** ARI will perform all requested services in accordance with appropriate methodology following ARI Standard Operating Procedures and the ARI Quality Assurance Program. This program meets standards for the industry. The total liability of ARI, its officers, agents, employees, or successors, arising out of or in connection with the requested services, shall not exceed the invoiced amount for said services. The acceptance by the client of a proposal for services by ARI release ARI from any liability in excess thereof, notwithstanding any provision to the contrary in any contract, purchase order or co-signed agreement between ARI and the Client.

**Sample Retention Policy:** All samples submitted to ARI will be appropriately discarded no sooner than 90 days after receipt or 60 days after submission of hardcopy data, whichever is longer, unless alternate retention schedules have been established by work-order or contract.



Analytical Resources, Incorporated  
Analytical Chemists and Consultants  
4611 South 134th Place, Suite 100  
Tukwila, WA 98168  
206-695-6200 206-695-6201 (fax)

APR 16 2015 11:50 AM



# Cooler Receipt Form

ARI Client: Aspect

Project Name: WR-IA 30

COC No(s) \_\_\_\_\_ NA

Delivered by Fed-Ex UPS Courier Hand Delivered Other \_\_\_\_\_

Assigned ARI Job No AEL6

Tracking No \_\_\_\_\_ NA

**Preliminary Examination Phase:**

Were intact, properly signed and dated custody seals attached to the outside of to cooler? YES  NO

Were custody papers included with the cooler? ..  YES  NO

Were custody papers properly filled out (ink, signed, etc.) .....  YES  NO

Temperature of Cooler(s) (°C) (recommended 2.0-6.0 °C for chemistry)

Time 1400 \_\_\_\_\_ 4.1

If cooler temperature is out of compliance fill out form 00070F

Temp Gun ID# 9087795C

Cooler Accepted by [Signature] Date 4/16/15 Time 1335

**Complete custody forms and attach all shipping documents**

**Log-In Phase:**

Was a temperature blank included in the cooler? ..... YES  NO

What kind of packing material was used? ... Bubble Wrap Wet Ice Get Packs Baggies Foam Block Paper Other \_\_\_\_\_

Was sufficient ice used (if appropriate)? ..... NA  YES  NO

Were all bottles sealed in individual plastic bags? .....  YES  NO

Did all bottles arrive in good condition (unbroken)? .....  YES  NO

Were all bottle labels complete and legible? .....  YES  NO

Did the number of containers listed on COC match with the number of containers received? .....  YES  NO

Did all bottle labels and tags agree with custody papers? ...  YES  NO

Were all bottles used correct for the requested analyses? .....  YES  NO

Do any of the analyses (bottles) require preservation? (attach preservation sheet, excluding VOCs) . NA  YES  NO

Were all VOC vials free of air bubbles? .....  NA  YES  NO

Was sufficient amount of sample sent in each bottle? .....  YES  NO

Date VOC Trip Blank was made at ARI.....  NA \_\_\_\_\_

Was Sample Split by ARI  NA YES Date/Time \_\_\_\_\_ Equipment: \_\_\_\_\_ Split by \_\_\_\_\_

Samples Logged by JB Date 4.16.15 Time 1510

**\*\* Notify Project Manager of discrepancies or concerns \*\***

Sample ID on Bottle	Sample ID on COC	Sample ID on Bottle	Sample ID on COC

**Additional Notes, Discrepancies, & Resolutions:**

By \_\_\_\_\_ Date \_\_\_\_\_

			Small → "sm" (< 2 mm) Peabubbles → "pb" (2 to < 4 mm) Large → "lg" (4 to < 6 mm) Headspace → "hs" (> 6 mm)
--	--	--	---

PRESERVATION VERIFICATION 04/16/15

Page 1 of 1



ARI Job No: AEL6

PC: Mark

VTSR: 04/16/15

Inquiry Number: NONE  
 Analysis Requested: 04/16/15  
 Contact: Rugh, David  
 Client: Aspect Consulting  
 Logged by: TS  
 Sample Set Used: Yes-481  
 Validatable Package: No  
 Deliverables:

Project #: 070024  
 Project: WRIA30  
 Sample Site:  
 SDG No:  
 Analytical Protocol: In-house

LOGNUM ARI ID	CLIENT ID	CN >12	WAD >12	NH3 <2	COD <2	ECG <2	MET <2	PHEN <2	PHOS <2	TKN <2	NO23 <2	TOC <2	S2 >9	TPHD <2	Fe2+ <2	DMET DOC FLT FLT	PARAMETER	ADJUSTED TO	LOT NUMBER	AMOUNT ADDED	DATE/BY
15-7498 AEL6A	27A2-041515						TOT (6.5)														
15-7499 AEL6B	27D6-041515						TOT														
15-7500 AEL6C	2881-041515						TOT														
15-7501 AEL6D	22P1-041515						TOT														
15-7502 AEL6E	27C1-041515						TOT														
15-7503 AEL6F	27D4-041515						TOT (6.5)														
15-7509 AEL6G	27A2-041515						DIS F									N					
15-7510 AEL6H	27D6-041515						DIS									N					
15-7511 AEL6I	2831-041515						DIS									N					
15-7512 AEL6J	22P1-041515						DIS									N					
15-7513 AEL6K	27C1-041515						DIS									N					
15-7514 AEL6L	27D4-041515						DIS F									N					

F - Fail

Checked By TS Date 4.16.15

000000

# Sample ID Cross Reference Report



ARI Job No: AEL6  
Client: Aspect Consulting  
Project Event: 070024  
Project Name: WRIA30

Sample ID	ARI Lab ID	ARI LIMS ID	Matrix	Sample Date/Time	VTSR
1. 27A2-041515	AEL6A	15-7498	Water	04/15/15 08:55	04/16/15 13:35
2. 27D6-041515	AEL6B	15-7499	Water	04/15/15 10:40	04/16/15 13:35
3. 28B1-041515	AEL6C	15-7500	Water	04/15/15 12:20	04/16/15 13:35
4. 22P1-041515	AEL6D	15-7501	Water	04/15/15 13:45	04/16/15 13:35
5. 27C1-041515	AEL6E	15-7502	Water	04/15/15 15:10	04/16/15 13:35
6. 27D4-041515	AEL6F	15-7503	Water	04/15/15 16:20	04/16/15 13:35
7. 27A2-041515	AEL6G	15-7509	Water	04/15/15 08:55	04/16/15 13:35
8. 27D6-041515	AEL6H	15-7510	Water	04/15/15 10:40	04/16/15 13:35
9. 28B1-041515	AEL6I	15-7511	Water	04/15/15 12:20	04/16/15 13:35
10. 22P1-041515	AEL6J	15-7512	Water	04/15/15 13:45	04/16/15 13:35
11. 27C1-041515	AEL6K	15-7513	Water	04/15/15 15:10	04/16/15 13:35
12. 27D4-041515	AEL6L	15-7514	Water	04/15/15 16:20	04/16/15 13:35



## Data Reporting Qualifiers

Effective 12/31/13

### Inorganic Data

- U Indicates that the target analyte was not detected at the reported concentration
- \* Duplicate RPD is not within established control limits
- B Reported value is less than the CRDL but  $\geq$  the Reporting Limit
- N Matrix Spike recovery not within established control limits
- NA Not Applicable, analyte not spiked
- H The natural concentration of the spiked element is so much greater than the concentration spiked that an accurate determination of spike recovery is not possible
- L Analyte concentration is  $\leq 5$  times the Reporting Limit and the replicate control limit defaults to  $\pm 1$  RL instead of the normal 20% RPD

### Organic Data

- U Indicates that the target analyte was not detected at the reported concentration
- \* Flagged value is not within established control limits
- B Analyte detected in an associated Method Blank at a concentration greater than one-half of ARI's Reporting Limit or 5% of the regulatory limit or 5% of the analyte concentration in the sample.
- J Estimated concentration when the value is less than ARI's established reporting limits
- D The spiked compound was not detected due to sample extract dilution
- E Estimated concentration calculated for an analyte response above the valid instrument calibration range. A dilution is required to obtain an accurate quantification of the analyte.



Analytical Resources,  
Incorporated  
Analytical Chemists and  
Consultants

- Q Indicates a detected analyte with an initial or continuing calibration that does not meet established acceptance criteria (<20%RSD, <20%Drift or minimum RRF).
- S Indicates an analyte response that has saturated the detector. The calculated concentration is not valid; a dilution is required to obtain valid quantification of the analyte
- NA The flagged analyte was not analyzed for
- NR Spiked compound recovery is not reported due to chromatographic interference
- NS The flagged analyte was not spiked into the sample
- M Estimated value for an analyte detected and confirmed by an analyst but with low spectral match parameters. This flag is used only for GC-MS analyses
- N The analysis indicates the presence of an analyte for which there is presumptive evidence to make a "tentative identification"
- Y The analyte is not detected at or above the reported concentration. The reporting limit is raised due to chromatographic interference. The Y flag is equivalent to the U flag with a raised reporting limit.
- EMPC Estimated Maximum Possible Concentration (EMPC) defined in EPA Statement of Work DLM02.2 as a value "calculated for 2,3,7,8-substituted isomers for which the quantitation and /or confirmation ion(s) has signal to noise in excess of 2.5, but does not meet identification criteria" **(Dioxin/Furan analysis only)**
- C The analyte was positively identified on only one of two chromatographic columns. Chromatographic interference prevented a positive identification on the second column
- P The analyte was detected on both chromatographic columns but the quantified values differ by  $\geq 40\%$  RPD with no obvious chromatographic interference
- X Analyte signal includes interference from polychlorinated diphenyl ethers. **(Dioxin/Furan analysis only)**
- Z Analyte signal includes interference from the sample matrix or perfluorokerosene ions. **(Dioxin/Furan analysis only)**



**Analytical Resources,  
Incorporated**  
Analytical Chemists and  
Consultants

## **Geotechnical Data**

- A The total of all fines fractions. This flag is used to report total fines when only sieve analysis is requested and balances total grain size with sample weight.
- F Samples were frozen prior to particle size determination
- SM Sample matrix was not appropriate for the requested analysis. This normally refers to samples contaminated with an organic product that interferes with the sieving process and/or moisture content, porosity and saturation calculations
- SS Sample did not contain the proportion of "fines" required to perform the pipette portion of the grain size analysis
- W Weight of sample in some pipette aliquots was below the level required for accurate weighting

SAMPLE RESULTS-CONVENTIONALS  
AEL6-Aspect Consulting



Matrix: Water  
Data Release Authorized:  
Reported: 04/28/15

Project: WRIA30  
Event: 070024  
Date Sampled: 04/15/15  
Date Received: 04/16/15

Client ID: 27A2-041515  
ARI ID: 15-7498 AEL6A

Analyte	Date Batch	Method	Units	RL	Sample
Alkalinity	04/20/15 042015#1	SM 2320	mg/L CaCO3	1.0	88.8
Carbonate	04/20/15	SM 2320	mg/L CaCO3	1.0	< 1.0 U
Bicarbonate	04/20/15	SM 2320	mg/L CaCO3	1.0	88.8
Hydroxide	04/20/15	SM 2320	mg/L CaCO3	1.0	< 1.0 U
Chloride	04/16/15 041615#1	EPA 300.0	mg/L	0.1	2.6
Fluoride	04/16/15 041615#1	EPA 300.0	mg/L	0.1	0.2
N-Nitrate	04/16/15 041615#1	EPA 300.0	mg-N/L	0.1	0.4
Sulfate	04/16/15 041615#1	EPA 300.0	mg/L	0.1	1.7

RL Analytical reporting limit  
U Undetected at reported detection limit

SAMPLE RESULTS-CONVENTIONALS  
AEL6-Aspect Consulting



Matrix: Water  
Data Release Authorized:  
Reported: 04/28/15

Project: WRIA30  
Event: 070024  
Date Sampled: 04/15/15  
Date Received: 04/16/15

Client ID: 27D6-041515  
ARI ID: 15-7499 AEL6B

Analyte	Date Batch	Method	Units	RL	Sample
Alkalinity	04/20/15 042015#1	SM 2320	mg/L CaCO3	1.0	138
Carbonate	04/20/15	SM 2320	mg/L CaCO3	1.0	< 1.0 U
Bicarbonate	04/20/15	SM 2320	mg/L CaCO3	1.0	138
Hydroxide	04/20/15	SM 2320	mg/L CaCO3	1.0	< 1.0 U
Chloride	04/16/15 041615#1	EPA 300.0	mg/L	0.1	2.5
Fluoride	04/16/15 041615#1	EPA 300.0	mg/L	0.1	0.2
N-Nitrate	04/16/15 041615#1	EPA 300.0	mg-N/L	0.1	< 0.1 U
Sulfate	04/16/15 041615#1	EPA 300.0	mg/L	0.1	3.8

RL Analytical reporting limit  
U Undetected at reported detection limit

SAMPLE RESULTS-CONVENTIONALS  
AEL6-Aspect Consulting



Matrix: Water  
Data Release Authorized:  
Reported: 04/28/15

A handwritten signature in black ink, appearing to be 'JH' or similar, written over the 'Data Release Authorized' text.

Project: WRIA30  
Event: 070024  
Date Sampled: 04/15/15  
Date Received: 04/16/15


Client ID: 28B1-041515  
ARI ID: 15-7500 AEL6C

Analyte	Date Batch	Method	Units	RL	Sample
Alkalinity	04/20/15 042015#1	SM 2320	mg/L CaCO3	1.0	103
Carbonate	04/20/15	SM 2320	mg/L CaCO3	1.0	< 1.0 U
Bicarbonate	04/20/15	SM 2320	mg/L CaCO3	1.0	103
Hydroxide	04/20/15	SM 2320	mg/L CaCO3	1.0	< 1.0 U
Chloride	04/23/15 042315#1	EPA 300.0	mg/L	0.5	13.1
Fluoride	04/16/15 041615#1	EPA 300.0	mg/L	0.1	0.4
N-Nitrate	04/16/15 041615#1	EPA 300.0	mg-N/L	0.1	1.0
Sulfate	04/23/15 042315#1	EPA 300.0	mg/L	0.2	7.0

RL Analytical reporting limit  
U Undetected at reported detection limit

SAMPLE RESULTS-CONVENTIONALS  
AEL6-Aspect Consulting



Matrix: Water  
Data Release Authorized:   
Reported: 04/28/15

Project: WRIA30  
Event: 070024  
Date Sampled: 04/15/15  
Date Received: 04/16/15

Client ID: 22P1-041515  
ARI ID: 15-7501 AEL6D

Analyte	Date Batch	Method	Units	RL	Sample
Alkalinity	04/20/15 042015#1	SM 2320	mg/L CaCO3	1.0	129
Carbonate	04/20/15	SM 2320	mg/L CaCO3	1.0	< 1.0 U
Bicarbonate	04/20/15	SM 2320	mg/L CaCO3	1.0	129
Hydroxide	04/20/15	SM 2320	mg/L CaCO3	1.0	< 1.0 U
Chloride	04/16/15 041615#1	EPA 300.0	mg/L	0.1	3.2
Fluoride	04/16/15 041615#1	EPA 300.0	mg/L	0.1	0.2
N-Nitrate	04/16/15 041615#1	EPA 300.0	mg-N/L	0.1	< 0.1 U
Sulfate	04/23/15 042315#1	EPA 300.0	mg/L	0.5	21.0

RL Analytical reporting limit  
U Undetected at reported detection limit

SAMPLE RESULTS-CONVENTIONALS  
AEL6-Aspect Consulting



Matrix: Water  
Data Release Authorized:  
Reported: 04/28/15

Project: WRIA30  
Event: 070024  
Date Sampled: 04/15/15  
Date Received: 04/16/15

Client ID: 27C1-041515  
ARI ID: 15-7502 AEL6E

Analyte	Date Batch	Method	Units	RL	Sample
Alkalinity	04/20/15 042015#1	SM 2320	mg/L CaCO3	1.0	113
Carbonate	04/20/15	SM 2320	mg/L CaCO3	1.0	< 1.0 U
Bicarbonate	04/20/15	SM 2320	mg/L CaCO3	1.0	113
Hydroxide	04/20/15	SM 2320	mg/L CaCO3	1.0	< 1.0 U
Chloride	04/16/15 041615#1	EPA 300.0	mg/L	0.1	4.6
Fluoride	04/16/15 041615#1	EPA 300.0	mg/L	0.1	0.2
N-Nitrate	04/16/15 041615#1	EPA 300.0	mg-N/L	0.1	0.9
Sulfate	04/16/15 041615#1	EPA 300.0	mg/L	0.1	1.6

RL Analytical reporting limit  
U Undetected at reported detection limit

SAMPLE RESULTS-CONVENTIONALS  
AEL6-Aspect Consulting



Matrix: Water  
Data Release Authorized:  
Reported: 04/28/15

A handwritten signature in black ink, appearing to be 'JFK', is written over the 'Data Release Authorized' text.

Project: WRIA30  
Event: 070024  
Date Sampled: 04/15/15  
Date Received: 04/16/15


Client ID: 27D4-041515  
ARI ID: 15-7503 AEL6F

Analyte	Date Batch	Method	Units	RL	Sample
Alkalinity	04/20/15 042015#1	SM 2320	mg/L CaCO3	1.0	124
Carbonate	04/20/15	SM 2320	mg/L CaCO3	1.0	< 1.0 U
Bicarbonate	04/20/15	SM 2320	mg/L CaCO3	1.0	124
Hydroxide	04/20/15	SM 2320	mg/L CaCO3	1.0	< 1.0 U
Chloride	04/16/15 041615#1	EPA 300.0	mg/L	0.1	3.8
Fluoride	04/16/15 041615#1	EPA 300.0	mg/L	0.1	0.2
N-Nitrate	04/16/15 041615#1	EPA 300.0	mg-N/L	0.1	0.2
Sulfate	04/16/15 041615#1	EPA 300.0	mg/L	0.1	3.4

RL Analytical reporting limit  
U Undetected at reported detection limit

METHOD BLANK RESULTS-CONVENTIONALS  
AEL6-Aspect Consulting



Matrix: Water  
Data Release Authorized:   
Reported: 04/28/15

Project: WRIA30  
Event: 070024  
Date Sampled: NA  
Date Received: NA

Analyte	Method	Date	Units	Blank	ID
Chloride	EPA 300.0	04/16/15	mg/L	< 0.1 U	
		04/23/15		< 0.1 U	
Fluoride	EPA 300.0	04/16/15	mg/L	< 0.1 U	
N-Nitrate	EPA 300.0	04/16/15	mg-N/L	< 0.1 U	
Sulfate	EPA 300.0	04/16/15	mg/L	< 0.1 U	
		04/23/15		< 0.1 U	

STANDARD REFERENCE RESULTS-CONVENTIONALS  
AEL6-Aspect Consulting



Matrix: Water  
Data Release Authorized:  
Reported: 04/28/15

A handwritten signature in black ink, appearing to be 'JW' or similar, written over the 'Data Release Authorized' text.

Project: WRIA30  
Event: 070024  
Date Sampled: NA  
Date Received: NA

Analyte/SRM ID	Method	Date	Units	SRM	True Value	Recovery
Alkalinity ERA #P224-506	SM 2320	04/20/15	mg/L CaCO3	60.9	61.7	98.7%
Chloride ERA #290313	EPA 300.0	04/16/15 04/23/15	mg/L	2.8 3.0	3.0 3.0	93.3% 100.0%
Fluoride ERA 330613	EPA 300.0	04/16/15	mg/L	2.8	3.0	93.3%
N-Nitrate ERA #320614	EPA 300.0	04/16/15	mg-N/L	2.8	3.0	93.3%
Sulfate ERA 131013	EPA 300.0	04/16/15 04/23/15	mg/L	2.7 3.0	3.0 3.0	90.0% 100.0%

REPLICATE RESULTS-CONVENTIONALS  
AEL6-Aspect Consulting



Matrix: Water  
Data Release Authorized:  
Reported: 04/28/15

A handwritten signature in black ink, appearing to be 'J. J.', written over the 'Data Release Authorized' line.

Project: WRIA30  
Event: 070024  
Date Sampled: 04/15/15  
Date Received: 04/16/15

Analyte	Method	Date	Units	Sample	Replicate(s)	RPD/RSD
ARI ID: AEL6A Client ID: 27A2-041515						
Alkalinity	SM 2320	04/20/15	mg/L CaCO3	88.8	89.4	0.7%
Carbonate	SM 2320	04/20/15	mg/L CaCO3	< 1.0	< 1.0	NA
Bicarbonate	SM 2320	04/20/15	mg/L CaCO3	88.8	89.4	0.7%
Hydroxide	SM 2320	04/20/15	mg/L CaCO3	< 1.0	< 1.0	NA

**INORGANICS ANALYSIS DATA SHEET**

**TOTAL METALS**

Page 1 of 1


Sample ID: 27A2-041515

**SAMPLE**

Lab Sample ID: AEL6A

LIMS ID: 15-7498

Matrix: Water

Data Release Authorized: 

Reported: 04/23/15

QC Report No: AEL6-Aspect Consulting

Project: WRIA30

070024

Date Sampled: 04/15/15

Date Received: 04/16/15

Prep Meth	Prep Date	Analysis Method	Analysis Date	CAS Number	Analyte	LOQ	mg/L	Q
3010A	04/20/15	6010C	04/22/15	7440-70-2	Calcium	0.05	16.1	
3010A	04/20/15	6010C	04/22/15	7439-95-4	Magnesium	0.05	7.88	
3010A	04/20/15	6010C	04/22/15	7440-09-7	Potassium	0.5	2.4	
3010A	04/20/15	6010C	04/22/15	7440-23-5	Sodium	0.5	8.8	

U-Analyte undetected at given LOQ

LOQ-Reporting Limit

**INORGANICS ANALYSIS DATA SHEET**

**TOTAL METALS**

Page 1 of 1

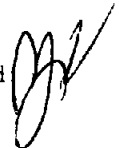
Sample ID: 27A2-041515

DUPLICATE

Lab Sample ID: AEL6A

LIMS ID: 15-7498

Matrix: Water

Data Release Authorized 

Reported: 04/23/15

QC Report No: AEL6-Aspect Consulting

Project: WRIA30

070024

Date Sampled: 04/15/15

Date Received: 04/16/15

**MATRIX DUPLICATE QUALITY CONTROL REPORT**

Analyte	Analysis Method	Sample	Duplicate	RPD	Control Limit	Q
Calcium	6010C	16.1	16.3	1.2%	+/- 20%	
Magnesium	6010C	7.88	7.96	1.0%	+/- 20%	
Potassium	6010C	2.4	2.5	4.1%	+/- 0.5	L
Sodium	6010C	8.8	8.8	0.0%	+/- 20%	

Reported in mg/L

\*-Control Limit Not Met

L-RPD Invalid, Limit = Detection Limit

**INORGANICS ANALYSIS DATA SHEET**

**TOTAL METALS**

Page 1 of 1

Sample ID: 27A2-041515

**MATRIX SPIKE**

Lab Sample ID: AEL6A

LIMS ID: 15-7498

Matrix: Water

Data Release Authorized: *JH*

Reported: 04/23/15

QC Report No: AEL6-Aspect Consulting

Project: WRIA30

070024

Date Sampled: 04/15/15

Date Received: 04/16/15

**MATRIX SPIKE QUALITY CONTROL REPORT**

Analyte	Analysis Method	Sample	Spike	Spike Added	% Recovery	Q
Calcium	6010C	16.1	26.4	10.0	103%	
Magnesium	6010C	7.88	18.9	10.0	110%	
Potassium	6010C	2.4	12.9	10.0	105%	
Sodium	6010C	8.8	19.6	10.0	108%	

Reported in mg/L

N-Control Limit Not Met

H-% Recovery Not Applicable, Sample Concentration Too High

NA-Not Applicable, Analyte Not Spiked

Percent Recovery Limits: 75-125%

**INORGANICS ANALYSIS DATA SHEET**

**TOTAL METALS**

Page 1 of 1


Sample ID: 27D6-041515

SAMPLE

Lab Sample ID: AEL6B

LIMS ID: 15-7499

Matrix: Water

Data Release Authorized: 

Reported: 04/23/15

QC Report No: AEL6-Aspect Consulting

Project: WRIA30

070024

Date Sampled: 04/15/15

Date Received: 04/16/15

Prep Meth	Prep Date	Analysis Method	Analysis Date	CAS Number	Analyte	LOQ	mg/L	Q
3010A	04/20/15	6010C	04/22/15	7440-70-2	Calcium	0.05	23.5	
3010A	04/20/15	6010C	04/22/15	7439-95-4	Magnesium	0.05	14.0	
3010A	04/20/15	6010C	04/22/15	7440-09-7	Potassium	0.5	2.6	
3010A	04/20/15	6010C	04/22/15	7440-23-5	Sodium	0.5	11.3	

U-Analyte undetected at given LOQ

LOQ-Reporting Limit

**INORGANICS ANALYSIS DATA SHEET**

**TOTAL METALS**

Page 1 of 1

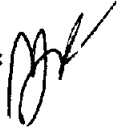
Sample ID: 28B1-041515

SAMPLE

Lab Sample ID: AEL6C

LIMS ID: 15-7500

Matrix: Water

Data Release Authorized: 

Reported: 04/23/15

QC Report No: AEL6-Aspect Consulting

Project: WRIA30

070024

Date Sampled: 04/15/15

Date Received: 04/16/15

Prep Meth	Prep Date	Analysis Method	Analysis Date	CAS Number	Analyte	LOQ	mg/L	Q
3010A	04/20/15	6010C	04/22/15	7440-70-2	Calcium	0.05	19.8	
3010A	04/20/15	6010C	04/22/15	7439-95-4	Magnesium	0.05	11.4	
3010A	04/20/15	6010C	04/22/15	7440-09-7	Potassium	0.5	2.6	
3010A	04/20/15	6010C	04/22/15	7440-23-5	Sodium	0.5	14.6	

U-Analyte undetected at given LOQ

LOQ-Reporting Limit

**INORGANICS ANALYSIS DATA SHEET**

**TOTAL METALS**

Page 1 of 1

Sample ID: 22P1-041515  
SAMPLE

Lab Sample ID: AEL6D  
LIMS ID: 15-7501  
Matrix: Water  
Data Release Authorized:  
Reported: 04/23/15



QC Report No: AEL6-Aspect Consulting  
Project: WRIA30  
070024  
Date Sampled: 04/15/15  
Date Received: 04/16/15

Prep Meth	Prep Date	Analysis Method	Analysis Date	CAS Number	Analyte	LOQ	mg/L	Q
3010A	04/20/15	6010C	04/22/15	7440-70-2	Calcium	0.05	24.4	
3010A	04/20/15	6010C	04/22/15	7439-95-4	Magnesium	0.05	15.4	
3010A	04/20/15	6010C	04/22/15	7440-09-7	Potassium	0.5	3.4	
3010A	04/20/15	6010C	04/22/15	7440-23-5	Sodium	0.5	11.7	

U-Analyte undetected at given LOQ  
LOQ-Reporting Limit

**INORGANICS ANALYSIS DATA SHEET**

**TOTAL METALS**


Page 1 of 1

Sample ID: 27C1-041515  
SAMPLE

Lab Sample ID: AEL6E

LIMS ID: 15-7502

Matrix: Water

Data Release Authorized: 

Reported: 04/23/15

QC Report No: AEL6-Aspect Consulting

Project: WRIA30

070024

Date Sampled: 04/15/15

Date Received: 04/16/15

Prep Meth	Prep Date	Analysis Method	Analysis Date	CAS Number	Analyte	LOQ	mg/L	Q
3010A	04/20/15	6010C	04/22/15	7440-70-2	Calcium	0.05	21.0	
3010A	04/20/15	6010C	04/22/15	7439-95-4	Magnesium	0.05	9.91	
3010A	04/20/15	6010C	04/22/15	7440-09-7	Potassium	0.5	2.3	
3010A	04/20/15	6010C	04/22/15	7440-23-5	Sodium	0.5	11.6	

U-Analyte undetected at given LOQ  
LOQ-Reporting Limit

**INORGANICS ANALYSIS DATA SHEET**

**TOTAL METALS**


Page 1 of 1

Sample ID: 27D4-041515  
SAMPLE

Lab Sample ID: AEL6F

LIMS ID: 15-7503

Matrix: Water

Data Release Authorized: 

Reported: 04/23/15

QC Report No: AEL6-Aspect Consulting

Project: WRIA30

070024

Date Sampled: 04/15/15

Date Received: 04/16/15


Prep Meth	Prep Date	Analysis Method	Analysis Date	CAS Number	Analyte	LOQ	mg/L	Q
3010A	04/20/15	6010C	04/22/15	7440-70-2	Calcium	0.05	22.2	
3010A	04/20/15	6010C	04/22/15	7439-95-4	Magnesium	0.05	11.6	
3010A	04/20/15	6010C	04/22/15	7440-09-7	Potassium	0.5	3.2	
3010A	04/20/15	6010C	04/22/15	7440-23-5	Sodium	0.5	11.2	

U-Analyte undetected at given LOQ

LOQ-Reporting Limit

**INORGANICS ANALYSIS DATA SHEET**  
**DISSOLVED METALS**  
Page 1 of 1

Sample ID: 27A2-041515  
SAMPLE

Lab Sample ID: AEL6G  
LIMS ID: 15-7509  
Matrix: Water  
Data Release Authorized:   
Reported: 04/23/15

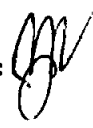
QC Report No: AEL6-Aspect Consulting  
Project: WRIA30  
070024  
Date Sampled: 04/15/15  
Date Received: 04/16/15

Prep Meth	Prep Date	Analysis Method	Analysis Date	CAS Number	Analyte	LOQ	mg/L	Q
6010C	04/20/15	6010C	04/22/15	7440-21-3	Silicon	0.06	27.0	

U-Analyte undetected at given LOQ  
LOQ-Limit of Quantitation

**INORGANICS ANALYSIS DATA SHEET**  
**DISSOLVED METALS**  
Page 1 of 1

Sample ID: 27A2-041515  
DUPLICATE

Lab Sample ID: AEL6G  
LIMS ID: 15-7509  
Matrix: Water  
Data Release Authorized:   
Reported: 04/23/15

QC Report No: AEL6-Aspect Consulting  
Project: WRIA30  
070024  
Date Sampled: 04/15/15  
Date Received: 04/16/15

**MATRIX DUPLICATE QUALITY CONTROL REPORT**

Analyte	Analysis Method	Sample	Duplicate	RPD	Control Limit	Q
Silicon	6010C	27.0	26.9	0.4%	+/- 20%	

Reported in mg/L

\*-Control Limit Not Met  
L-RPD Invalid, Limit = Detection Limit

**INORGANICS ANALYSIS DATA SHEET**

**DISSOLVED METALS**

Page 1 of 1

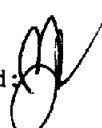
Sample ID: 27A2-041515

MATRIX SPIKE

Lab Sample ID: AEL6G

LIMS ID: 15-7509

Matrix: Water

Data Release Authorized: 

Reported: 04/23/15

QC Report No: AEL6-Aspect Consulting

Project: WRIA30

070024

Date Sampled: 04/15/15

Date Received: 04/16/15

**MATRIX SPIKE QUALITY CONTROL REPORT**

Analyte	Analysis Method	Sample	Spike	Spike Added	% Recovery	Q
Silicon	6010C	27.0	36.0	10.0	90.0%	

Reported in mg/L

N-Control Limit Not Met

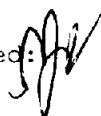
H-% Recovery Not Applicable, Sample Concentration Too High

NA-Not Applicable, Analyte Not Spiked

Percent Recovery Limits: 75-125%

**INORGANICS ANALYSIS DATA SHEET**  
**DISSOLVED METALS**  
 Page 1 of 1

Sample ID: 27D6-041515  
**SAMPLE**

Lab Sample ID: AEL6H  
 LIMS ID: 15-7510  
 Matrix: Water  
 Data Release Authorized:   
 Reported: 04/23/15


QC Report No: AEL6-Aspect Consulting  
 Project: WRIA30  
 070024  
 Date Sampled: 04/15/15  
 Date Received: 04/16/15

Prep Meth	Prep Date	Analysis Method	Analysis Date	CAS Number	Analyte	LOQ	mg/L	Q
6010C	04/20/15	6010C	04/22/15	7440-21-3	Silicon	0.06	19.7	

U-Analyte undetected at given LOQ  
 LOQ-Limit of Quantitation

**INORGANICS ANALYSIS DATA SHEET**  
**DISSOLVED METALS**  
Page 1 of 1

Sample ID: 28B1-041515  
SAMPLE

Lab Sample ID: AEL6I  
LIMS ID: 15-7511  
Matrix: Water  
Data Release Authorized:   
Reported: 04/23/15

QC Report No: AEL6-Aspect Consulting  
Project: WRIA30  
070024  
Date Sampled: 04/15/15  
Date Received: 04/16/15

Prep Meth	Prep Date	Analysis Method	Analysis Date	CAS Number	Analyte	LOQ	mg/L	Q
6010C	04/20/15	6010C	04/22/15	7440-21-3	Silicon	0.06	26.1	

U-Analyte undetected at given LOQ  
LOQ-Limit of Quantitation

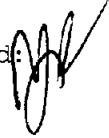
**INORGANICS ANALYSIS DATA SHEET**

**DISSOLVED METALS**

Page 1 of 1

Sample ID: 22P1-041515  
SAMPLE

Lab Sample ID: AEL6J  
LIMS ID: 15-7512  
Matrix: Water  
Data Release Authorized:  
Reported: 04/23/15



QC Report No: AEL6-Aspect Consulting  
Project: WRIA30  
070024  
Date Sampled: 04/15/15  
Date Received: 04/16/15

Prep Meth	Prep Date	Analysis Method	Analysis Date	CAS Number	Analyte	LOQ	mg/L	Q
6010C	04/20/15	6010C	04/22/15	7440-21-3	Silicon	0.06	22.1	

U-Analyte undetected at given LOQ  
LOQ-Limit of Quantitation

**INORGANICS ANALYSIS DATA SHEET**

**DISSOLVED METALS**


Page 1 of 1

Sample ID: 27C1-041515  
SAMPLE

Lab Sample ID: AEL6K

LIMS ID: 15-7513

Matrix: Water

Data Release Authorized: 

Reported: 04/23/15

QC Report No: AEL6-Aspect Consulting

Project: WRIA30

070024

Date Sampled: 04/15/15

Date Received: 04/16/15

Prep Meth	Prep Date	Analysis Method	Analysis Date	CAS Number	Analyte	LOQ	mg/L	Q
6010C	04/20/15	6010C	04/22/15	7440-21-3	Silicon	0.06	28.5	

U-Analyte undetected at given LOQ  
LOQ-Limit of Quantitation

**INORGANICS ANALYSIS DATA SHEET**

**DISSOLVED METALS**


Page 1 of 1

Sample ID: 27D4-041515  
SAMPLE

Lab Sample ID: AEL6L

LIMS ID: 15-7514

Matrix: Water

Data Release Authorized: 

Reported: 04/23/15

QC Report No: AEL6-Aspect Consulting

Project: WRIA30

070024

Date Sampled: 04/15/15

Date Received: 04/16/15

Prep Meth	Prep Date	Analysis Method	Analysis Date	CAS Number	Analyte	LOQ	mg/L	Q
6010C	04/20/15	6010C	04/22/15	7440-21-3	Silicon	0.06	23.4	

U-Analyte undetected at given LOQ  
LOQ-Limit of Quantitation

**INORGANICS ANALYSIS DATA SHEET**

**TOTAL METALS**

**Sample ID: METHOD BLANK**

Page 1 of 1

Lab Sample ID: AEL6MB


QC Report No: AEL6-Aspect Consulting

LIMS ID: 15-7503

Project: WRIA30

Matrix: Water

070024

Data Release Authorized: 

Date Sampled: NA

Reported: 04/23/15

Date Received: NA

Prep Meth	Prep Date	Analysis Method	Analysis Date	CAS Number	Analyte	LOQ	mg/L	Q
3010A	04/20/15	6010C	04/22/15	7440-70-2	Calcium	0.05	0.05	U
3010A	04/20/15	6010C	04/22/15	7439-95-4	Magnesium	0.05	0.05	U
3010A	04/20/15	6010C	04/22/15	7440-09-7	Potassium	0.5	0.5	U
3010A	04/20/15	6010C	04/22/15	7440-23-5	Sodium	0.5	0.5	U

U-Analyte undetected at given LOQ  
LOQ-Reporting Limit

**INORGANICS ANALYSIS DATA SHEET**

**TOTAL METALS**

**Sample ID: LAB CONTROL**

Page 1 of 1

Lab Sample ID: AEL6LCS


QC Report No: AEL6-Aspect Consulting

LIMS ID: 15-7503

Project: WRIA30

Matrix: Water

070024

Data Release Authorized: 

Date Sampled: NA

Reported: 04/23/15

Date Received: NA

**BLANK SPIKE QUALITY CONTROL REPORT**

Analyte	Analysis Method	Spike Found	Spike Added	% Recovery	Q
Calcium	6010C	10.0	10.0	100%	
Magnesium	6010C	10.4	10.0	104%	
Potassium	6010C	10.4	10.0	104%	
Sodium	6010C	10.7	10.0	107%	

Reported in mg/L

N-Control limit not met

Control Limits: 80-120%

**INORGANICS ANALYSIS DATA SHEET**

**DISSOLVED METALS**

Sample ID: METHOD BLANK

Page 1 of 1

Lab Sample ID: AEL6MB

QC Report No: AEL6-Aspect Consulting

LIMS ID: 15-7514

Project: WRIA30

Matrix: Water

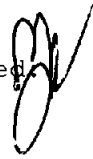
070024

Data Release Authorized

Date Sampled: NA

Reported: 04/23/15

Date Received: NA



Prep Meth	Prep Date	Analysis Method	Analysis Date	CAS Number	Analyte	LOQ	mg/L	Q
6010C	04/20/15	6010C	04/22/15	7440-21-3	Silicon	0.06	0.06	U

U-Analyte undetected at given LOQ  
LOQ-Limit of Quantitation

**INORGANICS ANALYSIS DATA SHEET**  
**DISSOLVED METALS**  
Page 1 of 1

Sample ID: LAB CONTROL

Lab Sample ID: AEL6LCS  
LIMS ID: 15-7514  
Matrix: Water  
Data Release Authorized:  
Reported: 04/23/15



QC Report No: AEL6-Aspect Consulting  
Project: WRIA30  
070024  
Date Sampled: NA  
Date Received: NA

**BLANK SPIKE QUALITY CONTROL REPORT**

Analyte	Analysis Method	Spike Found	Spike Added	% Recovery	Q
Silicon	6010C	9.22	10.0	92.2%	

Reported in mg/L

N-Control limit not met  
Control Limits: 80-120%



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www.radiocarbon.com

Darden Hood  
President

Ronald Hatfield  
Christopher Patrick  
Deputy Directors

May 7, 2015

Mr. David Rugh  
Aspect Consulting  
401 2nd Ave South  
Seattle, WA 98104  
United States

RE: Radiocarbon Dating Results For Samples 27A2-041415 , 27D6-041415 , 28B1-041415 , 22P1-041415 , 27C1-041415 , 27D4-041415

Dear Mr. Rugh:

Enclosed are the radiocarbon dating results for six samples recently sent to us. The report sheet contains the Conventional Radiocarbon Age (BP), the method used, material type, and applied pretreatments, any sample specific comments and, where applicable, the two-sigma calendar calibration range. The Conventional Radiocarbon ages have been corrected for total isotopic fractionation effects (natural and laboratory induced).

All results (excluding some inappropriate material types) which fall within the range of available calibration data are calibrated to calendar years (cal BC/AD) and calibrated radiocarbon years (cal BP). Calibration was calculated using the one of the databases associated with the 2013 INTCAL program (cited in the references on the bottom of the calibration graph page provided for each sample.) Multiple probability ranges may appear in some cases, due to short-term variations in the atmospheric <sup>14</sup>C contents at certain time periods. Looking closely at the calibration graph provided and where the BP sigma limits intercept the calibration curve will help you understand this phenomenon.

Conventional Radiocarbon Ages and sigmas are rounded to the nearest 10 years per the conventions of the 1977 International Radiocarbon Conference. When counting statistics produce sigmas lower than +/- 30 years, a conservative +/- 30 BP is cited for the result.

All work on these samples was performed in our laboratories in Miami under strict chain of custody and quality control under ISO/IEC 17025:2005 Testing Accreditation PJLA #59423 accreditation protocols. Sample, modern and blanks were all analyzed in the same chemistry lines by qualified professional technicians using identical reagents and counting parameters within our own particle accelerators. A quality assurance report is posted to your directory for each result.

Thank you for prepaying the analyses. As always, if you have any questions or would like to discuss the results, don't hesitate to contact me.

Sincerely,

  
Digital signature on file



# REPORT OF RADIOCARBON DATING ANALYSES

Mr. David Rugh

Report Date: 5/7/2015

Aspect Consulting

Material Received: 4/24/2015

Sample Data	pMC	Fmdn	d13C
Beta - 409509 SAMPLE : 27A2-041415 ANALYSIS : AMS-Standard delivery MATERIAL/PRETREATMENT : (water DIC): acidify-gas strip COMMENT: The equivalent "Apparent" radiocarbon age to the reported pMC/fMDN values is ~ 4090 BP (not adjusted for any hydro-geochemical effects on meteoric water <sup>14</sup> CO <sub>2</sub> ). Given the complex nature of groundwater DIC <sup>14</sup> chemistry, duplicate measurements within 1-2 pMC are reasonable for a single water sample. For very low DIC concentration waters (< 20 mg/L HCO <sub>3</sub> ) DIC <sup>14</sup> and waters with complex organic chemistry, results can vary significantly outside of this expectation.	60.1 +/- 0.2 pMC	0.6010 +/- 0.0022	-18.7 o/oo
Beta - 409510 SAMPLE : 27D6-041415 ANALYSIS : AMS-Standard delivery MATERIAL/PRETREATMENT : (water DIC): acidify-gas strip COMMENT: The equivalent "Apparent" radiocarbon age to the reported pMC/fMDN values is ~ 7570 BP (not adjusted for any hydro-geochemical effects on meteoric water <sup>14</sup> CO <sub>2</sub> ). Given the complex nature of groundwater DIC <sup>14</sup> chemistry, duplicate measurements within 1-2 pMC are reasonable for a single water sample. For very low DIC concentration waters (< 20 mg/L HCO <sub>3</sub> ) DIC <sup>14</sup> and waters with complex organic chemistry, results can vary significantly outside of this expectation.	39.0 +/- 0.1 pMC	0.3897 +/- 0.0014	-19.8 o/oo
Beta - 409511 SAMPLE : 28B1-041415 ANALYSIS : AMS-Standard delivery MATERIAL/PRETREATMENT : (water DIC): acidify-gas strip COMMENT: The equivalent "Apparent" radiocarbon age to the reported pMC/fMDN values is ~ 5920 BP (not adjusted for any hydro-geochemical effects on meteoric water <sup>14</sup> CO <sub>2</sub> ). Given the complex nature of groundwater DIC <sup>14</sup> chemistry, duplicate measurements within 1-2 pMC are reasonable for a single water sample. For very low DIC concentration waters (< 20 mg/L HCO <sub>3</sub> ) DIC <sup>14</sup> and waters with complex organic chemistry, results can vary significantly outside of this expectation.	47.9 +/- 0.2 pMC	0.4786 +/- 0.0018	-19.4 o/oo

Dates are reported as RCYBP (radiocarbon years before present, "present" = AD 1950). By international convention, the modern reference standard was 95% the <sup>14</sup>C activity of the National Institute of Standards and Technology (NIST) Oxalic Acid (SRM 4990C) and calculated using the Libby <sup>14</sup>C half-life (5568 years). Quoted errors represent 1 relative standard deviation statistics (68% probability) counting errors based on the combined measurements of the sample, background, and modern reference standards. Measured <sup>13</sup>C/<sup>12</sup>C ratios (delta <sup>13</sup>C) were calculated relative to the PDB-1 standard.

The Conventional Radiocarbon Age represents the Measured Radiocarbon Age corrected for isotopic fractionation, calculated using the delta <sup>13</sup>C. On rare occasion where the Conventional Radiocarbon Age was calculated using an assumed delta <sup>13</sup>C, the ratio and the Conventional Radiocarbon Age will be followed by "m". The Conventional Radiocarbon Age is not calendar calibrated. When available, the Calendar Calibrated result is calculated from the Conventional Radiocarbon Age and is listed as the "Two Sigma Calibrated Result" for each sample.



REPORT OF RADIOCARBON DATING ANALYSES

Mr. David Rugh

Report Date: 5/7/2015

Table with 4 columns: Sample Data, pMC, Fmdn, d13C. Contains three rows of data for samples Beta-409512, Beta-409513, and Beta-409514, each with associated sample ID, analysis type, material/pretreatment, and a detailed comment.

Dates are reported as RCYBP (radiocarbon years before present, "present" = AD 1950). By international convention, the modern reference standard was 95% the 14C activity of the National Institute of Standards and Technology (NIST) Oxalic Acid (SRM 4990C) and calculated using the Libby 14C half-life (5568 years). Quoted errors represent 1 relative standard deviation statistics (68% probability) counting errors based on the combined measurements of the sample, background, and modern reference standards. Measured 13C/12C ratios (delta 13C) were calculated relative to the PDB-1 standard.

The Conventional Radiocarbon Age represents the Measured Radiocarbon Age corrected for isotopic fractionation, calculated using the delta 13C. On rare occasion where the Conventional Radiocarbon Age was calculated using an assumed delta 13C, the ratio and the Conventional Radiocarbon Age will be followed by "...". The Conventional Radiocarbon Age is not calendar calibrated. When available, the Calendar Calibrated result is calculated from the Conventional Radiocarbon Age and is listed as the "Two Sigma Calibrated Result" for each sample.



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Mr. Darden Hood  
President

Mr. Ronald Hatfield  
Mr. Christopher Patrick  
Deputy Directors

The Radiocarbon Laboratory Accredited to ISO/IEC 17025:2005 Testing Accreditation PJLA #59423

## Quality Assurance Report

This report provides the results of reference materials used to validate radiocarbon analyses prior to reporting. Known value reference materials were analyzed quasi-simultaneously with the unknowns. Results are reported as expected values vs measured values. Reported values are calculated relative to NIST SRM-4990B and corrected for isotopic fractionation. Results are reported using the direct analytical measure percent modern carbon (pMC) with one relative standard deviation.

Report Date: May 11, 2015  
Submitter : Mr. David Rugh

### QA MEASUREMENTS

Reference 1	Expected Value: 96.7 +/- 0.5 pMC Measured Value: 96.3 +/- 0.4 pMC Agreement: Accepted
Reference 2	Expected Value: 47.9 +/- 0.3 Measured Value: 47.9 +/- 0.2 pMC Agreement: Accepted
Reference 3	Expected Value: 27.2 +/- 0.2 Measured Value: 27.3 +/- 0.1 pMC Agreement: Accepted

COMMENT: All measurements passed acceptance tests.

Validation:

Date: May 11, 2015

## **APPENDIX B**

**Well Logs for Study Area Wells  
Deeper than 400 Feet (Sections 21,  
22, 27, 28 of T13N/R13E)**



# WATER WELL REPORT

STATE OF WASHINGTON

Application No. \_\_\_\_\_  
 Permit No. \_\_\_\_\_

(1) **OWNER:** Name John Mott Address 2101 S. 324th Federal Way, Wa.  
 (2) **LOCATION OF WELL:** County Klickitat - NW  $\frac{1}{4}$  NE  $\frac{1}{4}$  Sec. 21 T. 3 N. R. 13E W.M.  
 \_\_\_\_\_ and distance from section or subdivision corner

(3) **PROPOSED USE:** Domestic  Industrial  Municipal   
 Irrigation  Test Well  Other

(4) **TYPE OF WORK:** Owner's number of well (if more than one) \_\_\_\_\_  
 Method: New well  Deepened  Reconditioned   
 Dug  Cable  Rotary   
 Bored  Driven  Jetted

(5) **DIMENSIONS:** Diameter of well \_\_\_\_\_ inches.  
 Drilled 490 ft. Depth of completed well 490 ft.

(6) **CONSTRUCTION DETAILS:**  
 Casing installed: 6 " Diam. from 0 ft. to 18 ft.  
 Threaded  " Diam. from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.  
 Welded  " Diam. from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.

Perforations: Yes  No   
 Type of perforator used \_\_\_\_\_  
 SIZE of perforations \_\_\_\_\_ in. by \_\_\_\_\_ in.  
 \_\_\_\_\_ perforations from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.  
 \_\_\_\_\_ perforations from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.  
 \_\_\_\_\_ perforations from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.

Screens: Yes  No   
 Manufacturer's Name \_\_\_\_\_  
 Type \_\_\_\_\_ Model No. \_\_\_\_\_  
 Diam. \_\_\_\_\_ Slot size \_\_\_\_\_ from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.  
 Diam. \_\_\_\_\_ Slot size \_\_\_\_\_ from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.

Gravel packed: Yes  No  Size of gravel: \_\_\_\_\_  
 Gravel placed from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.

Surface seal: Yes  No  To what depth? 18 ft.  
 Material used in seal Bentonite  
 Did any strata contain unusable water? Yes  No   
 Type of water? \_\_\_\_\_ Depth of strata \_\_\_\_\_  
 Method of sealing strata off \_\_\_\_\_

(7) **PUMP:** Manufacturer's Name \_\_\_\_\_  
 Type \_\_\_\_\_ H.P. \_\_\_\_\_

(8) **WATER LEVELS:** Land-surface elevation 1500 ft.  
 above mean sea level. Static level 247 ft. below top of well Date 9 June  
 Artesian pressure \_\_\_\_\_ lbs. per square inch Date \_\_\_\_\_  
 Artesian water is controlled by \_\_\_\_\_ (Cap, valve, etc.)

(9) **WELL TESTS:** Drawdown is amount water level is lowered below static level  
 Was a pump test made? Yes  No  If yes, by whom? \_\_\_\_\_  
 Yield: \_\_\_\_\_ gal./min. with \_\_\_\_\_ ft. drawdown after \_\_\_\_\_ hrs.  
" 15 gal min ait test with drillpipe "  
" at 490' for one hour "

Recovery data (time taken as zero when pump turned off) (water level measured from well top to water level)

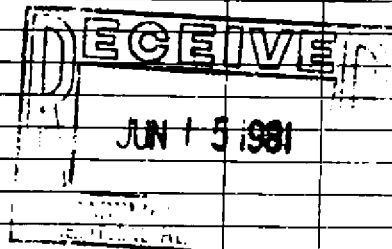
Time	Water Level	Time	Water Level	Time	Water Level

Rate of test \_\_\_\_\_  
 Better test \_\_\_\_\_ gal./min. with \_\_\_\_\_ ft. drawdown after \_\_\_\_\_ hrs.  
 Artesian flow \_\_\_\_\_ g.p.m. Date \_\_\_\_\_  
 Temperature of water \_\_\_\_\_ Was a chemical analysis made? Yes  No

**(10) WELL LOG:**

Formation: Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change of formation.

MATERIAL	FROM	TO
Soil	0	8
Basalt gray	8	37
Basalt brown	37	41
Basalt gray	41	46
Rock brown soft	46	55
Basalt gray	55	88
Conglomerate	88	112
Basalt gray hard	112	441
Basalt black visic.	441	460
Conglomerate WB	460	470
Basalt black WB	470	490



Work started 6 June, 1981 Completed 9 June, 1981

**WELL DRILLER'S STATEMENT:**

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

NAME Murray Well Drilling Inc.  
 (Person, firm, or corporation) (Type or print)

Address 3712 W. 8th The Dalles, Oregon

[Signed] Richard Murray  
 (Well Driller)

License No. 325 Date 11 June, 1981

DK 6.16.81

The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

# WATER WELL REPORT

STATE OF WASHINGTON

Application No. \_\_\_\_\_  
 Permit No. \_\_\_\_\_

(1) **OWNER:** Name Doug Taylor Address Rt.4 Box 84 Lyle, Wa.  
 (2) **LOCATION OF WELL:** County Klickitat - NE SW 21 3 13E  
 and distance from section or subdivision corner

(3) **PROPOSED USE:** Domestic  Industrial  Municipal   
 Irrigation  Test Well  Other

(4) **TYPE OF WORK:** Owner's number of well (if more than one) \_\_\_\_\_  
 New well  Method: Dug  Bored   
 Deepened  Cable  Driven   
 Reconditioned  Rotary  Jetted

(5) **DIMENSIONS:** Diameter of well 6 inches.  
 Drilled 449 ft. Depth of completed well 449 ft.

(6) **CONSTRUCTION DETAILS:**  
 Casing installed: \_\_\_\_\_ " Diam. from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.  
 Threaded  \_\_\_\_\_ " Diam. from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.  
 Welded  \_\_\_\_\_ " Diam. from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.  
 Perforations: Yes  No   
 Type of perforator used \_\_\_\_\_  
 SIZE of perforations \_\_\_\_\_ in. by \_\_\_\_\_ in.  
 \_\_\_\_\_ perforations from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.  
 \_\_\_\_\_ perforations from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.  
 \_\_\_\_\_ perforations from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.

Screens: Yes  No   
 Manufacturer's Name \_\_\_\_\_  
 Type \_\_\_\_\_ Model No \_\_\_\_\_  
 Diam. \_\_\_\_\_ Slot size \_\_\_\_\_ from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.  
 Diam. \_\_\_\_\_ Slot size \_\_\_\_\_ from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.

Gravel packed: Yes  No  Size of gravel: \_\_\_\_\_  
 Gravel placed from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.

Surface seal: Yes  No  To what depth? \_\_\_\_\_ ft.  
 Material used in seal \_\_\_\_\_  
 Did any strata contain unusable water? Yes  No   
 Type of water? \_\_\_\_\_ Depth of strata \_\_\_\_\_  
 Method of sealing strata off \_\_\_\_\_

(7) **PUMP:** Manufacturer's Name \_\_\_\_\_  
 Type: \_\_\_\_\_ H.P.

(8) **WATER LEVELS:** Land-surface elevation 1500 ft.  
 above mean sea level. Static level 98 ft. below top of well Date 30 May  
 Artesian pressure \_\_\_\_\_ lbs. per square inch Date \_\_\_\_\_  
 Artesian water is controlled by \_\_\_\_\_ (Cap, valve, etc.)

(9) **WELL TESTS:** Drawdown is amount water level is lowered below static level  
 Was a pump test made? Yes  No  If yes, by whom? \_\_\_\_\_  
 Yield: \_\_\_\_\_ gal./min. with \_\_\_\_\_ ft. drawdown after \_\_\_\_\_ hrs.  
100 gal min air test with the drill - steel at 449' for 1 hr. "  
 Recovery data (time taken as zero when pump turned off) (water level measured from well top to water level)  

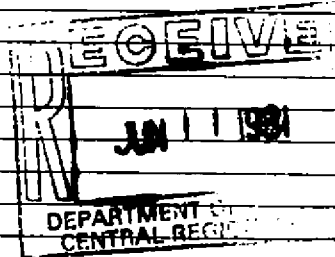
Time	Water Level	Time	Water Level	Time	Water Level

 Date of test \_\_\_\_\_  
 Bailer test \_\_\_\_\_ gal./min. with \_\_\_\_\_ ft. drawdown after \_\_\_\_\_ hrs.  
 Artesian flow \_\_\_\_\_ g.p.m. Date \_\_\_\_\_  
 Temperature of water \_\_\_\_\_ Was a chemical analysis made? Yes  No

(10) **WELL LOG:**  
 Formation: Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change of formation.

MATERIAL	FROM	TO
Basalt gray	205	248
Rock black	248	251
Basalt gray WB	251	350
Clay green	350	353
Basalt gray WB	353	435
Basalt black visic. WB	435	449

This could be developed into a very high yield well for irrigation as we did not go through the aquifer.



Work started 23 May 1981 Completed 30 May 1981

**WELL DRILLER'S STATEMENT:**  
 This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.  
 NAME Murray Well Drilling Inc.  
 (Person, firm, or corporation) (Type or print)  
 Address 3712 W 8th The Dalles, Oregon  
 [Signed] Richard J Murray  
 (Well Driller)  
 License No. 325 Date 8 June 1981

The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

AK 6/12/81

# WATER WELL REPORT

STATE OF WASHINGTON

Application No. L  
 Permit No. \_\_\_\_\_

(1) OWNER: Name Marcus Willis Address 15813 N.E. F. Plain Vancouver  
 LOCATION OF WELL: County Klickitat - NE 1/4 SW 1/4 Sec. 21 T. 3 N., R. 13 E. W.M.  
 Bearing and distance from section or subdivision corner SE Lot 8 Klickitat Ranch

(3) PROPOSED USE: Domestic  Industrial  Municipal   
 Irrigation  Test Well  Other

(4) TYPE OF WORK: Owner's number of well (if more than one) \_\_\_\_\_  
 New well  Method: Dug  Bored   
 Deepened  Cable  Driven   
 Reconditioned  Rotary  Jetted

(5) DIMENSIONS: Diameter of well 6 inches.  
 Drilled 550 ft. Depth of completed well 550 ft.

(6) CONSTRUCTION DETAILS:  
 Casing installed: 6" Diam. from 4" ft. to 87 ft.  
 Threaded  " Diam. from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.  
 Welded  " Diam. from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.  
 Perforations: Yes  No   
 Type of perforator used \_\_\_\_\_  
 SIZE of perforations \_\_\_\_\_ in. by \_\_\_\_\_ in.  
 \_\_\_\_\_ perforations from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.  
 \_\_\_\_\_ perforations from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.  
 \_\_\_\_\_ perforations from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.

Screens: Yes  No   
 Manufacturer's Name \_\_\_\_\_  
 Type \_\_\_\_\_ Model No. \_\_\_\_\_  
 Diam. \_\_\_\_\_ Slot size \_\_\_\_\_ from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.  
 Diam. \_\_\_\_\_ Slot size \_\_\_\_\_ from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.

Gravel packed: Yes  No  Size of gravel: \_\_\_\_\_  
 Gravel placed from \_\_\_\_\_ ft. to \_\_\_\_\_ ft.

Surface seal: Yes  No  To what depth? 25 ft.  
 Material used in seal Cement & bentonite  
 Did any strata contain unusable water? Yes  No   
 Type of water? \_\_\_\_\_ Depth of strata \_\_\_\_\_  
 Method of sealing strata off \_\_\_\_\_

(7) PUMP: Manufacturer's Name \_\_\_\_\_  
 Type: \_\_\_\_\_ H.P.

(8) WATER LEVELS: Land-surface elevation \_\_\_\_\_ ft.  
 above mean sea level. \_\_\_\_\_ ft.  
 Static level 370 ft. below top of well Date 4-11-83  
 Artesian pressure \_\_\_\_\_ lbs. per square inch Date \_\_\_\_\_  
 Artesian water is controlled by \_\_\_\_\_ (Cap, valve, etc.)

(9) WELL TESTS: Drawdown is amount water level is lowered below static level  
 Was a pump test made? Yes  No  If yes, by whom? \_\_\_\_\_  
 Yield: gal./min. with \_\_\_\_\_ ft. drawdown after \_\_\_\_\_ hrs.  
 " " " " " "  
 " " " " " "  
 Recovery data (time taken as zero when pump turned off) (water level measured from well top to water level)  

Time	Water Level	Time	Water Level	Time	Water Level
3:00	370	3:05	365	3:10	360
3:15	355	3:20	350	3:25	345
3:30	340	3:35	335	3:40	330
3:45	325	3:50	320	3:55	315
4:00	310	4:05	305	4:10	300
4:15	295	4:20	290	4:25	285
4:30	280	4:35	275	4:40	270
4:45	265	4:50	260	4:55	255
5:00	250	5:05	245	5:10	240
5:15	235	5:20	230	5:25	225
5:30	220	5:35	215	5:40	210
5:45	205	5:50	200	5:55	195
6:00	190	6:05	185	6:10	180
6:15	175	6:20	170	6:25	165
6:30	160	6:35	155	6:40	150
6:45	145	6:50	140	6:55	135
7:00	130	7:05	125	7:10	120
7:15	115	7:20	110	7:25	105
7:30	100	7:35	95	7:40	90
7:45	85	7:50	80	7:55	75
8:00	70	8:05	65	8:10	60
8:15	55	8:20	50	8:25	45
8:30	40	8:35	35	8:40	30
8:45	25	8:50	20	8:55	15
9:00	10	9:05	5	9:10	0

 Baller test \_\_\_\_\_ gal./min. with \_\_\_\_\_ ft. drawdown after \_\_\_\_\_ hrs.  
 Artesian flow \_\_\_\_\_ g.p.m. Date \_\_\_\_\_  
 Temperature of water \_\_\_\_\_ Was a chemical analysis made? Yes  No

(10) WELL LOG:  
 Formation: Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change of formation.

MATERIAL	FROM	TO
Top Soil	0'	3'
River gravel cemented, brown basalt, brown clay	3'	46'
White clay	46'	71'
river gravel cemented	71'	75'
brown basalt, med	75'	87'
brown basalt, med. hard	87'	110'
brown basalt, broken	110'	113'
brown basalt, med. hard	113'	128'
brown basalt, L. brown clay	128'	133'
gray basalt, hard	133'	168'
brown basalt, med. hard	168'	232'
White clay	232'	236'
brown basalt; White clay	236'	239'
brown basalt, porous	239'	246'
brown's gray basalt, med. hard	246'	250'
gray basalt, hard	250'	274'
brown basalt, porous, med.	274'	285'
brown basalt, med. hard	285'	293'
gray basalt, hard	293'	433'
brown basalt, med. hard	433'	445'
gray basalt, hard	445'	453'
brown basalt, porous, med.	453'	482'
gray basalt, hard	482'	550'

Work started 4-4- 1983 Completed 4-11- 1983

WELL DRILLER'S STATEMENT:  
 This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.  
 NAME M-K Drilling Company  
 (Person, firm, or corporation) (Type or print)  
 Address P.O. Box 373 Dallesport, WA 98611  
 [Signed] Karl S Moon  
 (Well Driller)  
 License No. 0973 Date 4-11 1983

The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

4767

M

**WATER WELL REPORT**  
STATE OF WASHINGTON

Start Card No. 079095  
Water Right Permit No. N/A

(1) OWNER: Name **ROGERS, ERIC** Address **BOX 727 BINGEN, WA 98605-**

(2) LOCATION OF WELL: County **Klickitat** - NW 1/4 SW 1/4 Sec 21 T 3 N., R 13E W4  
(2a) STREET ADDRESS OF WELL (or nearest address) **WINNY RIDGE RD.**

(3) PROPOSED USE: **DOMESTIC** (10) WELL LOG

(4) TYPE OF WORK: Owner's Number of well (if more than one) **NEW WELL**  
Method: **ROTARY**

Formations: Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change in formation.

(5) DIMENSIONS: Diameter of well **6** inches  
Drilled **465** ft. Depth of completed well **465** ft.

MATERIAL	FROM	TO
TOP SOIL & RIVER GRAVEL	0	3
CEMENTED GRAVEL	3	16
BROWN CLAY & RIVER GRAVEL	16	28
CEMENTED GRAVEL	28	42
WHITE SILTSTONE	42	59
BROWN SANDSTONE	59	78
BROWN BASALT & CLAY	78	103
BLACK BASALT	103	112
GRAY BASALT, HARD	112	228
BROWN BASALT	228	234
BLACK BASALT & BLUE CLAYSTONE	234	242
GRAY BASALT, HARD	242	287
BROWN BASALT & CLAY	287	293
GRAY BASALT, HARD	297	435
BLACK & RED BASALT, WATER BEARING	435	465

(6) CONSTRUCTION DETAILS:  
Casing installed: **6** " Dia. from **-1** ft. to **104.5** ft.  
**WELDED** " Dia. from ft. to ft.  
" Dia. from ft. to ft.

Perforations: **NO**  
Type of perforator used  
SIZE of perforations in. by in.  
perforations from ft. to ft.  
perforations from ft. to ft.  
perforations from ft. to ft.

Screens: **NO**  
Manufacturer's Name  
Type Model No.  
Diam. slot size from ft. to ft.  
Diam. slot size from ft. to ft.

Gravel packed: **NO** Size of gravel  
Gravel placed from ft. to ft.

Surface seal: **YES** To what depth? **30** ft.  
Material used in seal **CEMENT & BENTONITE**.  
Do any strata contain unusable water? **NO**  
Type of water? Depth of strata ft.  
Method of sealing strata off

(7) PUMP: Manufacturer's Name  
Type H.P.

(8) WATER LEVELS: Land-surface elevation  
above mean sea level ... ft.  
Static level **365** ft. below top of well Date **03/25/90**  
Artesian Pressure lbs. per square inch Date  
Artesian water controlled by

Work started **12/11/90** Completed **03/25/91**

(9) WELL TESTS: Drawdown is amount water level is lowered below static level.  
Was a pump test made? **NO** If yes, by whom?  
Yield: gal./min with ft. drawdown after hrs.

WELL CONSTRUCTOR CERTIFICATION:  
I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards. Materials used and the information reported above are true to my best knowledge and belief.

Recovery data  
Time Water Level Time Water Level Time Water Level

NAME **M-K WELL DRILLING CO.**  
(Person, firm, or corporation) (Type or print)

Date of test / /  
Boiler test gal/min. ft. drawdown after hrs.  
Air test 20 gal/min. w/ steel set at **455** ft. for 1 hrs.  
Artesian flow g.p.m. Date  
Temperature of water Was a chemical analysis made? **NO**

ADDRESS **P.O. BOX 373 DANESPORT, WA 98617**  
(SIGNED) Charles S. Moore License No. **853 & 834 & 973**  
Contractor's Registration No. **KKDRIC134PE** Date **03/25/91**

WATER WELL REPORT  
STATE OF WASHINGTON

Start Card No. W 094076  
Water Right Permit No.

(1) OWNER: Name WILKINS, MAYLAND (01233) Address PO BOX 820 LYLE, WA 98635-

(2) LOCATION OF WELL: County KLUCKITAT - NW 1/4 SW 1/4 Sec 21 T 3 N., R 13E WM  
(2a) STREET ADDRESS OF WELL (or nearest address) WINDY RIVER RD, LYLE

(3) PROPOSED USE: DOMESTIC

(4) TYPE OF WORK: Owner's Number of well 01  
DEEPEMED Method: ROTARY

(5) DIMENSIONS: Diameter of well 6 inches  
Drilled 520 ft. Depth of completed well 520 ft.

(6) CONSTRUCTION DETAILS:  
Casing installed: " Dia. from ft. to ft.  
" Dia. from ft. to ft.  
" Dia. from ft. to ft.

Perforations: NO  
Type of perforator used  
SIZE of perforations in. by in.  
perforations from ft. to ft.  
perforations from ft. to ft.  
perforations from ft. to ft.

Screens: NO  
Manufacturer's Name  
Type from ft. to ft.  
Diam. slot size from ft. to ft.  
Diam. slot size from ft. to ft.

Gravel packed: NO  
Gravel placed from ft. to ft. Size of gravel ft.

Surface seal: YES To what depth? 30 ft.  
Material used in seal CEMENT & BENTON.  
Did any strata contain unusable water? NO  
Type of water? Depth of strata ft.  
Method of sealing strata off

(7) PUMP: Manufacturer's Name  
Type H.P.

(8) WATER LEVELS: Land-surface elevation  
above mean sea level ... ft.  
Static level 425 ft. below top of well Date 07/11/97  
Artesian Pressure lbs. per square inch Date  
Artesian water controlled by

(9) WELL TESTS: Drawdown is amount water level is lowered below static level.  
Was a pump test made? NO If yes, by whom?  
Yield: gal./min with ft. drawdown after hrs.

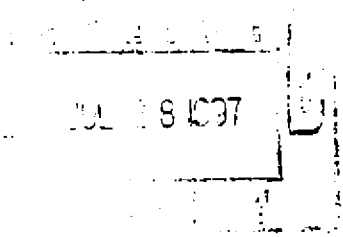
Recovery data  
Time Water Level Time Water Level Time Water Level

Date of test 7/11  
Bailer test gal./min. ft. drawdown after hrs.  
Air test 15 gal./min. w/ stem set at 510 ft. for 1 hrs.  
Artesian flow g.p.m. Date  
Temperature of water Was a chemical analysis made? NO

(10) WELL LOG ID# ACL 787

Formation: Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change in formation.

MATERIAL	FROM	TO
GRAY BASALT, HARD	465	473
BLACK BASALT & BLUE CLAYSTONE	473	482
BLACK BASALT, MEDIUM HARD	482	488
GRAY BASALT, HARD	488	520



Work started 07/02/97 Completed 07/11/97

WELL CONSTRUCTOR CERTIFICATION:  
I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards. Materials used and the information reported above are true to my best knowledge and belief.

NAME M-K DRILLING CO.  
(Person, firm, or corporation) (Type or print)

ADDRESS BOX 470 DALLESPORE, WA  
[SIGNED] *Paul Martin* License No. 833 & 834 & 973

Contractor's  
Registration No. MKDRIC134PE Date 07/15/97

The Dep. The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

WATER WELL REPORT  
STATE OF WASHINGTON

Start Card No. 079139  
Water Right Permit No.

(1) OWNER: Name WOLMAN, ABEL 00331 Address 2104 W. ROGERS AV. BALTIMORE, MD 21209-  
- SW 1/4 SE 1/4 Sec 21 T 3N W., R 13 WN

LOCATION OF WELL: County KLIKITAT  
(2a) STREET ADDRESS OF WELL (or nearest address) WIND RIDGE

(3) PROPOSED USE: DOMESTIC

(4) TYPE OF WORK: Owner's Number of well 1  
NEW WELL Method: ROTARY

(5) DIMENSIONS: Diameter of well 6 inches  
Drilled 520 ft. Depth of completed well 520 ft.

(6) CONSTRUCTION DETAILS:  
Casing installed: 6 - Dia. from -1 ft. to 108 ft.  
WELDED 4.5 - Dia. from 220 ft. to 520 ft.  
Dia. from ft. to ft.

Perforations: YES  
Type of perforator used SAW  
SIZE of perforations 1/8 in. by 4 in.  
50 perforations from 340 ft. to 510 ft.  
perforations from ft. to ft.  
perforations from ft. to ft.

Screens: NO  
Manufacturer's Name Model No.  
Type slot size from ft. to ft.  
Diam. slot size from ft. to ft.  
Diam. slot size from ft. to ft.

Gravel packed: NO  
Gravel placed from ft. to ft. Size of gravel ft.

Surface seal: YES To what depth? 25 ft.  
Material used in seal CEMENT & BENTO.  
Did any strata contain unusable water? NO  
Type of water? Depth of strata ft.  
Method of sealing strata off

(7) PUMP: Manufacturer's Name Type H.P.

(8) WATER LEVELS: Land-surface elevation ft.  
above mean sea level  
- Static level 305 ft. below top of well. Date 07/24/91  
Artesian Pressure lbs. per square inch Date  
Artesian water controlled by

(9) WELL TESTS: Drawdown is amount water level is lowered below static level.  
Was a pump test made? NO If yes, by whom?  
Yield: gal./min with ft. drawdown after hrs.

Recovery data  
Time Water Level Time Water Level Time Water Level

Date of test / /  
Boiler test gal./min. ft. drawdown after hrs.  
Air test 12 gal./min. w/ stem set at 510 ft. for 1 hrs.  
Artesian flow S.P.N. Date  
Temperature of water Was a chemical analysis made? NO

(10) WELL LOG  
Formation: Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change in formation.

MATERIAL	FROM	TO
BROWN CLAY	0	4
BROWN BASALT	4	39
CEMENTED RIVERGRAVEL	39	65
CEMENTED SAND & GRAVEL	65	76
WHITE CLAY	76	98
HARD	98	103
BLACK BASALT & GREEN CLAYSTONE	103	107
BLACK BASALT, HARD	107	127
GRAY BASALT, HARD	127	240
BROWN & BLACK CLAY BLACK BASALT	240	244
BLACK BASALT & BLUE CLAYSTONE	244	256
GRAY BASALT, HARD	256	307
BLACK BASALT, POROUS	307	312
GRAY BASALT	312	332
BROWN BASALT, POROUS, WATER BEARING	332	357
GRAY BASALT, HARD	357	423
BLACK BASALT, POROUS, WATER BEARING	423	429
GRAY BASALT	429	445
GRAY BASALT, HARD	445	462
GRAY BASALT	462	495
GRAY BASALT, HARD	495	520

Work started 07/19/91 Completed 07/24/91

WELL CONSTRUCTOR CERTIFICATION:  
I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards. Materials used and the information reported above are true to my best knowledge and belief.

NAME N-K WELL DRILLING CO.  
(Person, firm, or corporation) (Type or print)

ADDRESS BOX 470 DALLSPORT, WA.

[SIGNED] Charles B. Moore License No. 833 & 834 & 973

Contractor's Registration No. NEDRIC134PE Date 06/07/94

The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

36390

WATER WELL REPORT  
STATE OF WASHINGTON

Start Card No W 047720  
Water Right Permit No

(1) OWNER Name SPAULDING, BILL (01053) Address 107 ELM ST LYLE, WA 98635-  
 (2) LOCATION OF WELL County KLIICKITAT - SE 1/4 SE 1/4 Sec 21 T 3 N , R 13E WM  
 (2a) STREET ADDRESS OF WELL (or nearest address) OFF LYLE/CNTVILL RD,LYLE

(3) PROPOSED USE DOMESTIC

(4) TYPE OF WORK Owner's Number of well (If more than one) 01  
 Method ROTARY  
 NEW WELL

(5) DIMENSIONS Diameter of well 6 inches  
 Drilled 505 ft Depth of completed well 505 ft

(6) CONSTRUCTION DETAILS  
 Casing installed 6 " Dia from -1 ft to 90 ft  
 WELDED " Dia from ft to ft  
 " Dia from ft to ft

Perforations NO  
 Type of perforator used  
 SIZE of perforations in by in  
 perforations from ft to ft  
 perforations from ft to ft  
 perforations from ft to ft

Screens NO  
 Manufacturer's Name  
 Type Model No  
 Diam slot size from ft to ft  
 Diam slot size from ft to ft

Gravel packed NO  
 Gravel placed from ft to ft

Surface seal YES To what depth? 45 ft  
 Material used in seal CEMENT & BENTO  
 Did any strata contain unusable water? NO  
 Type of water? Depth of strata ft  
 Method of sealing strata off

(7) PUMP Manufacturer's Name  
 Type H P

(8) WATER LEVELS Land-surface elevation  
 above mean sea level ft  
 Static level 390 ft below top of well Date 06/01/95  
 Artesian Pressure lbs per square inch Date  
 Artesian water controlled by

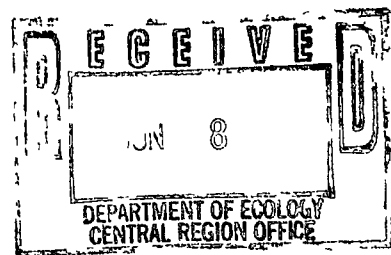
(9) WELL TESTS Drawdown is amount water level is lowered below static level  
 Was a pump test made? NO If yes, by whom?  
 Yield gal /min with ft drawdown after hrs

Recovery data  
 Time Water Level Time Water Level Time Water Level

Date of test / /  
 Bailer test gal/min ft drawdown after hrs  
 Air test 15 gal/min w/ stem set at 495 ft for 1 hrs  
 Artesian flow g p m Date  
 Temperature of water Was a chemical analysis made? NO

(10) WELL LOG  
 Formation Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change in formation

MATERIAL	FROM	TO
TOP SOIL	0	1
BROWN CLAY	1	8
BROWN BASALT & CLAY	8	24
SAND & GRAVEL	24	41
WHITE CLAY	41	70
BROWN BASALT ,MEDIUM	70	84
GRAY BASALT , HARD	84	111
BLACK BASALT , POROUS	111	119
GRAY BASALT , POROUS	119	210
GRAY BASALT , FRACTURED	210	218
GRAY BASALT , HARD	218	293
BROWN BASALT ,MEDIUM	293	302
GRAY BASALT , HARD	302	465
BLACK & GRAY BASALT CREVISED, , WATER BEARING	465	481
GRAY BASALT , HARD	481	505



Work started 05/31/95 Completed 06/01/95

WELL CONSTRUCTOR CERTIFICATION  
 I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards Materials used and the information reported above are true to my best knowledge and belief

NAME M-K DRILLING CO  
 (Person, firm, or corporation) (Type or print)  
 ADDRESS BOX 470 DALLESFORT, WA  
 [SIGNED] Charles S Moore License No (833) & 834 & 973  
 Contractor's Registration No MKDRIC134PE Date 06/05/95

The Dep. The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

WATER WELL REPORT  
STATE OF WASHINGTON

Start Card No. W100884  
Water Right Permit No.

(1) OWNER: Name FREE GERALD E (01350) Address 1320 BERYL ST SAN DIEGO, CA 92109-

(2) LOCATION OF WELL: County KLIKITAT - W 1/4 SE 1/4 Sec 21 T 3 N., R 13E WM  
(2a) STREET ADDRESS OF WELL (or nearest address) ODA KNIGHT RD LYLE WA

(3) PROPOSED USE: DOMESTIC

(10) WELL LOG ID # AC1506 K, Q

(4) TYPE OF WORK: Owner's Number of well (If more than one) 01  
NEW WELL Method: ROTARY

Formation: Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change in formation.

(5) DIMENSIONS: Diameter of well 6 inches  
Drilled 400 ft. Depth of completed well 400 ft.

MATERIAL	FROM	TO
TOP SOIL	0	2
BROWN CLAY & BROWN BASALT	2	6
BROWN BASALT, FRACTURED,	6	12
GRAY BASALT, MEDIUM HARD	12	32
BROWN BASALT, MEDIUM HARD	32	42
GRAY BASALT, MEDIUM HARD	42	60
GRAY BASALT, HARD	60	126
BLACK & GRAY BASALT, MEDIUM HARD	126	138
GRAY BASALT, HARD	138	190
BLACK BASALT, MEDIUM HARD	190	202
BROWN BASALT, MEDIUM HARD	202	212
GRAY BASALT, MEDIUM HARD	212	240
GRAY BASALT, HARD	240	348
BLACK BASALT, HARD	348	376
BROWN BASALT, MEDIUM HARD, WATER BEARING	376	395
GRAY BASALT, HARD	395	400

(6) CONSTRUCTION DETAILS:  
Casing installed: 6" Dia. from +1 ft. to 19 ft.  
WELDED " Dia. from ft. to ft.  
" Dia. from ft. to ft.

Perforations: NO  
Type of perforator used  
SIZE of perforations in. by in.  
perforations from ft. to ft.  
perforations from ft. to ft.  
perforations from ft. to ft.

Screens: NO  
Manufacturer's Name  
Type Model No.  
Diam. slot size from ft. to ft.  
Diam. slot size from ft. to ft.

Gravel packed: NO Size of gravel  
Gravel placed from ft. to ft.

Surface seal: YES To what depth? 18 ft.  
Material used in seal CEMENT & BENTON.  
Did any strata contain unusable water? NO  
Type of water? Depth of strata ft.  
Method of sealing strata off

(7) PUMP: Manufacturer's Name  
Type H.P.

(8) WATER LEVELS: Land-surface elevation  
above mean sea level ... ft.  
Static level 310 ft. below top of well Date 09/18/98  
Artesian Pressure lbs. per square inch Date  
Artesian water controlled by

Work started 09/16/98 Completed 09/18/98

(9) WELL TESTS: Drawdown is amount water level is lowered below static level.  
Was a pump test made? NO If yes, by whom?  
Yield: gal./min with ft. drawdown after hrs.

WELL CONSTRUCTOR CERTIFICATION:  
I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards. Materials used and the information reported above are true to my best knowledge and belief.

Recovery data  
Time Water Level Time Water Level Time Water Level

NAME M-K DRILLING CO.  
(Person, firm, or corporation) (Type or print)

ADDRESS BOX 470 DALLESPOIT, WA

Date of test / /  
Bailer test gal./min. ft. drawdown after hrs.  
Air test 12 gal./min. w/ stem set at 390 ft. for 1 hrs.  
Artesian flow g.p.m. Date  
Temperature of water Was a chemical analysis made? NO

[SIGNED] *Paul M. ...* License No. 833 & 834 & 973

Contractor's  
Registration No. MKDRIC134PE Date 09/21/98

The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

WATER WELL REPORT

Start Card No. W094067

STATE OF WASHINGTON

Unique Well I.D. # AFB015  
Water Right Permit No.

(1) OWNER: Name HUTCHISON DOUGLAS (01450) Address PO BOX 101 LYLE, WA 98635-0101

(2) LOCATION OF WELL: County KLIICKITAT *EW2* - SW 1/4 SW 1/4 Sec 22 T 3 N., R 13E WM  
(2a) STREET ADDRESS OF WELL (or nearest address) OFF CENTERVILLE HWY, LYLE

(3) PROPOSED USE: DOMESTIC

(10) WELL LOG

(4) TYPE OF WORK: Owner's Number of well (If more than one) 01  
NEW WELL Method: ROTARY

Formation: Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change in formation.

(5) DIMENSIONS: Diameter of well 6 inches  
Drilled 550 ft. Depth of completed well 550 ft.

MATERIAL	FROM	TO
TOP SOIL & CLAY	0	2
BROWN CLAY	2	11
BROWN BASALT	11	53
BROWN BASALT & WHITE CLAY	53	58
BROWN & GRAY BASALT	58	76
GRAY BASALT, HARD	76	148
BLACK BASALT, MEDIUM	148	158
GRAY BASALT, HARD	158	223
BROWN BASALT, HARD	223	225
BROWN BASALT, MEDIUM, POROUS	225	235
RED BASALT, POROUS	235	248
RED BASALT, MEDIUM HARD	248	253
GRAY BASALT, MEDIUM HARD	253	261
GRAY BASALT, HARD	261	326
BLACK BASALT W/GREEN & BROWN SEAMS	326	339
BLACK BASALT W/BLUE SEAMS PYRITE & WOOD	326	339
BLACK BASALT, HARD	339	346
BLACK BASALT, FRACTURED	346	356
BLACK BASALT, POROUS W/ GREEN CLAYSTONE & PYRITE	356	364
BLACK & GRAY BASALT, MEDIUM	364	378
GRAY BASALT, HARD	378	405
BLACK BASALT, FRACTURED, WATER BEARING	405	533
BLACK BASALT, HARD	533	545
	545	550

(6) CONSTRUCTION DETAILS:  
Casing installed: 6" Dia. from +1 ft. to 79 ft.  
WELDED " Dia. from ft. to ft.  
" Dia. from ft. to ft.

Perforations: NO  
Type of perforator used  
SIZE of perforations in. by in.  
perforations from ft. to ft.  
perforations from ft. to ft.  
perforations from ft. to ft.

Screens: NO  
Manufacturer's Name  
Type Model No.  
Diam. slot size from ft. to ft.  
Diam. slot size from ft. to ft.

Gravel packed: NO  
Gravel placed from ft. to ft. Size of gravel

Surface seal: YES To what depth? 25 ft.  
Material used in seal CEMENT & BENTON.  
Did any strata contain unusable water? NO  
Type of water? Depth of strata ft.  
Method of sealing strata off

(7) PUMP: Manufacturer's Name Type H.P.

(8) WATER LEVELS: Land-surface elevation above mean sea level ... ft.  
Static level 395 ft. below top of well Date 09/01/99  
Artesian Pressure lbs. per square inch Date  
Artesian water controlled by

Work started 08/30/99 Completed 09/01/99

(9) WELL TESTS: Drawdown is amount water level is lowered below static level.  
Was a pump test made? NO If yes, by whom?  
Yield: gal./min with ft. drawdown after hrs.

WELL CONSTRUCTOR CERTIFICATION:  
I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards. Materials used and the information reported above are true to my best knowledge and belief.

Recovery data  
Time Water Level Time Water Level Time Water Level

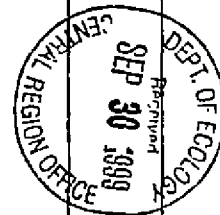
NAME M-K DRILLING CO.  
(Person, firm, or corporation) (Type or print)

ADDRESS BOX 470 DALLESPORT, WA

Date of test / /  
Bailer test gal./min. ft. drawdown after hrs.  
Air test 30 gal/min. w/ stem set at 440 ft. for 1 hrs.  
Artesian flow g.p.m. Date  
Temperature of water Was a chemical analysis made? NO

[SIGNED *Charles S. Moore* License No. 833 & 834 & 973

Contractor's Registration No. MKDRIC134PP Date 09/22/99



The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

WATER WELL REPORT

Start Card No W120589  
 Unique Well I D # AFB008  
 Water Right Permit No

STATE OF WASHINGTON

OWNER Name LONG GALE (01483) Address 3314 EDGEWOOD DR VANCOUVER, WA 98661-

LOCATION OF WELL County KLUCKITAT  
 (2a) STREET ADDRESS OF WELL (or nearest address) 7 5 MI UP LYLE-CENTERVILL, LYLE

(3) PROPOSED USE DOMESTIC

(4) TYPE OF WORK  
 NEW WELL  
 Owner's Number of well (If more than one) 01  
 Method ROTARY

(5) DIMENSIONS  
 Drilled 595 ft Diameter of well 6 inches  
 Depth of completed well 595 ft

(6) CONSTRUCTION DETAILS  
 Casing installed 6" Dia from +1 ft to 79 ft  
 WELDED 4 5" Dia from 15 ft to 595 ft

Perforations YES  
 Type of perforator used SAW  
 SIZE of perforations 1/8 in by 6 in  
 60 perforations from 555 ft to 595 ft  
 perforations from ft to ft  
 perforations from ft to ft

Screens NO  
 Manufacturer's Name  
 Type  
 Diam slot size from ft to ft  
 Diam slot size from ft to ft

Gravel packed NO  
 Gravel placed from ft to ft  
 Size of gravel

Surface seal YES To what depth? 25 ft  
 Material used in seal CEMENT & BENTO  
 Did any strata contain unusable water? NO  
 Type of water? Depth of strata  
 Method of sealing strata off

(7) PUMP Manufacturer's Name  
 Type H P

(8) WATER LEVELS  
 Land surface elevation above mean sea level ft  
 Static level 400 ft below top of well Date 11/16/99  
 Artesian Pressure lbs per square inch Date  
 Artesian water controlled by

(9) WELL TESTS Drawdown is amount water level is lowered below static level  
 Was a pump test made? NO If yes, by whom?  
 Yield gal/min with ft drawdown after hrs

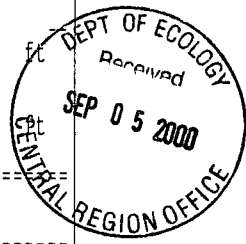
Recovery data  
 Time Water Level Time Water Level Time Water Level

Date of test / /  
 Bailer test gal/min ft drawdown after hrs  
 Air test 20 gal/min w/ stem set at 585 ft for 1 hrs  
 Artesian flow g p m Date  
 Temperature of water Was a chemical analysis made? NO

(10) WELL LOG

Formation Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change in formation

MATERIAL	FROM	TO
TOP SOIL	0	1
BROWN CLAY	1	10
BROWN BASALT, MEDIUM	10	27
WHITE CLAY	27	38
BROWN SANDSTONE	38	59
BROWN BASALT, MEDIUM	59	78
GRAY BASALT, HARD	78	107
BROWN BASALT, MEDIUM	107	118
GRAY & BLACK BASALT, HARD	118	208
BLACK BASALT W/GREEN CLAYSTONE	208	214
GRAY BASALT, HARD	214	286
BLACK BASALT W/BROWN SEAMS, MEDIUM HARD	286	294
GRAY BASALT, HARD	294	483
BLACK BASALT W/WHITE SEAMS, WATER BEARING	483	508
GRAY BASALT, HARD	508	573
BLACK BASALT, VERECULAR, WATER BEARING	573	592
GRAY BASALT, HARD	592	595



Corrected well log  
 \*See liner

Work started 11/11/99 Completed 11/16/99

WELL CONSTRUCTOR CERTIFICATION  
 I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards. Materials used and the information reported above are true to my best knowledge and belief

NAME M-K DRILLING CO  
 (Person, firm, or corporation) (Type or print)

ADDRESS BOX 470 DALLESFORT, WA

[SIGNED] Charles S Moore License No. 833 & 834 & 973

Contractor's Registration No MKDRIC134PE Date 08/09/00



# WATER WELL REPORT

Original & 1<sup>st</sup> copy - Ecology, 2<sup>nd</sup> copy - owner, 3<sup>rd</sup> copy - driller

CONSTRUCTION

Construction/Decommission ("x" in circle)

Construction

Decommission ORIGINAL INSTALLATION Notice

273540 of Intent Number

PROPOSED USE:  Domestic  Industrial  Municipal  
 DeWater  Irrigation  Test Well  Other

TYPE OF WORK: Owner's number of well (if more than one)  
 New well  Reconditioned Method:  Dug  Bored  Driven  
 Deepened  Cable  Rotary  Jetted

DIMENSIONS: Diameter of well 6 inches, drilled 577 ft.  
Depth of completed well 577 ft.

CONSTRUCTION DETAILS  
Casing:  Welded 6" Diam. from 2.5 ft. to 117.5 ft.  
Installed:  Liner installed 4" Diam. from 16 ft. to 557 ft.  
 Threaded " Diam. from ft. to ft.

Perforations:  Yes  No  
Type of perforator used \_\_\_\_\_  
SIZE of perfs in. by in. and no. of perfs from ft. to ft.

Screens:  Yes  No  K-Pac Location \_\_\_\_\_  
Manufacturer's Name Certa Loc  
Type PVC Sch 40 Model No. \_\_\_\_\_  
Diam. 4 Slot size .032 from 557 ft. to 577 ft.  
Diam. Slot size from ft. to ft.

Gravel/Filter packed:  Yes  No  Size of gravel/sand \_\_\_\_\_  
Materials placed from ft. to ft.

Surface Seal:  Yes  No To what depth? 117.5 ft.  
Material used in seal Bentonite Chips  
Did any strata contain unusable water?  Yes  No  
Type of water? \_\_\_\_\_ Depth of strata \_\_\_\_\_  
Method of sealing strata off \_\_\_\_\_

PUMP: Manufacturer's Name \_\_\_\_\_  
Type: \_\_\_\_\_ H.P.

WATER LEVELS: Land-surface elevation above mean sea level 1715 ft.  
Static level 345 ft. below top of well Date 9-25-07  
Artesian pressure \_\_\_\_\_ lbs. per square inch Date \_\_\_\_\_  
Artesian water is controlled by \_\_\_\_\_ (cap, valve, etc.)

WELL TESTS: Drawdown is amount water level is lowered below static level  
Was a pump test made?  Yes  No If yes, by whom? \_\_\_\_\_  
Yield: \_\_\_\_\_ gal./min. with \_\_\_\_\_ ft. drawdown after \_\_\_\_\_ hrs.  
Yield: \_\_\_\_\_ gal./min. with \_\_\_\_\_ ft. drawdown after \_\_\_\_\_ hrs.  
Yield: \_\_\_\_\_ gal./min. with \_\_\_\_\_ ft. drawdown after \_\_\_\_\_ hrs.

Recovery data (time taken as zero when pump turned off) (water level measured from well top to water level)

Time	Water Level	Time	Water Level	Time	Water Level

Date of test \_\_\_\_\_  
Bailer test \_\_\_\_\_ gal./min. with \_\_\_\_\_ ft. drawdown after \_\_\_\_\_ hrs.  
Airtest 85 gal./min. with stem set at 577 ft. for 1 hrs.  
Artesian flow \_\_\_\_\_ g.p.m. Date \_\_\_\_\_  
Temperature of water 60° Was a chemical analysis made?  Yes  No

## CURRENT

Notice of Intent No. W255885

Unique Ecology Well ID Tag No. APT511

Water Right Permit No. \_\_\_\_\_

Property Owner Name Kylea Garrett

Well Street Address Luffeld Road

City Lyle County Klickitat

Location SE 1/4-1/4 SW 1/4 Sec 22 Twn 3 R 13 EWM or WWM  check one

(Lat/Long (s, t, r Lat Deg N45° Lat Min/Sec 43.458

Still **REQUIRED**) Long Deg W121° Long Min/Sec 10.150

Tax Parcel No. 03132253000100

## CONSTRUCTION OR DECOMMISSION PROCEDURE

Formation: Describe by color, character, size of material and structure, and the kind and nature of the material in each stratum penetrated, with at least one entry for each change of information. (USE ADDITIONAL SHEETS IF NECESSARY.)

MATERIAL	FROM	TO
brown clay	0	9
broken brown & grey rock, few agates	9	55
light tan claystone going to sandstone	55	70
soft brown rock, sandstone	70	95
broken weathered brown rock - sandstone	95	101
hard grey basalt	101	195
soft brown rock	195	200
hard grey basalt	200	245
soft fractured black & grey rock	245	254
medium soft reddish grey rock	254	290
hard grey basalt with thin fractured layers	290	380
305-310 badly broken layer		
soft black basalt	380	387
med grey basalt	387	565
fractured grey basalt	565	567
black vesicular basalt, greenish claystone,	567	577
fractured black basalt w/reddish material in		
fractures W.B.		

P.H.: 6.5  
Hardness : 40ppm  
Iron : .05ppm  
Nitrate : N.D.

RECEIVED

OCT 03 2007

DEPARTMENT OF ECOLOGY  
WELL DRILLING UNIT

Start Date 9-24-2007

Completed Date 9-25-2007

WELL CONSTRUCTION CERTIFICATION: I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards. Materials used and the information reported above are true to my best knowledge and belief.

Driller  Engineer  Trainee Name (Print) Dwayne Person

Driller/Engineer/Trainee Signature [Signature]

Driller or trainee License No. 2705

Drilling Company Person Pump & Well Drilling

Address 166 Rimrock Road

City, State, Zip Goldendale, WA 98620

Contractor's Registration No. PERSOPW940PQ

Date 9-26-2007

IF TRAINEE,

Driller's Licensed No. \_\_\_\_\_

Driller's Signature \_\_\_\_\_

The Dep. The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

WATER WELL REPORT

Start Card No. W122802  
 Unique Well I.D. # APE005  
 Water Right Permit No.

STATE OF WASHINGTON

(1) OWNER: Name PALMER RIC (01482) Address PO BOX 495 LYLE, WA 98635-0495

(2) LOCATION OF WELL: County KLIICKITAT - NW 1/4 NE 1/4 Sec 27 T 3 N., R 13E WM  
 (2a) STREET ADDRESS OF WELL (or nearest address) 760 LYLE-CENTERVILLE HWY, LYLE

(3) PROPOSED USE: DOMESTIC (10) WELL LOG B

(4) TYPE OF WORK: Owner's Number of well (If more than one) 01  
 Method: ROTARY  
 NEW WELL

Formation: Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change in formation.

(5) DIMENSIONS: Diameter of well 6 inches  
 Drilled 335 ft. Depth of completed well 335 ft.

MATERIAL	FROM	TO
TOP SOIL	0	1
BROWN BASALT W/ CLAY	1	36
BROWN BASALT FRACTURED	36	124
BROWN & GRAY BASALT MEDIUM	124	163
BROWN BASALT FRACTURED	163	203
BROWN AGATE W/WHITE	203	218
CLAYSTONE	203	218
GRAY BASALT MEDIUM HARD	218	235
BROWN & GRAY BASALT	235	245
BROWN BASALT FRACTURED	245	255
GRAY BASALT HARD	255	270
BROWN & RED BASALT VESICULAR	270	279
WATER BEARING	270	279
BLACK BASALT HARD	279	305
BROWN & RED BASALT VESICULAR	305	320
GRAY BASALT HARD	320	335

(6) CONSTRUCTION DETAILS:  
 Casing installed: 6" Dia. from +1 ft. to 19 ft.  
 WELDED " Dia. from ft. to ft.  
 4.5" Dia. from 5 ft. to 325 ft.

Perforations: YES  
 Type of perforator used SAW  
 SIZE of perforations 1/8 in. by 6 in.  
 50 perforations from 285 ft. to 325 ft.  
 perforations from ft. to ft.  
 perforations from ft. to ft.

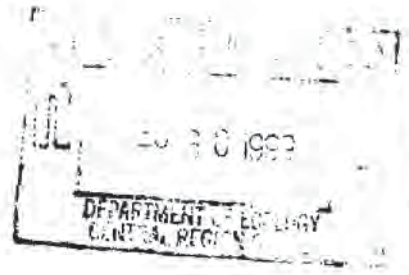
Screens: NO  
 Manufacturer's Name  
 Type Model No.  
 Diam. slot size from ft. to ft.  
 Diam. slot size from ft. to ft.

Gravel packed: NO  
 Gravel placed from ft. to ft. Size of gravel ft.

Surface seal: YES To what depth? 19 ft.  
 Material used in seal CEMENT & BENTON.  
 Did any strata contain unusable water? NO  
 Type of water? Depth of strata ft.  
 Method of sealing strata off

(7) PUMP: Manufacturer's Name Type H.P.

(8) WATER LEVELS: Land-surface elevation above mean sea level ... ft.  
 Static level 228 ft. below top of well Date 11/11/99  
 Artesian Pressure lbs. per square inch Date  
 Artesian water controlled by



Work started 11/09/99 Completed 11/11/99

(9) WELL TESTS: Drawdown is amount water level is lowered below static level.  
 Was a pump test made? NO If yes, by whom?  
 Yield: gal./min with ft. drawdown after hrs.

WELL CONSTRUCTOR CERTIFICATION:  
 I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards. Materials used and the information reported above are true to my best knowledge and belief.

Recovery data  
 Time Water Level Time Water Level Time Water Level

NAME M-K DRILLING CO.  
 (Person, firm, or corporation) (Type or print)  
 ADDRESS BOX 470 DALLSPORT, WA  
 [SIGNED Charles J. M... license No. 833 & 834 & 973  
 Contractor's Registration No. MKDRIC134PE Date 11/13/99

Date of test 1/1  
 Bailer test gal./min. ft. drawdown after hrs.  
 Air test 10 gal./min. w/ stem set at 325 ft. for 1 hrs.  
 Artesian flow g.p.m. Date  
 Temperature of water Was a chemical analysis made? NO



The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

104249

WATER WELL REPORT

Start Card No. W148860  
 Unique Well I.D. # AGM070  
 Water Right Permit No.

STATE OF WASHINGTON

(1) OWNER: Name ZABL JAMES B (01657) Address 1347 HRANY RD WHITE SALMON, WA 98672-

(2) LOCATION OF WELL: County KLUCKITAT - NW 1/4 NW 1/4 Sec 27 T 3 N., R 13E WM  
 (2a) STREET ADDRESS OF WELL (or nearest address) LOT 1 LYLE-CENTERVILLE RD, LYLE WA D

(3) PROPOSED USE: DOMESTIC (10) WELL LOG

(4) TYPE OF WORK: Owner's Number of well 1  
 (If more than one)  
 NEW WELL Method: ROTARY

(5) DIMENSIONS: Diameter of well 6 inches  
 Drilled 634 ft. Depth of completed well 634 ft.

(6) CONSTRUCTION DETAILS:  
 Casing installed: 6" Dia. from +1 ft. to 39 ft.  
 WBLDRD " Dia. from ft. to ft.  
 4.5" Dia. from 0 ft. to 350 ft.

Perforations: NO  
 Type of perforator used  
 SIZE of perforations in. by in.  
 perforations from ft. to ft.  
 perforations from ft. to ft.  
 perforations from ft. to ft.

Screens: NO  
 Manufacturer's Name  
 Type Model No.  
 Diam. slot size from ft. to ft.  
 Diam. slot size from ft. to ft.

Gravel packed: NO  
 Gravel placed from ft. to ft. Size of gravel

Surface seal: YES To what depth? 38 ft.  
 Material used in seal CEMENT & BENTONITE  
 Did any strata contain unusable water? NO  
 Type of water? Depth of strata ft.  
 Method of sealing strata off

(7) PUMP: Manufacturer's Name  
 Type H.P.

(8) WATER LEVELS: Land-surface elevation  
 above mean sea level ... ft.  
 Static level 155 ft. below top of well Date 10/08/01  
 Artesian Pressure lbs. per square inch Date  
 Artesian water controlled by

(9) WELL TESTS: Drawdown is amount water level is lowered below static level.  
 Was a pump test made? NO If yes, by whom?  
 Yield: gal./min with ft. drawdown after hrs.  
 Recovery data  
 Time Water Level Time Water Level Time Water Level

Date of test / /  
 Bailer test gal/min. ft. drawdown after hrs.  
 Air test 150 gal/min. w/ stem set at 624 ft. for / hrs.  
 Artesian flow g.p.m. Date  
 Temperature of water Was a chemical analysis made? NO

Formation: Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change in formation.

MATERIAL	FROM	TO
TOP SOIL	0	1
BROWN CLAY	1	31
BROWN BASALT, MEDIUM	31	88
BROWN BASALT, FRACTURED	88	110
BROWN BASALT W/GRAY CLAY	110	132
BROWN BASALT, MEDIUM	132	173
AGATE	173	179
BROWN BASALT, MEDIUM	179	185
GRAY BASALT, MEDIUM HARD	185	203
GRAY BASALT, HARD	203	230
GRAY BASALT BROWN SEAMS	230	238
GRAY BASALT, HARD	238	255
GRAY BASALT W/WHT MINERALS	255	260
BLACK SANDSTONE	260	268
GRAY BASALT, HARD	268	301
GRAY BASALT W/BROWN & BLACK SEAMS	301	309
GRAY BASALT, HARD	309	443
GRAY BASALT W/BROWN SEAMS	443	447
GRAY BASALT, HARD	447	625
GRAY BASALT, FRACTURED, WATER BEARING	625	634



Work started 10/03/01 Completed 10/08/01

WELL CONSTRUCTOR CERTIFICATION:  
 I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards. Materials used and the information reported above are true to my best knowledge and belief.

NAME M-K DRILLING CO.  
 (Person, firm, or corporation) (Type or print)  
 ADDRESS BOX 470 DALLESPORT, WA  
 [SIGNED] *Charles J. Moore* license No 833 & 834 & 973  
 Contractor's Registration No. MKDRIC134PE Date 10/09/01

# WATER WELL REPORT

STATE OF WASHINGTON

(1) OWNER Name Linda, John COX Address 2040 green ST. white Salmon WA.  
 (2) LOCATION OF WELL County Klickitat NW 1/4 NW 1/4 Sec 27 T. 3 N. R. 13E WM  
 (2a) STREET ADDRESS OF WELL (or nearest address) Adams view rd. D  
 TAX PARCEL NO \_\_\_\_\_

(3) PROPOSED USE  Domestic  Industrial  Municipal  
 Irrigation  Test Well  Other  
 DeWater

(4) TYPE OF WORK Owner's number of well (if more than one) \_\_\_\_\_  
 New Well Method \_\_\_\_\_  
 Deepened  Dug  Bored  
 Reconditioned  Cable  Driven  
 Decommission  Rotary  Jetted

(5) DIMENSIONS Diameter of well 6 inches  
 Drilled 200 feet Depth of completed well 200 ft

(6) CONSTRUCTION DETAILS  
 Casing Installed 6 Diam from +1 1/2 ft to 27 ft  
 Welded 4 Diam from -5 ft to 200 ft  
 Liner installed \_\_\_\_\_  
 Threaded \_\_\_\_\_

Perforations  Yes  No  
 Type of perforator used SAW  
 SIZE of perforations 6 in by 1/8 in  
36 perforations from 180 ft to 198 ft

Screens  Yes  No  K Pac Location \_\_\_\_\_  
 Manufacturer's Name \_\_\_\_\_  
 Type \_\_\_\_\_ Model No \_\_\_\_\_  
 Diam \_\_\_\_\_ Slot Size \_\_\_\_\_ from \_\_\_\_\_ ft to \_\_\_\_\_ ft  
 Diam \_\_\_\_\_ Slot Size \_\_\_\_\_ from \_\_\_\_\_ ft to \_\_\_\_\_ ft

Gravel/Filter packed  Yes  No  Size of gravel/sand \_\_\_\_\_  
 Material placed from \_\_\_\_\_ ft to \_\_\_\_\_ ft

Surface seal  Yes  No To what depth? 24 ft  
 Material used in seal Bentonite  
 Did any strata contain unusable water?  Yes  No  
 Type of water? \_\_\_\_\_ Depth of strata \_\_\_\_\_  
 Method of sealing strata off \_\_\_\_\_

(7) PUMP Manufacturer's Name myers  
 Type SUBMERSIBLE HP 1

(8) WATER LEVELS Land surface elevation above mean sea level \_\_\_\_\_ ft  
 Static level 178 ft below top of well Date April 01  
 Artesian pressure \_\_\_\_\_ lbs per square inch Date \_\_\_\_\_  
 Artesian water is controlled by \_\_\_\_\_ (Cap, valve, etc)

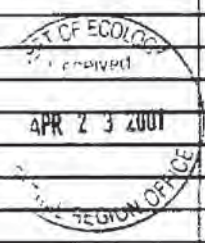
(9) WELL TESTS Drawdown is amount water level is lowered below static level  
 Was a pump test made?  Yes  No If yes by whom? \_\_\_\_\_  
 Yield \_\_\_\_\_ gal/min with \_\_\_\_\_ ft drawdown after \_\_\_\_\_ hrs  
 Yield \_\_\_\_\_ gal/min with \_\_\_\_\_ ft drawdown after \_\_\_\_\_ hrs  
 Yield \_\_\_\_\_ gal/min with \_\_\_\_\_ ft drawdown after \_\_\_\_\_ hrs  
 Recovery data (time taken as zero when pump turned off) (water level measured from well top to water level)  

Time	Water Level	Time	Water Level	Time	Water Level

 Date of test \_\_\_\_\_  
 Bailer test \_\_\_\_\_ gal/min with \_\_\_\_\_ ft drawdown after \_\_\_\_\_ hrs  
 Artesian 13 gal/min with \_\_\_\_\_ ft drawdown after 1 1/2 hrs  
 Artesian flow \_\_\_\_\_ gpm Date \_\_\_\_\_  
 Temperature of water 49 Was a chemical analysis made?  Yes  No

(10) WELL LOG or DECOMMISSIONING PROCEDURE DESCRIPTION  
 Formation Describe by color, character, size of material and structure, and the kind and nature of the material in each stratum penetrated, with at least one entry for each change of information Indicate all water encountered

MATERIAL	FROM	TO
SOIL	0	1 1/2
Brown CLAY with small gravel	1 1/2	21
Brown BASALT	21	127
HARD BROWN CLAY	127	138
<del>SOIL</del> cemented gravel	138	178
GRAY BROWN SANDY CLAY, HARD	178	182
FISSURED BASALT with	182	200



Work Started 4/6 01 Completed 4/7 01

**WELL CONSTRUCTION CERTIFICATION**  
 I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards. Materials used and the information reported above are true to my best knowledge and belief.  
 Type or Print Name Lindsay HAZARD License No 2498  
 (Licensed Driller/Engineer)  
 Trainee Name \_\_\_\_\_ License No \_\_\_\_\_  
 Drilling Company COLUMBIA WELL DRILLING  
 (Signed) Lindsay Hazard License No 2498  
 (Licensed Driller/Engineer)  
 Address PO BOX 1460, white Salmon WA, 9867  
 Contractor's Registration No Colum 0335 MD Date 4/17 01  
 (USE ADDITIONAL SHEETS IF NECESSARY)

The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

373656

WATER WELL REPORT

Start Card No. W268670

STATE OF WASHINGTON

Unique Well I.D. # AFQ965

Water Right Permit No.

(1) OWNER: Name COX JOHN A (02352) Address PO BOX 107 LYLE, WA 98635-

(2) LOCATION OF WELL: County KLUCKITAT - NW 1/4 NW 1/4 Sec 27 T 3 N., R 13E WM  
(2a) STREET ADDRESS OF WELL (or nearest address) 28 ADAMS VIEW DR, LYLE 03-13-2700-0005-00

(3) PROPOSED USE: DOMESTIC (10) WELL LOG

(4) TYPE OF WORK: Owner's Number of well (If more than one) 1  
DEEPEMED Method: ROTARY

Formation: Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change in formation.

(5) DIMENSIONS: Diameter of well 6 inches  
Drilled 465 ft. Depth of completed well 665 ft.

MATERIAL	FROM	TO
GRAY BASALT, HARD	200	241
GRAY BASALT W/BROWN SEAMS	241	260
BLACK BASALT, POROUS	260	285
GRAY BASALT, MEDIUM HARD	285	315
RED & BLACK BASALT, POROUS	315	332
GRAY BASALT, MEDIUM HARD	332	351
GRAY BASALT, HARD	351	462
BLACK & BLUE BASALT, MILD FRACTURED	462	482
GRAY & BLACK BASALT, MEDIUM HARD	482	500
GRAY BASALT, HARD	500	638
BLACK BASALT, POROUS W/	638	652
BLUE CLAYSTONE, WATER BEARING	638	665
GRAY BASALT, MEDIUM HARD	652	665

(6) CONSTRUCTION DETAILS:  
Casing installed: 4.5 " Dia. from 20 ft. to 660 ft.  
WELDED & LINER " Dia. from ft. to ft.  
" Dia. from ft. to ft.

Perforations: YES  
Type of perforator used SAW  
SIZE of perforations 1/8 in. by 6 in.  
40 perforations from 620 ft. to 660 ft.  
perforations from ft. to ft.  
perforations from ft. to ft.

Screens: NO  
Manufacturer's Name  
Type  
Diam. slot size from ft. to ft.  
Diam. slot size from ft. to ft.

Gravel packed: NO  
Gravel placed from ft. to ft. Size of gravel ft.

Surface seal: NO To what depth? ft.  
Material used in seal  
Did any strata contain unusable water? NO  
Type of water? Depth of strata ft.  
Method of sealing strata off

(7) PUMP: Manufacturer's Name  
Type H.P.

(8) WATER LEVELS: Land-surface elevation  
above mean sea level ... ft.  
Static level 480 ft. below top of well Date 02/17/10  
Artesian Pressure lbs. per square inch Date  
Artesian water controlled by

(9) WELL TESTS: Drawdown is amount water level is lowered below static level.  
Was a pump test made? NO If yes, by whom?  
Yield: gal./min with ft. drawdown after hrs.

Recovery data  
Time Water Level Time Water Level Time Water Level

Date of test 1/1  
Bailer test gal/min. ft. drawdown after hrs.  
Air test 25 gal/min. w/ stem set at 655 ft. for 1 hrs.  
Artesian flow g.p.m. Date  
Temperature of water Was a chemical analysis made? NO

Work started 02/12/10 Completed 02/17/10

WELL CONSTRUCTOR CERTIFICATION:  
I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards. Materials used and the information reported above are true to my best knowledge and belief.

NAME M-K DRILLING CO.  
(Person, firm, or corporation) (Type or print)  
ADDRESS PO BOX 470 DALLESPORT, WA  
[SIGNED] *[Signature]* License No. 0833,2740, (019)  
Contractor's  
Registration No. MKDRIC\*948Q7 Date 02/22/10

RECEIVED

FEB 25 2010

DEPARTMENT OF ECOLOGY - CENTRAL REGIONAL OFFICE





The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

181184

WATER WELL REPORT

Start Card No. W175990  
 Unique Well I.D. # ALC859  
 Water Right Permit No.

STATE OF WASHINGTON

(1) OWNER: Name **ESTRADA JOEL, DAMARIS(2004)** Address **PO BOX 644 LYLE, WA 98635-**

(2) LOCATION OF WELL: County **Klickitat** - **SE 1/4 SE 1/4 Sec 27 T 3 N., R 13E WM**  
 (2a) STREET ADDRESS OF WELL (or nearest address) **15 MT BUDMORE RD, LYLE**

(3) PROPOSED USE: **DOMESTIC**

(10) WELL LOG

**R**

(4) TYPE OF WORK: Owner's Number of well (If more than one) **1**  
**NEW WELL** Method: **ROTARY**

Formation: Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change in formation.

(5) DIMENSIONS: Diameter of well **6** inches  
 Drilled **370** ft. Depth of completed well **370** ft.

MATERIAL	FROM	TO
TOP SOIL	0	1
BROWN BASALT, FRACTURED	1	215
BROWN BASALT, MEDIUM HARD	215	271
GRAY BASALT	271	280
BROWN BASALT w/ AGATE	280	313
WATER BEARING	280	313
GRAY BASALT, HARD	313	355
BLACK & BLUE	355	365
BASALT, POROUS, WATER BEARING	355	365
GRAY BASALT	365	370

(6) CONSTRUCTION DETAILS:  
 Casing installed: **6** " Dia. from **+1** ft. to **319** ft.  
**WELDED & LINER** " Dia. from ft. to ft.  
 " Dia. from ft. to ft.

Perforations: **YES**  
 Type of perforator used **HOLTE**  
 SIZE of perforations **1/8** in. by **6** in.  
**30** perforations from **280** ft. to **310** ft.  
 perforations from ft. to ft.  
 perforations from ft. to ft.

Screens: **NO**  
 Manufacturer's Name  
 Type Model No.  
 Diam. slot size from ft. to ft.  
 Diam. slot size from ft. to ft.

Gravel packed: **NO** Size of gravel  
 Gravel placed from ft. to ft.

Surface seal: **YES** To what depth? **20** ft.  
 Material used in seal **CEMENT & BENTONITE**.  
 Did any strata contain unusable water? **NO**  
 Type of water? Depth of strata ft.  
 Method of sealing strata off

(7) PUMP: Manufacturer's Name  
 Type H.P.

(8) WATER LEVELS: Land-surface elevation  
 Static level **270** ft. above mean sea level ... ft.  
 Date **09/07/05**  
 Artesian Pressure lbs. per square inch Date  
 Artesian water controlled by

Work started **09/01/05** Completed **09/07/05**

(9) WELL TESTS: Drawdown is amount water level is lowered below static level.  
 Was a pump test made? **NO** If yes, by whom?  
 Yield: gal./min with ft. drawdown after hrs.

WELL CONSTRUCTOR CERTIFICATION:  
 I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards. Materials used and the information reported above are true to my best knowledge and belief.

Recovery data  
 Time Water Level Time Water Level Time Water Level

NAME **M-K DRILLING CO.**  
 (Person, firm, or corporation) (Type or print)

ADDRESS **BOX 470 DALLESPORT, WA**

Date of test **1/1**  
 Bailer test gal./min. ft. drawdown after hrs.  
 Air test **15** gal./min. w/ stem set at **360** ft. for **1** hrs.  
 Artesian flow g.p.m. Date  
 Temperature of water Was a chemical analysis made? **NO**

[SIGNED] *J. J. Thornton* License No. **0833,2740,2559**  
 Contractor's  
 Registration No. **MKDRIC134PE** Date **09/09/05**





The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

172045

WATER WELL REPORT

Start Card No. W183111  
Unique Well I.D. # ALC251  
Water Right Permit No.

STATE OF WASHINGTON

(1) OWNER: Name JENKINS STEPHEN (01941) Address P O BOX 93 LYLE, WA 98635-

(2) LOCATION OF WELL: County KLUCKITAT  
(2a) STREET ADDRESS OF WELL (or nearest address) 18 MT BUDMORE RD, LYLE - SW 1/4 NE 1/4 Sec 27 T 3 N., R 13E WM

(3) PROPOSED USE: DOMESTIC

(4) TYPE OF WORK: Owner's Number of well 1  
NEW WELL Method: ROTARY

(5) DIMENSIONS: Diameter of well 6 inches  
Drilled 330 ft. Depth of completed well 280 ft.

(6) CONSTRUCTION DETAILS:  
Casing installed: 6 " Dia. from +1 ft. to 19 ft.  
WELDED & LINER 4.5 " Dia. from 1 ft. to 280 ft.

Perforations: YES  
Type of perforator used SAW  
SIZE of perforations 1/8 in. by 6 in.  
80 perforations from 200 ft. to 280 ft.  
perforations from ft. to ft.  
perforations from ft. to ft.

Screens: NO  
Manufacturer's Name  
Type Model No.  
Diam. slot size from ft. to ft.  
Diam. slot size from ft. to ft.

Gravel packed: NO  
Gravel placed from ft. to ft. Size of gravel ft.

Surface seal: YES To what depth? 20 ft.  
Material used in seal CEMENT & BENTON.  
Did any strata contain unusable water? NO  
Type of water? Depth of strata ft.  
Method of sealing strata off

(7) PUMP: Manufacturer's Name Type H.P.

(8) WATER LEVELS: Land-surface elevation  
Static level 240 ft. below top of well Date 03/31/05  
Artesian Pressure lbs. per square inch Date  
Artesian water controlled by

(9) WELL TESTS: Drawdown is amount water level is lowered below static level.  
Was a pump test made? NO If yes, by whom?  
Yield: gal./min with ft. drawdown after hrs.

Recovery data  
Time Water Level Time Water Level Time Water Level  
Date of test / /  
Bailer test gal./min. ft. drawdown after hrs.  
Air test 20 gal./min. w/ stem set at 270 ft. for 1 hrs.  
Artesian flow g.p.m. Date  
Temperature of water Was a chemical analysis made? NO

(10) WELL LOG G  
Formation: Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change in formation.

MATERIAL	FROM	TO
TOP SOIL	0	2
BROWN BASALT, FRACTURED	2	55
BROWN BASALT, MEDIUM	55	82
BROWN BASALT, WEATHERED	82	120
GRAY & BROWN BASALT, FRACTURED	120	135
BROWN BASALT, WEATHERED	135	200
GRAY CLAYSTONE	200	215
WHITE CLAY & RIVERGRAVEL	215	230
BROWN SANDSTONE	230	245
BROWN BASALT, WEATHERED, WATER BEARING	245	275
BROWN BASALT w/ WHITE CLAYSTONE & BROWN SOAPSTONE	275	289
WATER BEARING	275	289
BROWN BASALT, WEATHERED	289	330

Work started 03/30/05 Completed 03/31/05

WELL CONSTRUCTOR CERTIFICATION:  
I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards. Materials used and the information reported above are true to my best knowledge and belief.

NAME M-K DRILLING CO.  
(Person, firm, or corporation) (Type or print)  
ADDRESS BOX 470 DALLSPORT, WA  
[SIGNBD] *Jyles Throner* License No. 0833,2740 (2559)  
Contractor's Registration No. MKDRIC134PE Date 04/04/05







